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AN ADDITIONAL STUDY AND IMPLEMENTATION OF  
TONE CALIBRATED TECHNIQUE OF MODULATION

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Final Report

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## 1. INTRODUCTION

The material presented in this Final report is concerned with the work performed on An Additional Study and Implementation of Tone Calibrated Technique of Modulation for the Jet Propulsion Laboratory, contract number 957190.

Earlier studies [1,2,3] have shown that pilot-aided coherent modulation techniques, of which the Tone Calibrated Technique (TCT) is an example, can be used to alleviate the effects of multipath fading in Land Mobile Radio (LMR) communication links. It appears, at the moment, that there are no commercial pilot-aided LMR links in operation. Conventional LMR links predominantly use non-coherent detection methods at the receiver to allow rapid burst signal acquisition. This also has the advantage of fast re-acquisition of the the transmit signal when multipath fading is encountered. However, non-coherent detection generally has a poorer bit error rate (BER) performance than coherent and differentially coherent detection schemes.

Coherent detection schemes which regenerate a phase reference directly from the received signal, are typically not used on LMR links due to the complexity involved in configuring them to track fading signals. As an alternative, pilot-aided techniques have much to offer due to the presence of a transmitted reference. They are the subject of this report. The differentially coherent receiver enjoys a BER performance which, for additive white gaussian channels, lies somewhere between that of the coherent and non-coherent detection schemes. In the presence of multipath fading, this receiver displays an irreducible error detection floor, just as the in the case of the non-coherent detector.

The TCT communication method has been shown [4] to be theoretically free from an error floor, and is only limited, in practice, by implementation constraints. Section 2 of this report introduces the concept of the TCT transmission scheme along with a baseband implementation of a suitable demodulator. Two techniques for the generation of the TCT signal are considered: a Manchester source encoding scheme (MTCT) and a subcarrier based technique (STCT).

Section 3 summarizes the results of the TCT link computer simulation which was previously described in detail in the First Interim Report[5]. Section 4 addresses the hardware implementation of the MTCT system and outlines the digital signal processing design considerations involved in satisfying the modulator/demodulator requirements.

Section 5 presents a discussion on the program findings and suggests future directions based on conclusions made regarding the suitability of the TCT system for the transmission channel presently under consideration.

## 2. TCT DATA TRANSMISSION SYSTEM

The Tone Calibrated Technique has been explored in a related program [1], sponsored by JPL, and discussed in the open literature [2]. The underlying concept is the use of a pilot, or tone, to synchronously remove channel perturbations from the data bearing sidebands and, simultaneously, perform coherent data detection. This requires that the pilot be situated at a suitable location in the transmit frequency band; the channel distortions should be distributed symmetrically around this location and there should be no data sideband energy present. It also assumes that the transmit link is linear to avoid capture of the pilot due to hardlimiting effects.

The TCT system positions the pilot at the midpoint of the transmit band. Prior to carrier modulation, the data modulated signal has been removed from this location by the creation of a spectral null at zero frequency. The data modulation scheme employed is M-ary Phase Shift Keying (PSK); this requirement is imposed by channel bandwidth constraints and is not a limitation of the TCT method, which is compatible with many other types of modulation schemes. For the given signalling requirements, the transmission of data at a rate of 2.4 kbps in a 3.6 kHz RF bandwidth, using quadriphase PSK (QPSK) modulation offers the minimum possible PSK signalling set.

The previous TCT program [1] was concerned with the proof-of-concept phase and was principally a hardware implementation study. Of major interest was the realization of the TCT demodulator and its performance in the presence

of additive white gaussian noise (AWGN) and hardware simulated multipath fading. An IF TCT demodulator was designed and studied. Results derived from the experimental set-up indicated that the pilot-aided demodulation could remove the error floor normally associated with non-coherent and strictly coherent receivers, the latter case holding true when conditioned on the fact that no attempt has been made to compensate for fading effects. This result was subsequently supported by theoretical analyses [4]. The TCT system bit error rate performance appears to be acceptable given the power penalty of including the pilot. This encouraging result was somewhat overshadowed by the doubling of the transmit bandwidth over that actually required by other modulation schemes. This is due to the Manchester source encoding which was employed to generate the spectral null around zero frequency.

Although the bandwidth constraints can be mitigated by using higher order PSK signalling sets, it is reasonable to assume that their use would cause the link bit error rate performance to degrade significantly due to the reduced decision space and sensitivity to the recovered pilot.

This report is concerned with two major areas of the TCT system, (a) the generation of the pre-modulation spectral null in the transmitter and (b) the use of baseband processing techniques to implement the demodulator. The use of digital signal processing elements to implement both the modulator and demodulator was considered to be a key element and, consequently, is a topic of detailed discussion in the report.

Two schemes were initially investigated for the generation of the TCT signalling format and are described in the remainder of this section. The first to be considered is based on a Manchester encoding scheme to generate the spectral null at the transmitter; this was the method investigated in the previous study. The other method considered centers on the use of subcarrier modulation techniques for spectral null generation. It was decided during the course of the program, primarily due to time constraints, to pursue only the Manchester TCT system to full hardware implementation.

## 2.1 Manchester Encoded TCT

### 2.1.1 Modulator

Manchester source encoding acts upon the input digital data in such a way as to redistribute the data energy away from zero frequency. The resulting power spectrum is given by:

$$M(f) = \sin^2(x) \text{sinc}^2(x) \quad (2.1)$$

where

$$x = \pi f T_s / 2$$

$$\text{sinc}(x) = \sin(x)/x$$

Eqn. (2.1) clearly shows that a null is created at zero frequency and that the main spectral lobe has almost doubled in width. To meet the single-sided RF occupancy requirements, which call for the transmit signal to be attenuated by 40dBC at 1.8 kHz removed from the center of the band, some form of spectral shaping must be used. The shaping employed is the raised-cosine pulse in the frequency domain with a maximum excess bandwidth fraction,  $\beta$ , of 0.5. The shaping is implemented as a time domain function and can be expressed as follows:

$$p(t) = \frac{\sin(\pi t/T_b)}{\pi t/T_b} \frac{\cos(\pi \beta t/T_b)}{(1-(2\beta t/T_b)^2)} \quad -\infty < t < \infty \quad (2.2)$$

where  $T_b$  is the bit rate, 2.4 kbps. The corresponding frequency spectrum is given by eqn.(2.3).

$$p(f) = \begin{cases} 1; & 0 \leq f \leq (1-\beta)/2T_b \\ \frac{1}{2}[1-\sin(\pi T_b(f-1/2T_b)/\beta)]; & \frac{(1-\beta)}{2T_b} \leq f \leq \frac{(1+\beta)}{2T_b} \end{cases} \quad (2.3)$$

As previously mentioned, the modulation scheme employed is QPSK, so the input data is split into even and odd streams, where the Manchester encoding and pulse-shaping will be performed independently of each other. Figure 2.1 illustrates the complete Manchester system pre-modulation data processing.

Included in both processing paths of Figure 2.1 are highpass filters to enlarge the necessary spectral null. It has been determined [1] that Manchester encoding by itself does not create a sufficiently wide spectral null. There is simply too much residual data energy which will overlap the pilot recovery passband at the receiver and result in the degradation of the TCT calibration process in the demodulator. Moreover, the pulse-shaping employed has a constant amplitude frequency response in the vicinity of d.c. (see 2.3), hence the need for additional spectral shaping through the use of the highpass filters.

The pre-modulation processing is implemented digitally, this allows for the use of linear phase, finite impulse response highpass filters. In this way, an attempt is made to minimize the effects of intersymbol interference (ISI) arising from the removal of the low frequency data energy.

The output of the highpass filters constitute the inphase (I) and quadrature (Q) components of the QPSK modulation. It is desired to use I and Q path staggering to generate offset QPSK (OQPSK) as this reduces transmit envelope amplitude variations. The Q path,  $S_q(t)$ , is therefore delayed  $T_b/2$  seconds relative to the I path,  $S_i(t)$ . The exact description of  $S_i(t)$  and  $S_q(t)$  is delayed until section 4.2 where they are described in relation to the hardware implementation. Signals  $S_i(t)$  and  $S_q(t)$  are converted to analog waveforms, then passed through lowpass reconstruction filters to generate signals  $S_i'(t)$  and  $S_q'(t)$ . These are then used to modulate a quadrature carrier pair as follows,

$$\text{OQPSK}(t) = S_i'(t)\cos(w_0 t) + S_q'(t)\sin(w_0 t) \quad (2.4)$$

where  $w_0$  is the radian carrier frequency.

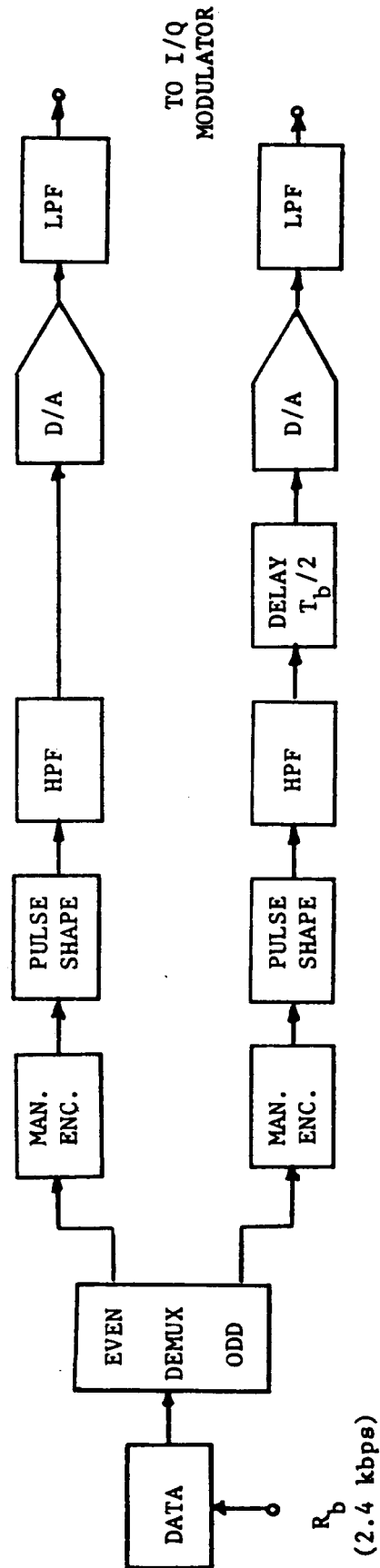


FIGURE 2.1 TCT MANCHESTER BASEBAND PROCESSING



### 2.1.2 Demodulator

The demodulator configuration of the previous TCT study was an IF arrangement which employed analog techniques. This study is considered to be the next stage in the TCT demodulator development since it employs digital baseband I/Q signal processing. The baseband approach is particularly attractive because its low data rate makes possible the extensive use of various DSP techniques. Many signal processing chips are commercially available, and could be utilized in this low data rate environment. This should reduce the complexity of TCT transceiver hardware as well as result in an implementation that is well suited to custom IC fabrication.

The demodulator configuration investigated was derived from that suggested by Davarian [2]. Figure 2.2 illustrates the digital Manchester based TCT demodulator.

The received signal at the demodulator consists of the pilot tone and OQPSK data signal, corrupted by multipath fading, along with a thermal noise component. This signal can be expressed as follows,

$$\begin{aligned} r(t) = & aX_t \cos(w_0 t + Y_t) \\ & + A/\sqrt{2} Si(t)W_t \cos(w_0 t + Y_t) \\ & + A/\sqrt{2} Sq(t)X_t \sin(w_0 t + Y_t) \\ & + Ni(t)\cos(w_0 t) + Nq(t)\sin(w_0 t) \end{aligned} \tag{2.5}$$

The first term of eqn.(2.5) represents the pilot term, the second and third terms correspond to the OQPSK signal, while the remaining terms are attributed to the thermal noise.  $X_t$  and  $Y_t$  are random variables which describe the amplitude and phase variations used to model the multipath fading effects [2].

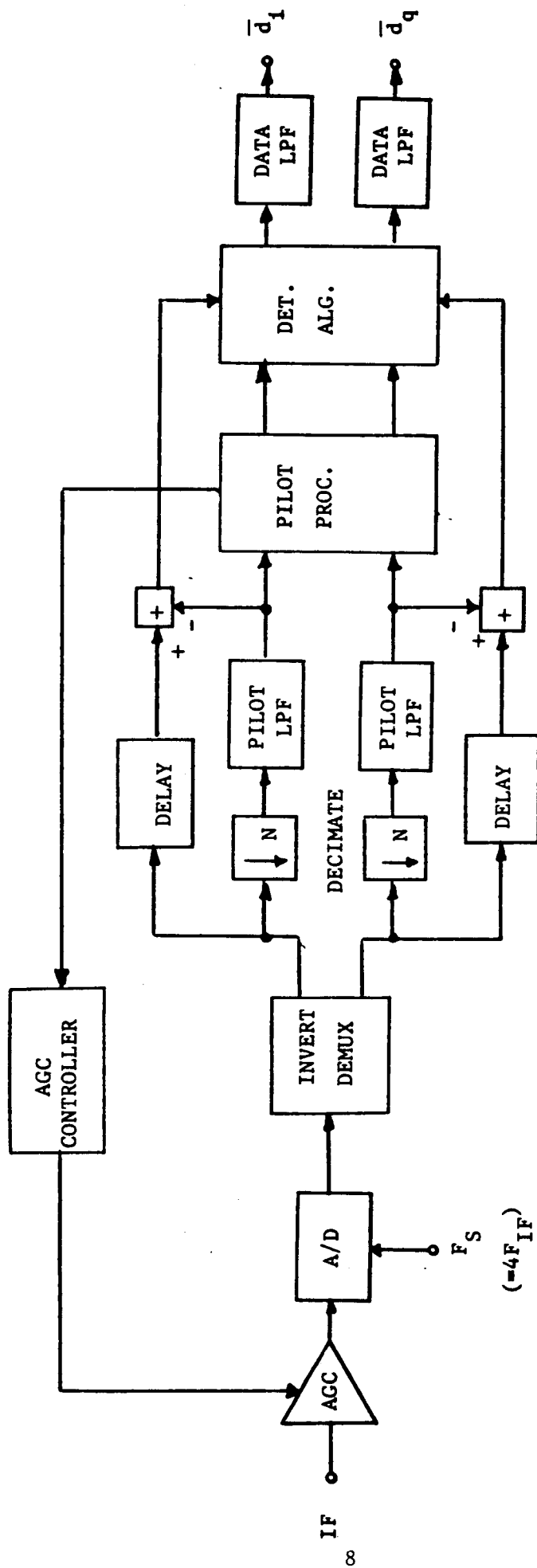


FIGURE 2.2 DIGITAL MTCT DEMODULATOR

The received signal is first passed through a bandpass filter and the AGC amplifier before it is translated to baseband, where the majority of the processing will take place. The bandpass filter is used to reduce the composite input signal strength and excess noise bandwidth. The translation to baseband is performed by mixing the received signal with quadrature sinusoids operating at the IF frequency. In this way the inphase (I) and quadrature (Q) signals necessary for baseband processing are generated.

The I and Q components of the received pilot are recovered by passing the two streams through a filter which has a passband equivalent to the fading bandwidth [1]. In parallel with this operation, the I and Q signals are also fed to a delay buffer which compensates for the overall pilot processing time. The delayed signals will eventually be utilized in conjunction with the appropriately processed pilot I and Q signals, to obtain an estimate of the transmitted data.

The received signal is corrupted by channel perturbations and for the link considered, these perturbations are induced by additive white gaussian noise and multipath fading. Hence, the recovered pilot signal will have impressed upon it amplitude and phase related information about the fading. The task of the pilot processing section is to extract this information from the recovered pilot prior to data detection. A linear TCT pilot processor that was considered previously produces an output with an amplitude component which is the reciprocal of the input pilot amplitude. This method necessitates a squaring and division operation. The processing scheme employed here uses I/Q hardlimiting in a similar fashion to that proposed earlier by Davarian[6]. This has two advantages: it removes the fading amplitude component from the recovered pilot and it simplifies the arithmetic processing requirements. The I/Q hardlimiting is performed by taking the arctangent of  $Q_p/I_p$ , recall (2.5),

$$\hat{\varphi} = \tan^{-1} \left[ \frac{aX_t \cos(\Omega t + \theta_0 - Y_t)}{aX_t \sin(\Omega t + \theta_0 - Y_t)} \right] = (\Omega t + \theta_0 - Y_t) \quad (2.6)$$

where  $\theta_0$  and  $\Omega t$  are residual system phase and frequency offsets. It can be

seen that the amplitude fading has been removed and that the output of the arctangent function is an estimate of the phase perturbation process. This output is then passed on to the detection algorithm. Since data detection is a phase comparison process the pilot amplitude is not strictly required. The long term data sideband amplitude variations can be handled using an AGC loop with a control signal as given below. Faster variations can be addressed by maintaining a sufficient processing signal-to-noise ratio to meet the system performance requirements at low absolute input levels, however, this is probably only realistic for Rician fading channels.

The detection section of the demodulator performs the simultaneous operations of data recovery and the removal of channel phase perturbations. The output of the arctangent function is converted to sine and cosine terms which act as coherent phase references. The detection algorithm can be expressed as follows,

$$Z_I = I_D C + Q_D S \quad (2.7a)$$

$$Z_Q = Q_D C - I_D S \quad (2.7b)$$

where

$$C = 2\cos(\Psi), \quad S = 2\sin(\Psi)$$

and  $\Psi$  is as given in 2.6.  $I_D$  and  $Q_D$  are the outputs of the delay buffers from which the inphase and quadrature components of the recovered pilot,  $I_p$  and  $Q_p$ , have been removed, see Figure 2.2. This is accomplished by the action of the adders immediately following the delay buffers. Signals  $Z_I$  and  $Z_Q$  are then passed on to integrate-and-dump filters to produce estimates of the transmitted data.

An AGC control signal can be derived by taking advantage of the pilot and data detection processors. For example, the amplitude variations on the inphase pilot component can be obtained as follows.

$$E = I_p / \cos(\frac{\pi}{2}) \quad (2.8)$$

E can then be compared to a nominal value and suitably lowpass filtered to generate a control signal which will be used to set the gain of the IF AGC amplifier.

## 2.2 Subcarrier TCT

The subcarrier version of the TCT (STCT) modem is, in fact, very similar to the previously described Manchester modem. The main difference between the two is the manner in which the spectral null at d.c., which is necessary for the proper transmission of the pilot tone, is created. The MTCT version relies upon Manchester coding followed by highpass filtering of the shaped data to remove unwanted sideband energy around zero frequency. The STCT method, on the other hand, modulates the shaped data onto a very low frequency subcarrier to redistribute its data sideband energy away from d.c. The resulting frequency spectra of the two methods are similar, as would be expected, however, software simulations indicate that the subcarrier method does provide some advantages, and, hence, warrants attention.

### 2.2.1 Modulator

Two advantages of the subcarrier method are immediately obvious. For one, the modulation allows the arbitrary location of the data sidebands in a symmetric position around d.c. Also, the pulse shaping can then be used to control the low and high-side roll-off of these sidebands, which cannot be done in the case of the Manchester encoded data.

The implementation of this STCT modulator is quite simple, see Figure 2.3. The data bits are split into even and odd streams, bipolar encoded, then pulse-shaped using the same raised-cosine filtering employed in the MTCT modulator. In this case, however, the excess bandwidth fraction must be reduced to 0.4. The shaped data streams then modulate a quadrature subcarrier signal pair operating at a frequency of 960 Hz. This frequency is a submultiple of the data clock, which is very useful from an implementation standpoint since

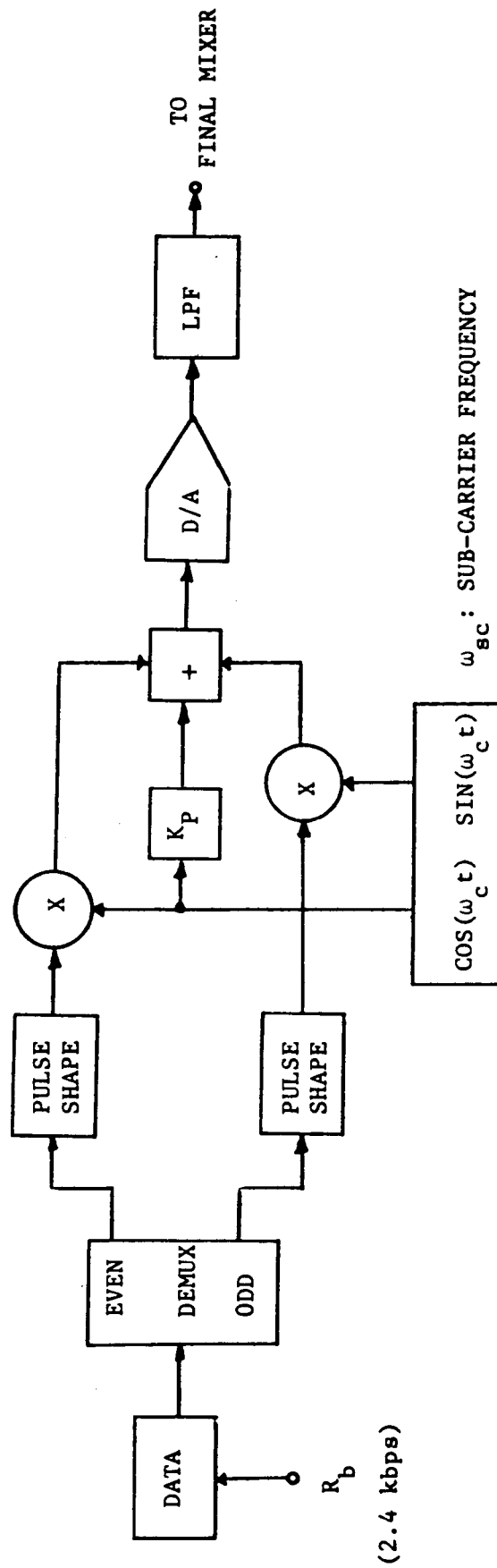


FIGURE 2.3 SUB-CARRIER TCT MODULATOR

the sine and cosine generators are effectively synchronized to this data clock.

It will be shown in section 3.2.1 that this method of frequency redistribution does in fact produce the desired null at d.c. without the need for dual highpass filters and the attendant penalty of added data ISI.

### 2.2.2 Demodulator

The demodulator for the subcarrier version of TCT, illustrated in Figure 2.4, resembles its MTCT counterpart. The difference here is the added remodulation and subcarrier phase estimation functions. Fading compensation and synchronous detection are performed at the subcarrier frequency; hence the need for the remodulation function which modulates the recovered pilot phase onto locally generated sine and cosine subcarrier phase references. These local references are produced by phase-locking a local source to the incoming suppressed subcarrier. It should be noted that the action of the pilot in the synchronous detector is to remove any residual frequency and phase offsets, thus the subcarrier recovery circuits, in theory, only have to align the phase of the local reference to the transmitted one.

This synchronization is performed by a first order phase-locked loop. The outputs of the final data filters serve as a source of the receive phase states. The receive phase states are compared to the known nominal receive data phase states. The angular difference between these two quantities becomes the error signal. The phase-locked loop output is an estimate of the phase difference between the local and the received subcarrier, this is added to the recovered pilot phase angle prior to the remodulation process.

## 3. TCT SYSTEM COMPUTER SIMULATION

The initial investigation of the baseband Tone Calibrated Technique required the development of a software simulation. A simulation was generated which omitted the modelling of any channel perturbations so that the modem performance could be evaluated solely in terms of system parameters.

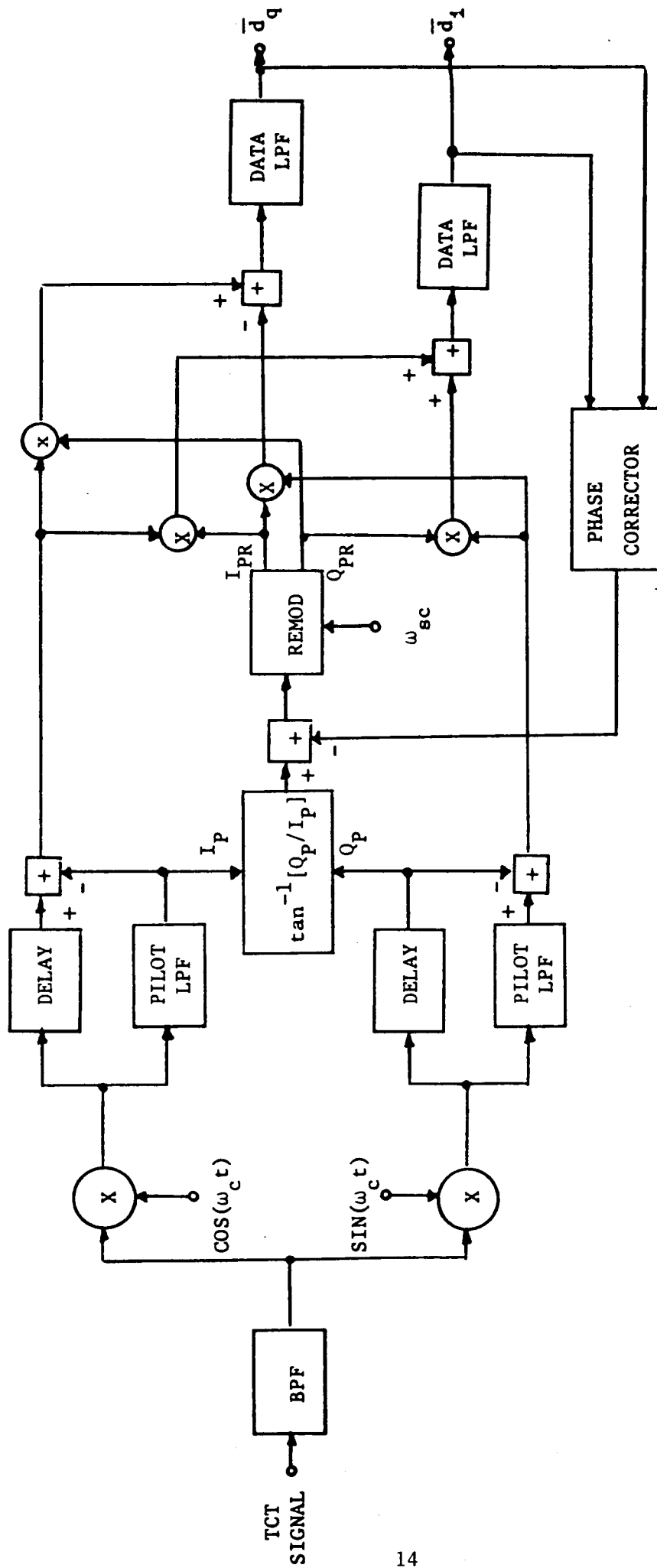


FIGURE 2.4 STCT DEMODULATOR



Subsequent development continued to focus on the signal processing structures of the modem. By concentrating on emulating the elements of the real-time implementation, the simulation effectively became a valuable design tool. The structure of the final design could be fully developed before committing it to hardware, allowing for a relatively smooth implementation. The inclusion of multipath fading and thermal noise to the simulation was not viewed as critical, since the impact of these effects would be examined in the real-time system.

The simulations were written in FORTRAN and interfaced to the Interactive Laboratory System (ILS) digital signal processing software package for purposes of graphical presentation and analysis. In addition, ILS was employed in designing all the required digital filters. Linear phase filters were used throughout to minimize phase distortion and the design algorithm employed was the Remez Exchange Algorithm which produces equiripple in both the passband and stopband. A data eye pattern was generated from a  $2^{10} - 1$  pseudo-random bit sequence and the recovered eye quality was used as an indication of system performance. ILS is commercially available through Signal Technology, Inc.

Appendix I contains a program listing of the MTCT modem simulation described in the next section.

### 3.1 Manchester Encoded TCT

#### 3.1.1 Modulator

The Manchester encoded TCT modulator was first simulated as shown in Figure 2.1, except without the highpass filters. Since no channel modelling was performed, the data was QPSK modulated to 12 kHz, the receiver final IF frequency. The data at IF was represented as a 48 kHz sampled signal, consistent with the demodulator IF sampling frequency.

In order to meet the specified bandwidth requirements, frequency domain raised-cosine pulse-shaping was employed with a Nyquist excess fraction,  $\beta$ , of 0.5 at a data rate of 2.4 kbps. Figures 3.1(a) and 3.1(b) show respectively the baseband data eye and the data eye spectrum. The pulse shape extends over

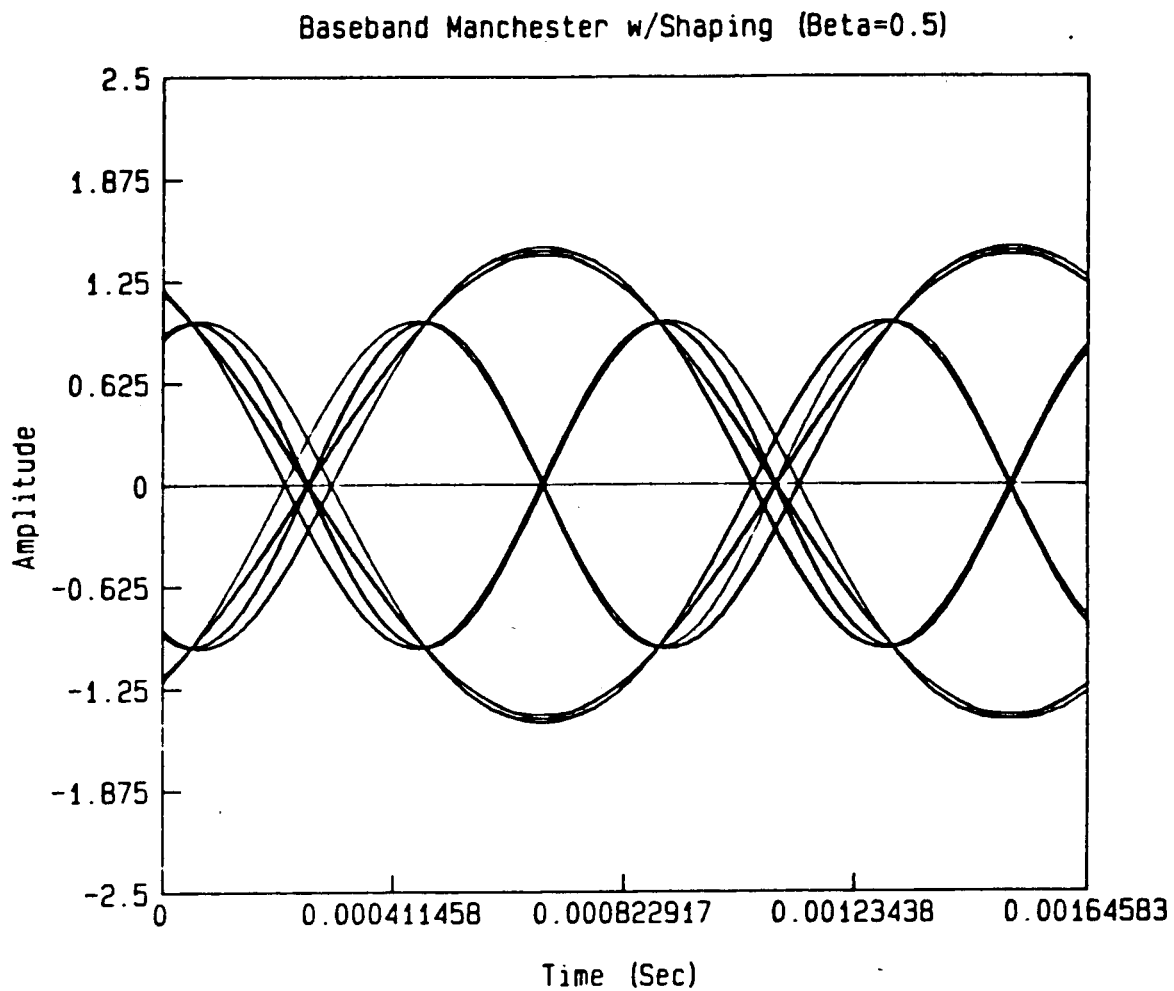


FIGURE 3.1(a) SHAPED MANCHESTER ENCODED DATA, NO HIGHPASS FILTER

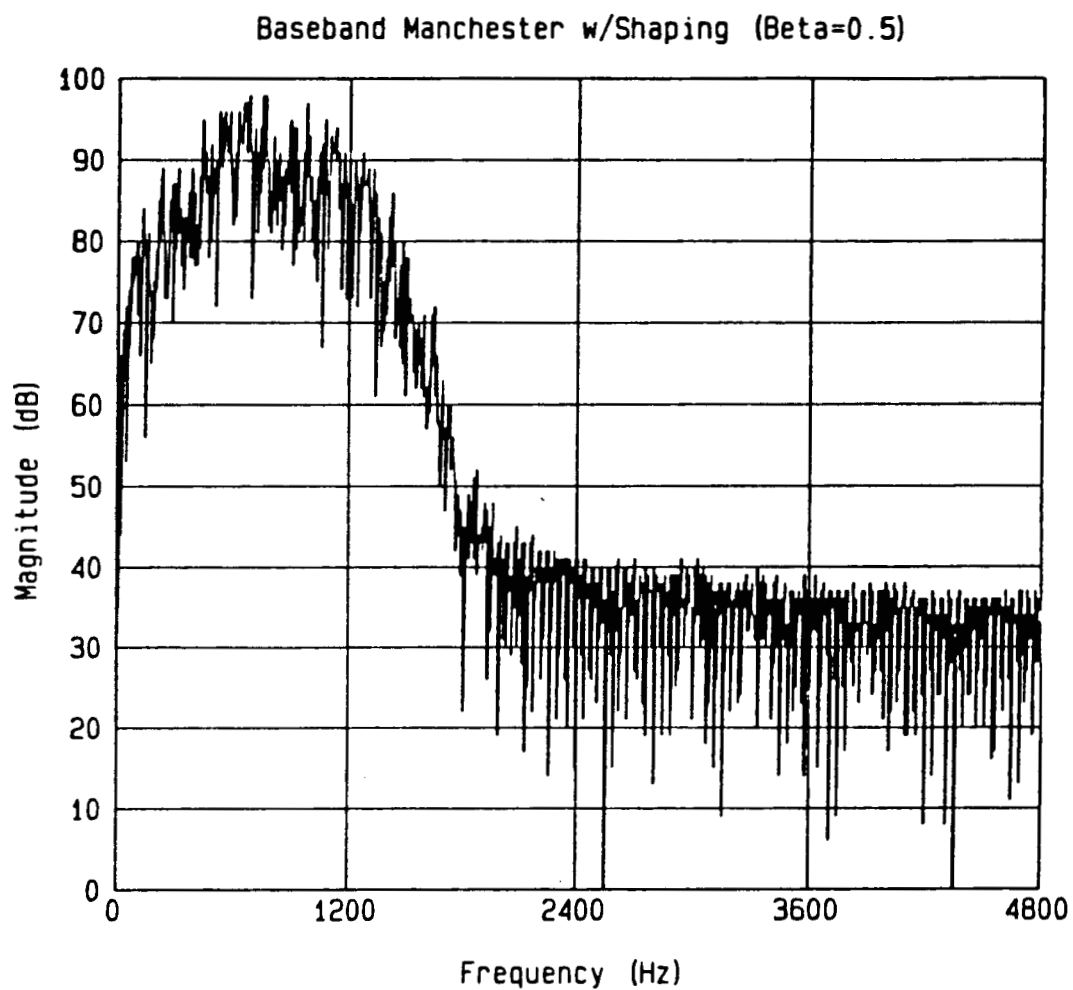


FIGURE 3.1(b) FREQUENCY SPECTRUM OF FIGURE 3.1(a)

eight Manchester bit time periods and provides sufficient spectral occupancy characteristics, i.e. over 40 dB of attenuation at 1.8 kHz from the center frequency, while generating an eye pattern with points of no ISI.

Although the pulse shaping is more than adequate in fulfilling bandwidth constraints, the generation of a zero frequency null is poorly implemented with Manchester encoding alone. A null width of 100 Hz is desired for the insertion of a carrier to track multipath fading characteristics. If a highpass filter is employed, a significant null can be created, see Figure 3.2(b); however, Figure 3.2(a) shows the distortion introduced by filtering out low frequency components from the data.

A 91 tap highpass filter is used initially as a control to establish a frequency response with a very sharp cut-off and no passband ripple. The 91 tap filter has a 3 dB point at 150 Hz and functions at the baseband processing rate of 9.6 kHz. The degradation due to this filter is approximately 16% as measured by comparing the size of the eye closure to the nominal opening. A 45 tap highpass filter design is also examined, since the longer length filter cannot be implemented in the proposed processor for the real-time system. The frequency response of this filter has a half dB ripple in the passband, a 3 dB point at 150 Hz and less attenuation in the stopband. Figures 3.3(a) and 3.3(b) show the data eye pattern and the data frequency spectrum. Both diagrams appear quite close to the 91 tap control filter simulation results, with the 45 tap filter eye pattern showing slightly more ISI.

The final step in the modulator simulation involved generating a 48 kHz sampled signal from the 9.6 kHz baseband process for the demodulator IF input requirements. This was done in two steps. First, the 9.6 kHz signal was zero insertion upsampled by a factor of 1:5 to a sampling frequency of 48 kHz. The spectrum of this signal is shown in Figure 3.4(a). The baseband spectrum is centered at multiples of 9.6 kHz. The high frequency images are then removed by lowpass filtering, yielding the spectrum of Figure 3.4(b). Although the baseband images are still recognizable, they represent negligible energy compared to the data spectrum. The 48 kHz sampled baseband data is then QPSK modulated to the 12 kHz demodulator IF frequency.

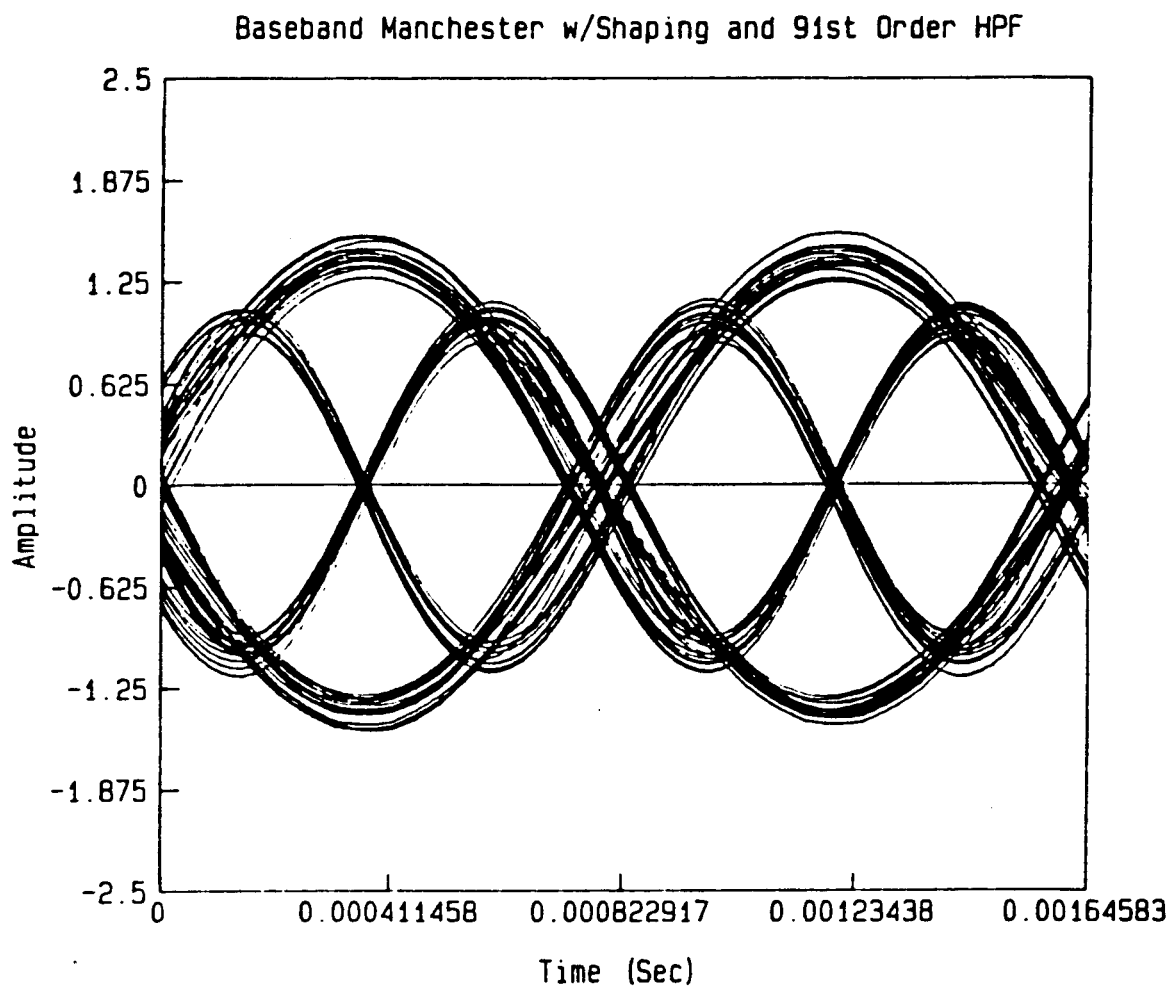


FIGURE 3.2(a) SHAPED MANCHESTER ENCODED DATA WITH HIGHPASS FILTERING  
(91st ORDER)

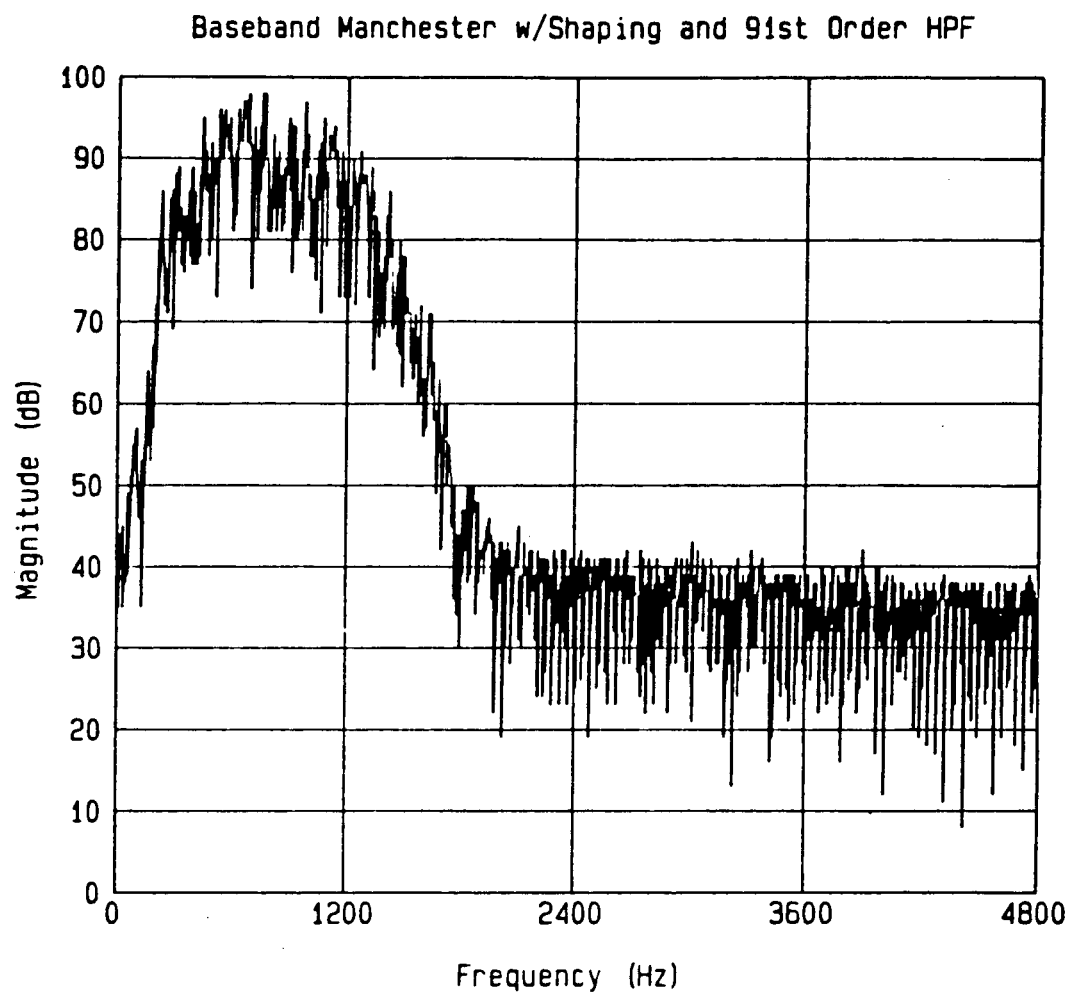


FIGURE 3.2(b) FREQUENCY SPECTRUM OF FIGURE 3.2(a)

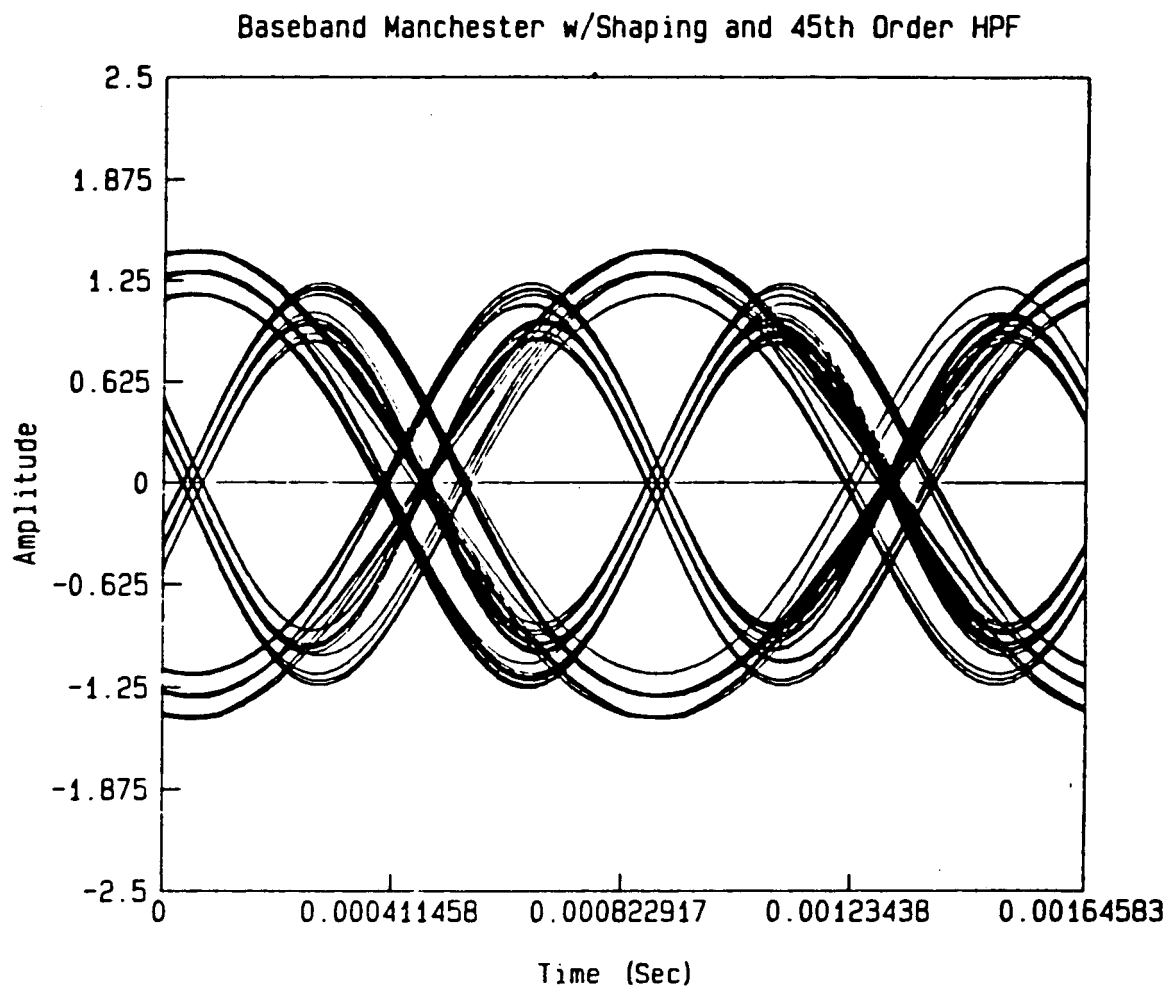


FIGURE 3.3(a) SHAPED MANCHESTER ENCODED DATA WITH HIGHPASS FILTERING  
(45th ORDER)

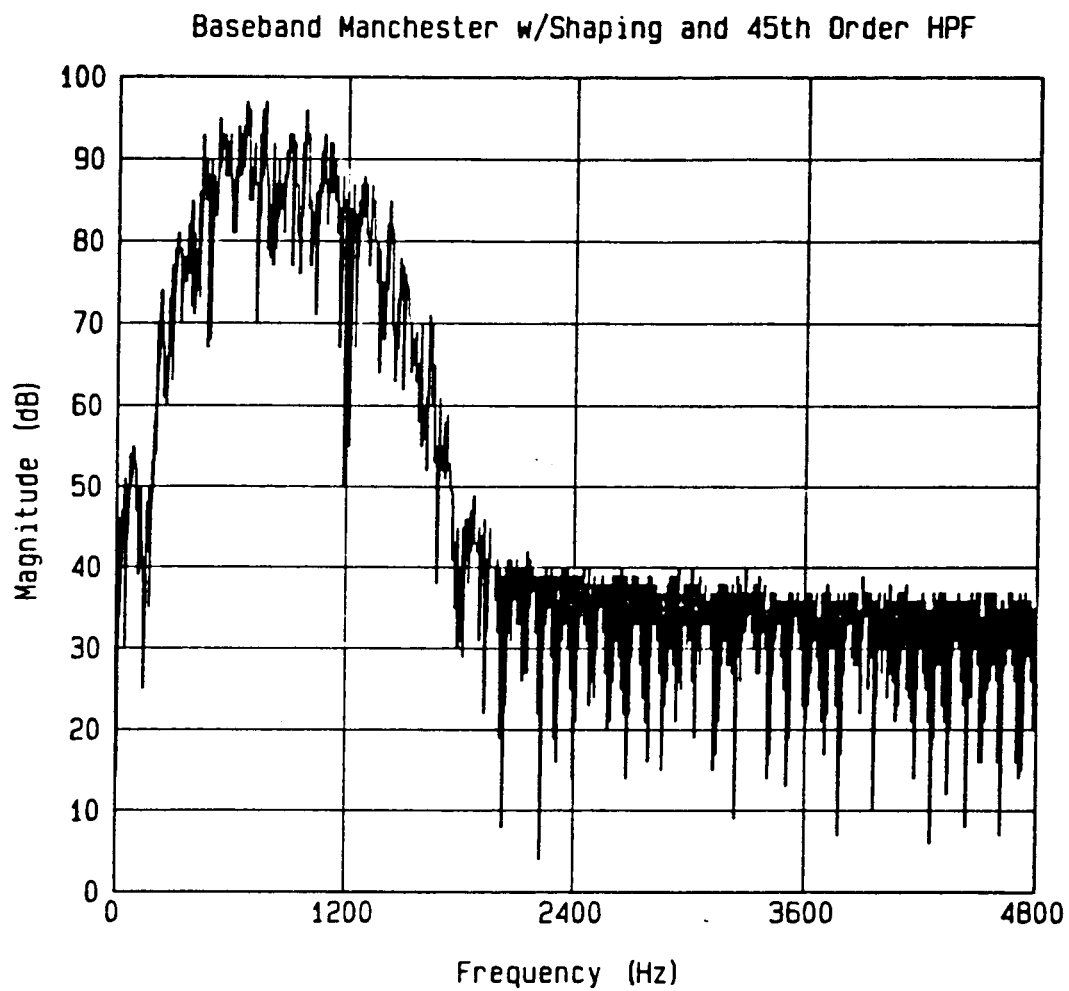


FIGURE 3.3(b) FREQUENCY SPECTRUM OF FIGURE 3.3(a)



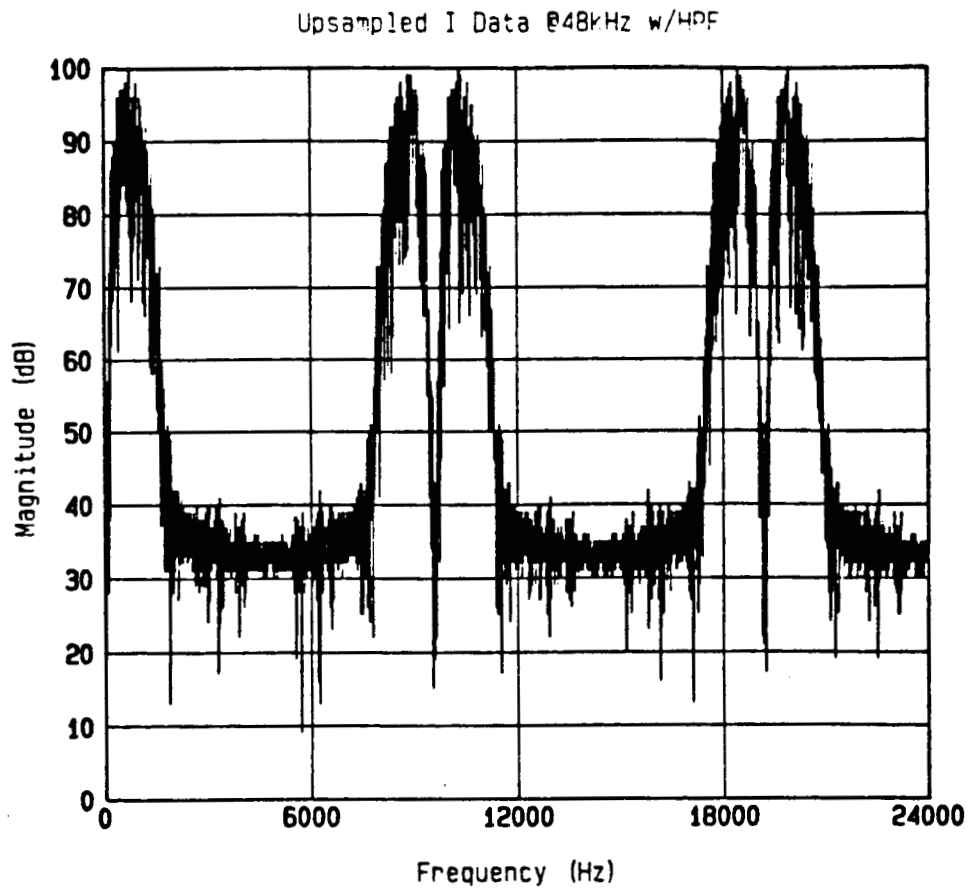


FIGURE 3.4(a) SPECTRUM OF 1:5 UPSAMPLED 9.6 kHz  
INPHASE SIGNAL

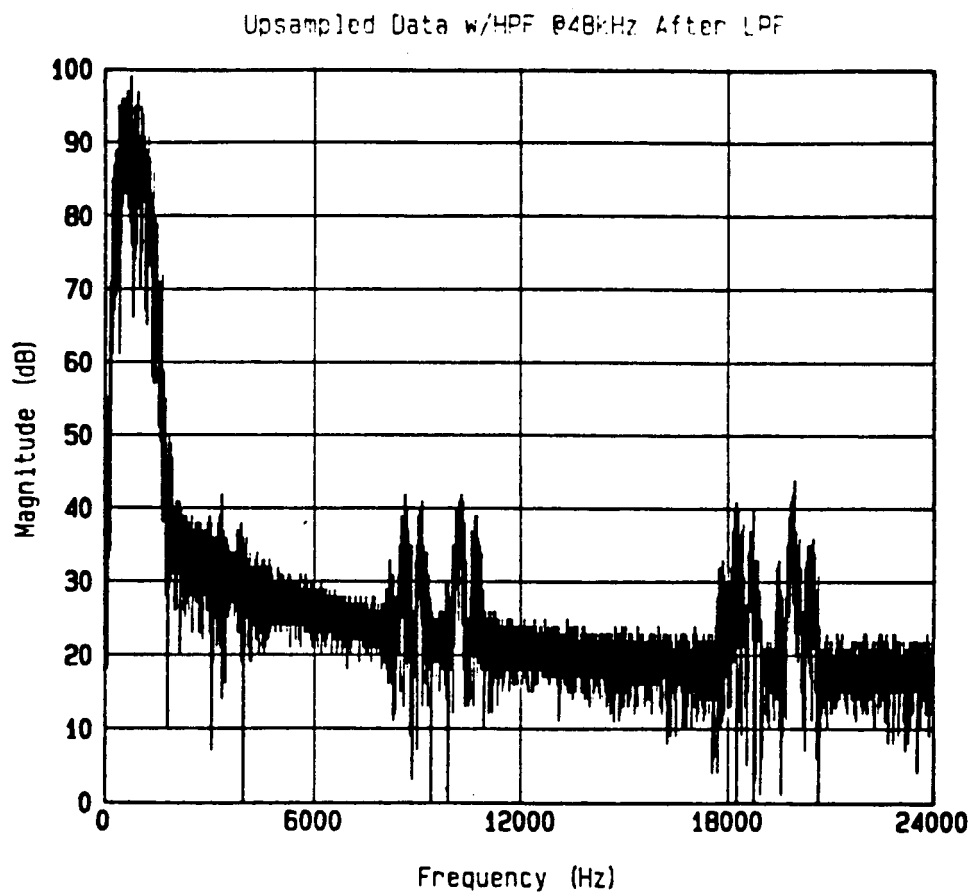


FIGURE 3.4(b) LOWPASS FILTERED SPECTRUM OF  
1:5 UPSAMPLED 9.6 kHz INPHASE SIGNAL

### 3.1.2 Demodulator

The demodulator of Figure 3.5 was simulated in modular form with each block representing a different signal processing task that could be tested separately for functionality. A specific effort was made during simulation development to exercise system parameters for optimization of the real-time demodulator design. The efficiencies of multi-rate processing were emphasized.

Since the analog-to-digital converter is operating at a sampling frequency of 48 kHz, four times the IF frequency, all adjacent samples are in time quadrature. Translation to baseband is achieved by multiplying with a square wave a four sample period which, in the digital domain, is spectrally identical to a sinusoid of the same frequency. Every other sample of the baseband signal is then separated into in-phase and quadrature components sampled at a 24 kHz rate. Each component is divided into two streams. One undergoes pilot recovery and the other is delay equalized to match the lowpass filtering in the pilot processing.

The advantage of lowering the sampling frequencies clearly results in reduced digital processing cost. Decimation in the signal paths leading to the pilot recovery lowpass filters significantly eases both the processing burden and the digital filter design. A decimation ratio of 5:1 causes no aliasing and improves the lowpass cut-off to sampling frequency ratio, allowing a much lower order filter implementation. The recovered pilot streams are subtracted off from the delayed data and estimates of the channel phase perturbations are passed to the detection algorithm. The pilot processing and data detection are simulated essentially as described in section 2.1.2; however, since there are different processing rates in the demodulator, some method must be chosen to handle the different rate boundaries. A full interpolation to reconstruct the lower rate signal is expensive in processing cost. A zero-order hold is simple to implement but has a poor frequency characteristic as higher frequency images roll off with only a  $\sin(x)/x$  response. As a result, a first-order hold is implemented providing much better attenuation of images. The processing cost is relatively low requiring only a one sample delay in the pilot path and a linear interpolation.

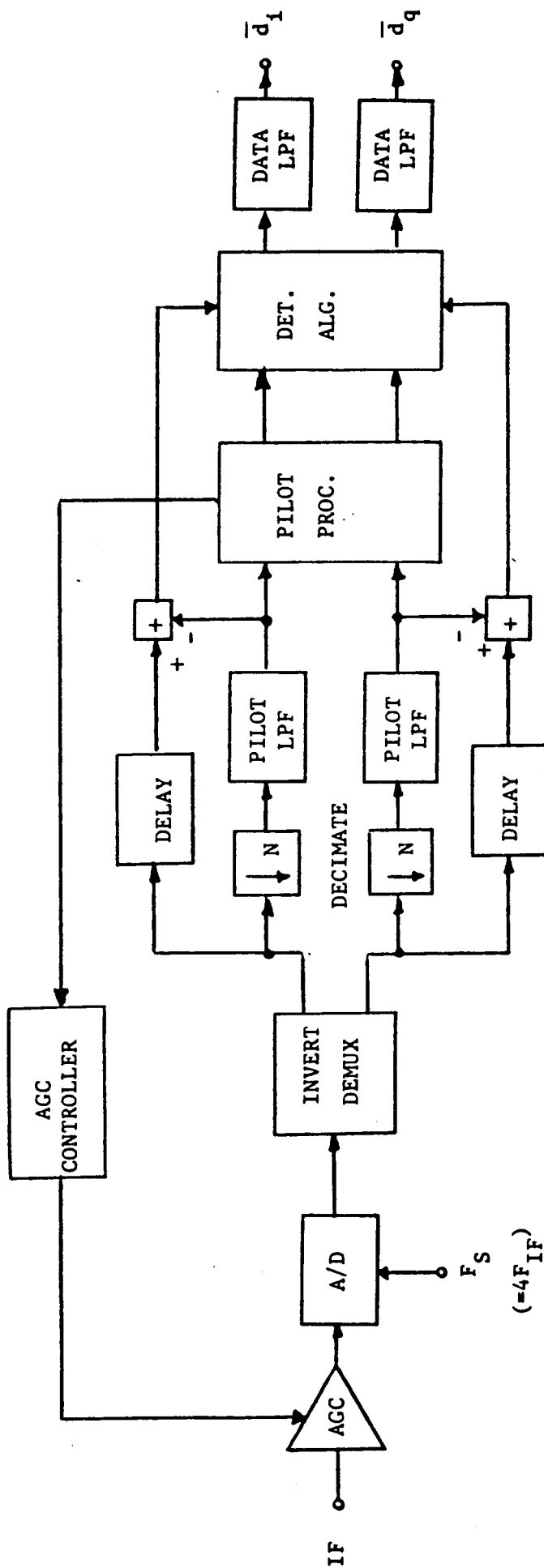


FIGURE 3.5 DIGITAL MTCT DEMODULATOR

The results of the simulated demodulator output are compared with respect to two performance criteria : recovered pilot quality and data eye quality. Two different pilot recovery filters were used with 3 dB cut-off frequencies representing maximum desired pilot bandwidth, 150 Hz, and minimum usable bandwidth, 80 Hz. The filter characteristics are summarized in table 3.1. The transmitted pilot level is 0.5 and the nominal eye opening is 2.0.

Figure 3.6(a) shows the recovered pilot using the 150 Hz lowpass filter without the benefit of a highpass filter on the transmit end. The large variation from the transmitted level is due solely to data modulation of the pilot. If the pilot of Figure 3.7(a) is compared to this one, a significant decrease in variance is observed. Although data energy continues to leak into the pilot recovery channel, the amount is greatly reduced at the transmit side by the Manchester encoding. The large reduction in pilot variance suggests that there is little data energy remaining in the frequency band below 80 Hz.

Figures 3.6(b) and 3.7(b) show the eye diagrams corresponding to the recovered pilots. Both show the ISI introduced by the demodulator at the detection algorithm. The eye pattern generated from the system employing the 150 Hz recovery filter is particularly bad due to the large data modulation induced variance.

With the addition of a transmit highpass filter, the demodulator recovered pilots more closely approach the transmitted levels. Figure 3.8(a) shows the pilot obtained with the 150 Hz recovery filter and Figure 3.9(a) shows the pilot recovered through the 80 Hz lowpass filter. Both pilots exhibit considerable improvement due to the inclusion of the highpass filter.

The respective data eye patterns are shown in Figures 3.8(b) and 3.9(b). A comparison between the detected eye diagram obtained with the 80 Hz recovery filter and the transmitted data eyes of Figures 3.2(a) and 3.3(a) indicates negligible distortion introduced by the demodulator.

A configuration which was not simulated but potentially results in reduced ISI at the demodulator consists of transmit highpass filtering at a frequency of 80 Hz and also employing an 80 Hz pilot recovery filter. This

TABLE 3.1

PILOT RECOVERY FILTER CHARACTERISTICS

150 Hz Pilot Recovery Filter:

3 dB bandwidth	150 Hz
40 dB bandwidth	300 Hz
passband ripple	0.1 dB
sampling frequency	4.8 kHz

80 Hz Pilot Recovery Filter:

3 dB bandwidth	80 Hz
40 dB bandwidth	160 Hz
passband ripple	0.1 dB
sampling frequency	4.8 kHz

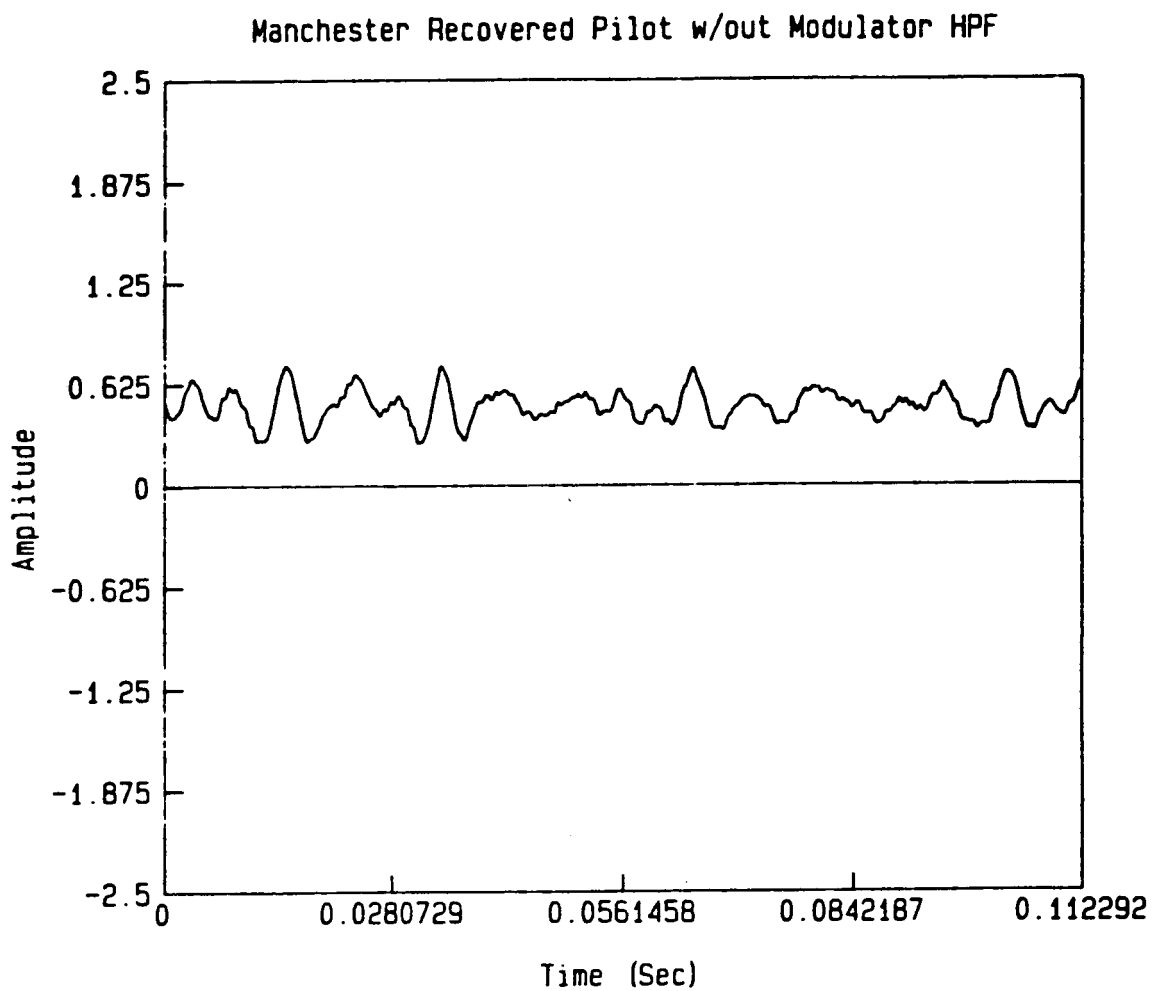


FIGURE 3.6(a) MTCT RECOVERED PILOT, 150 HZ PILOT  
LOWPASS FILTER, NO TRANSMIT HIGHPASS FILTER

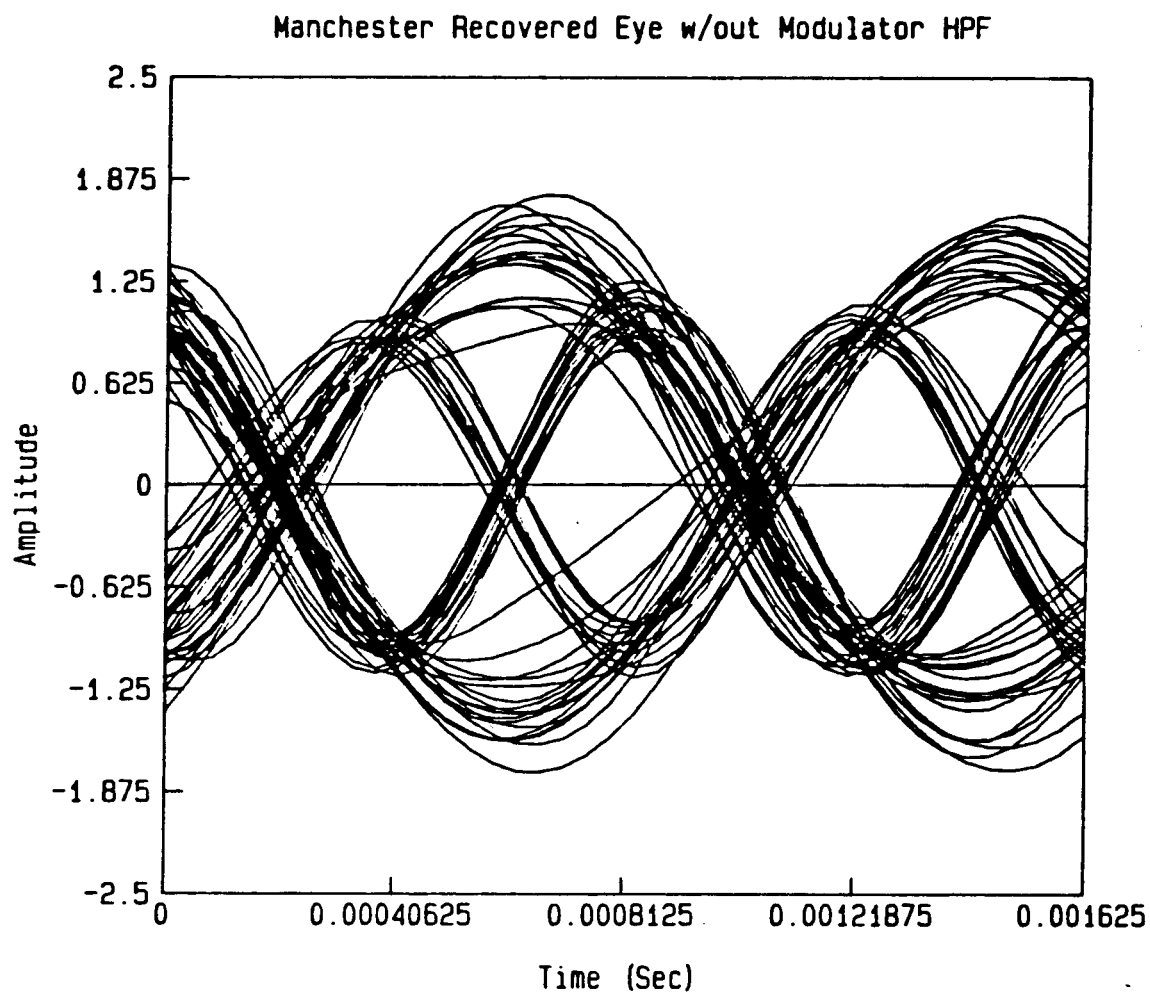


FIGURE 3.6 (b) MTCT RECOVERED EYE FOR THE PILOT OF  
FIGURE 3.6 (a)



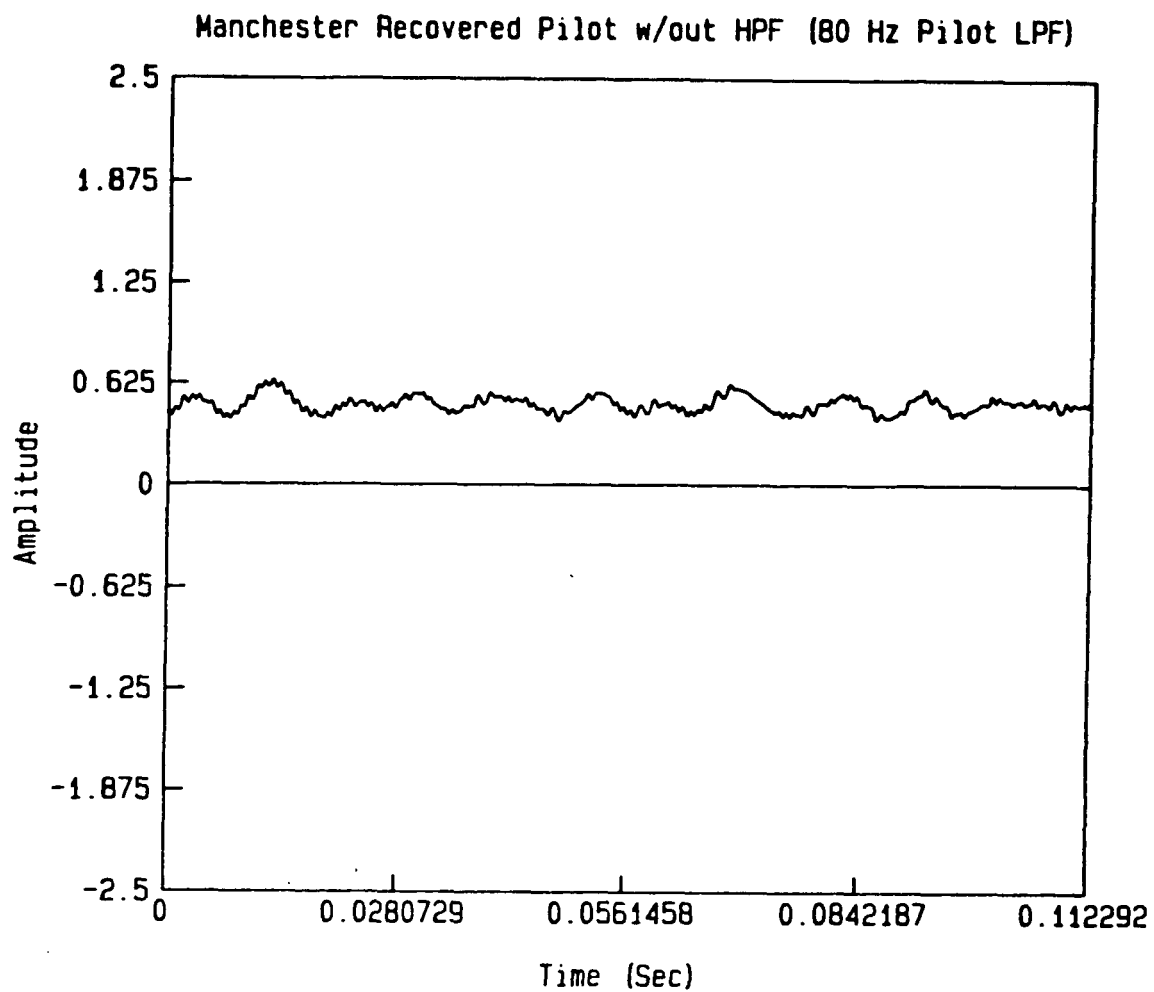


FIGURE 3.7(a) MTCT RECOVERED PILOT, 80 HZ PILOT LOWPASS  
FILTER, NO TRANSMIT HIGHPASS FILTER

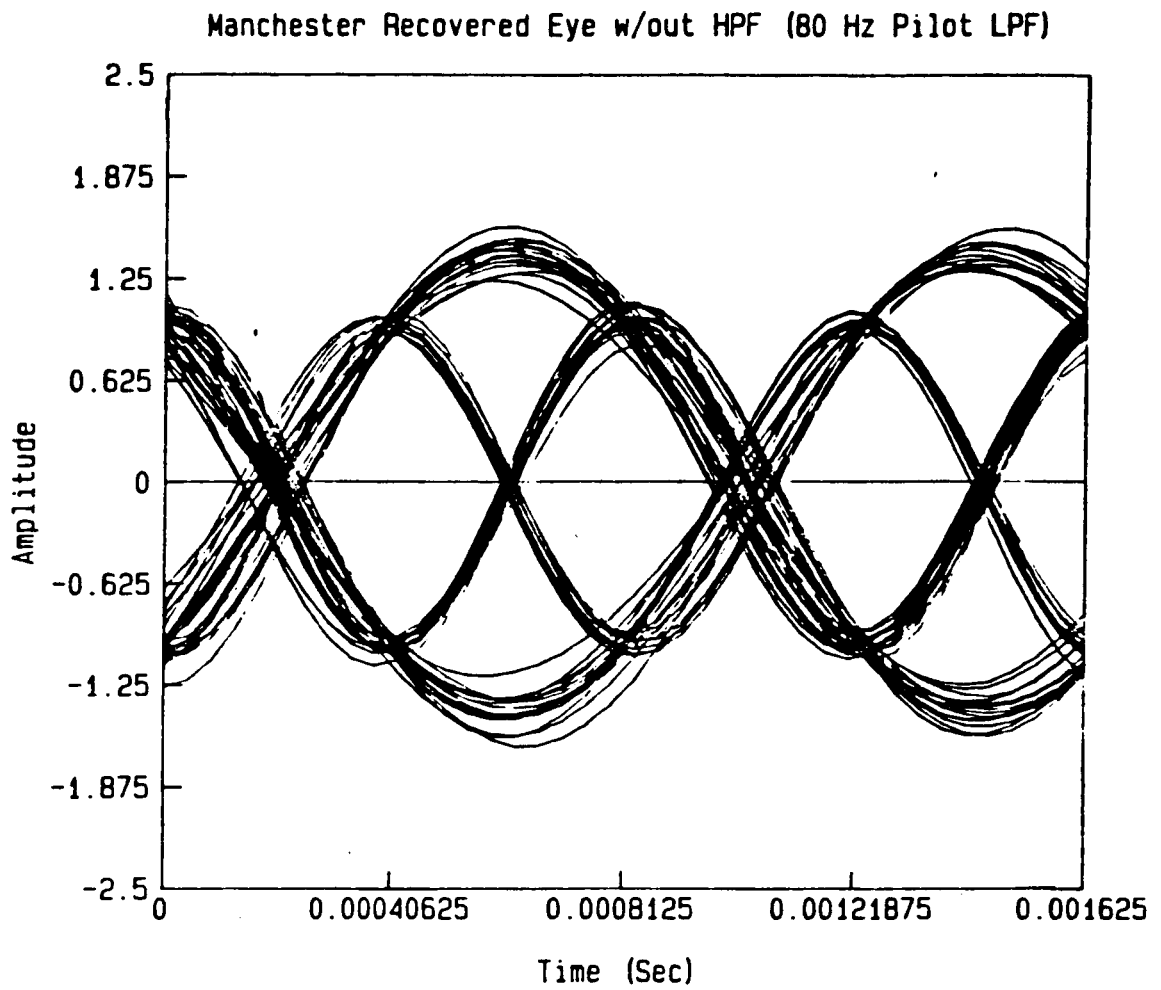


FIGURE 3.7(b) MTCT RECOVERED EYE FOR THE PILOT OF FIGURE 3.7(a)

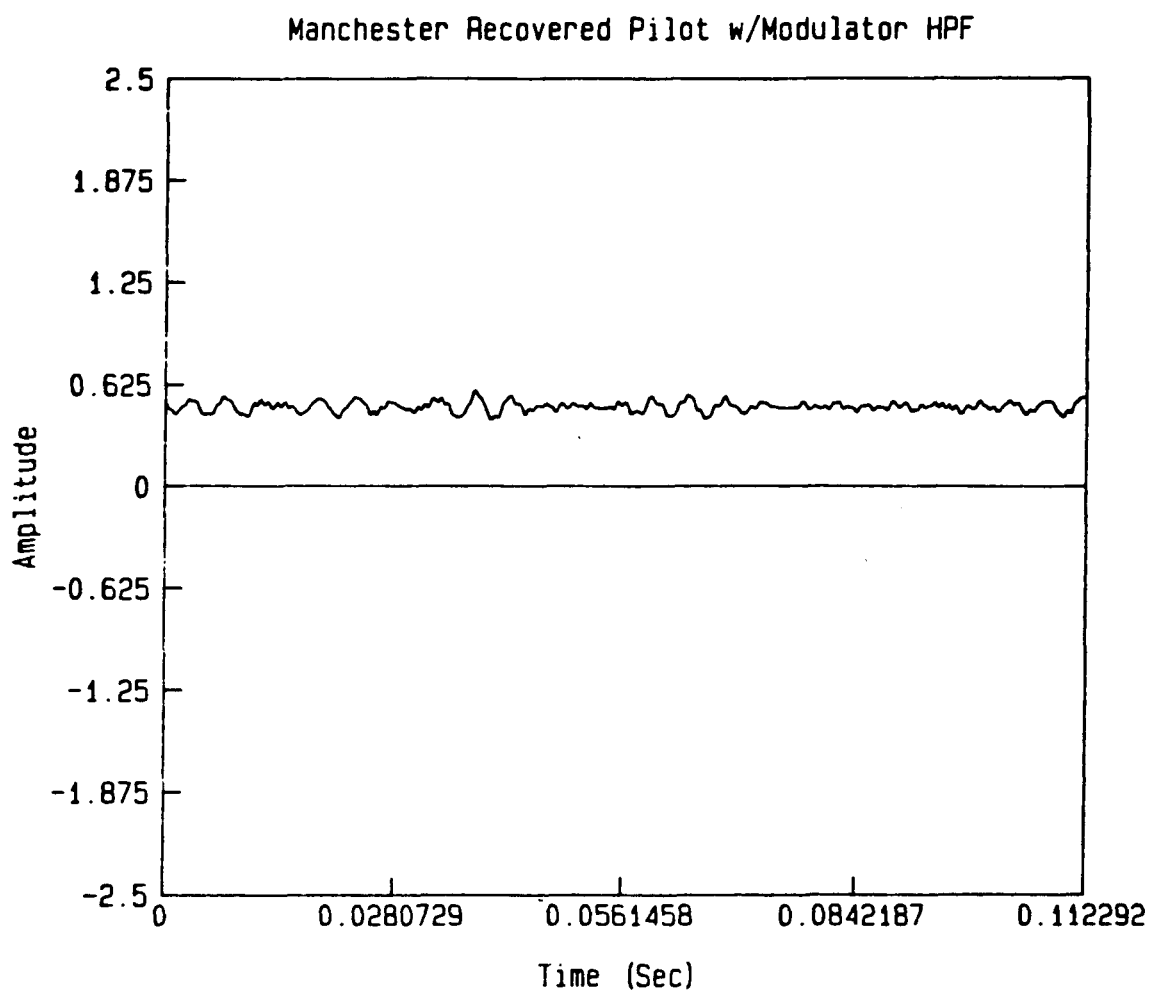


FIGURE 3.8(a) MTCT RECOVERED PILOT, 150 HZ LOWPASS FILTER AND  
TRANSMIT HIGHPASS FILTER

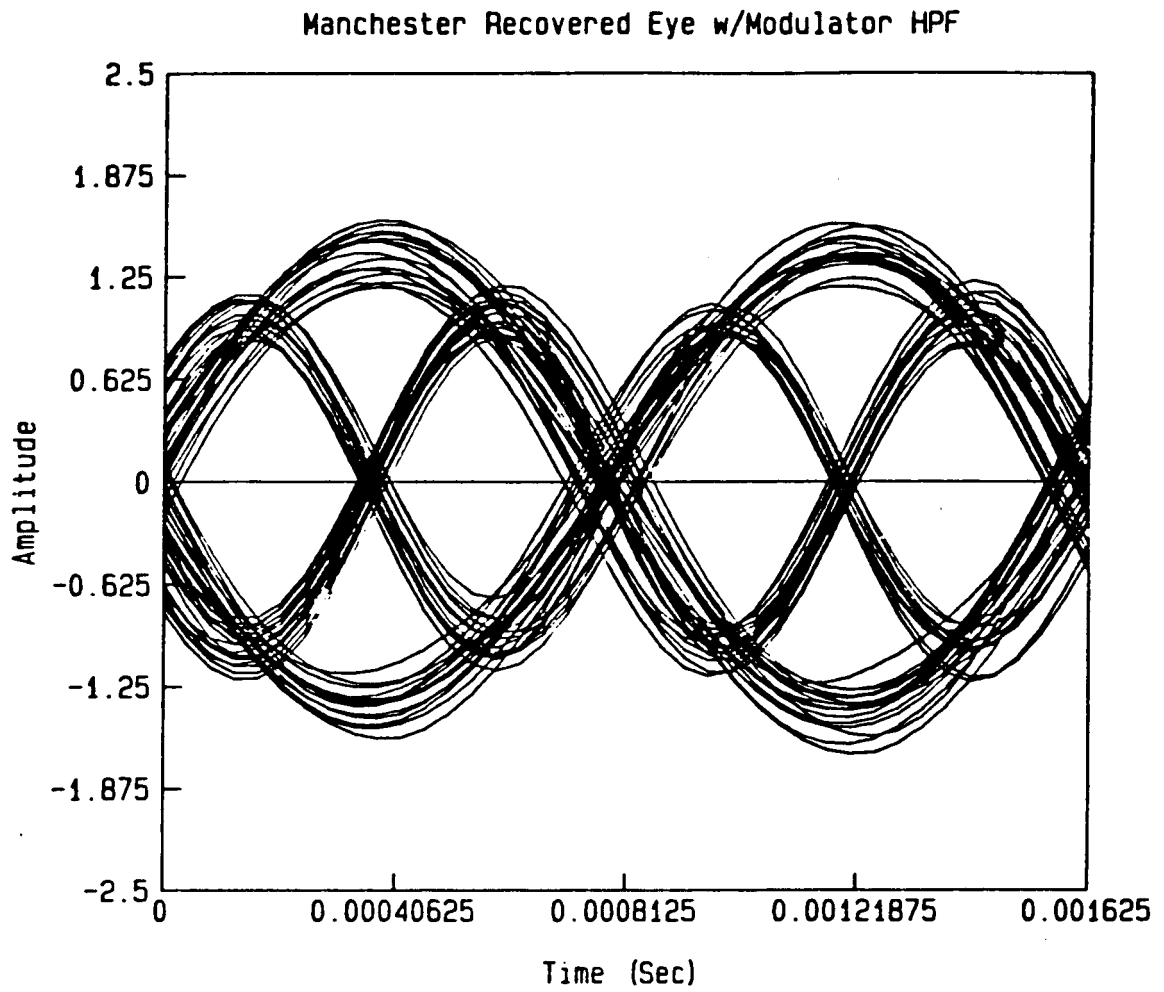


FIGURE 3.8(b) MTCT RECOVERED EYE FOR THE PILOT OF FIGURE 3.8(a)

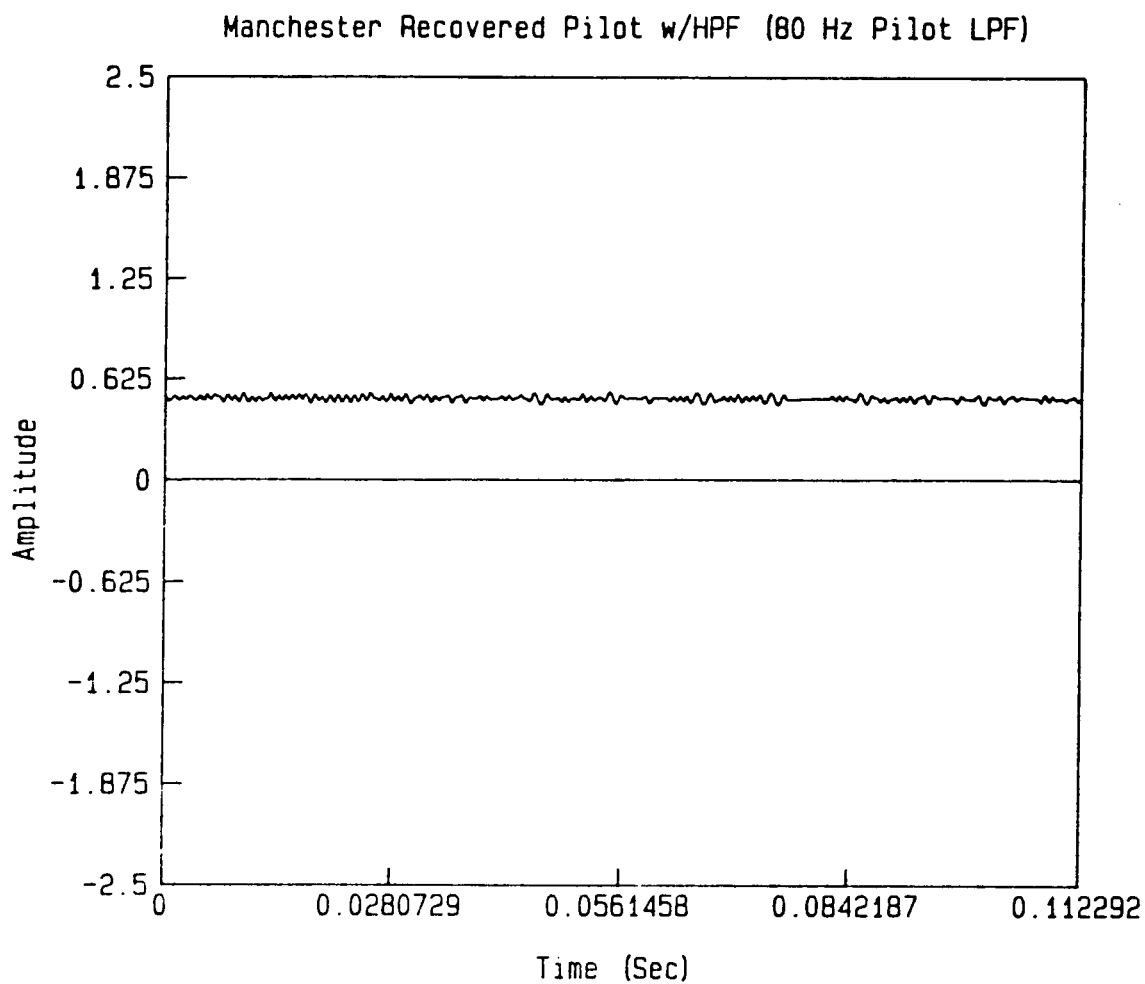


FIGURE 3.9(a) MTCT RECOVERED PILOT, 80 HZ LOWPASS FILTER AND  
HIGHPASS TRANSMIT FILTER

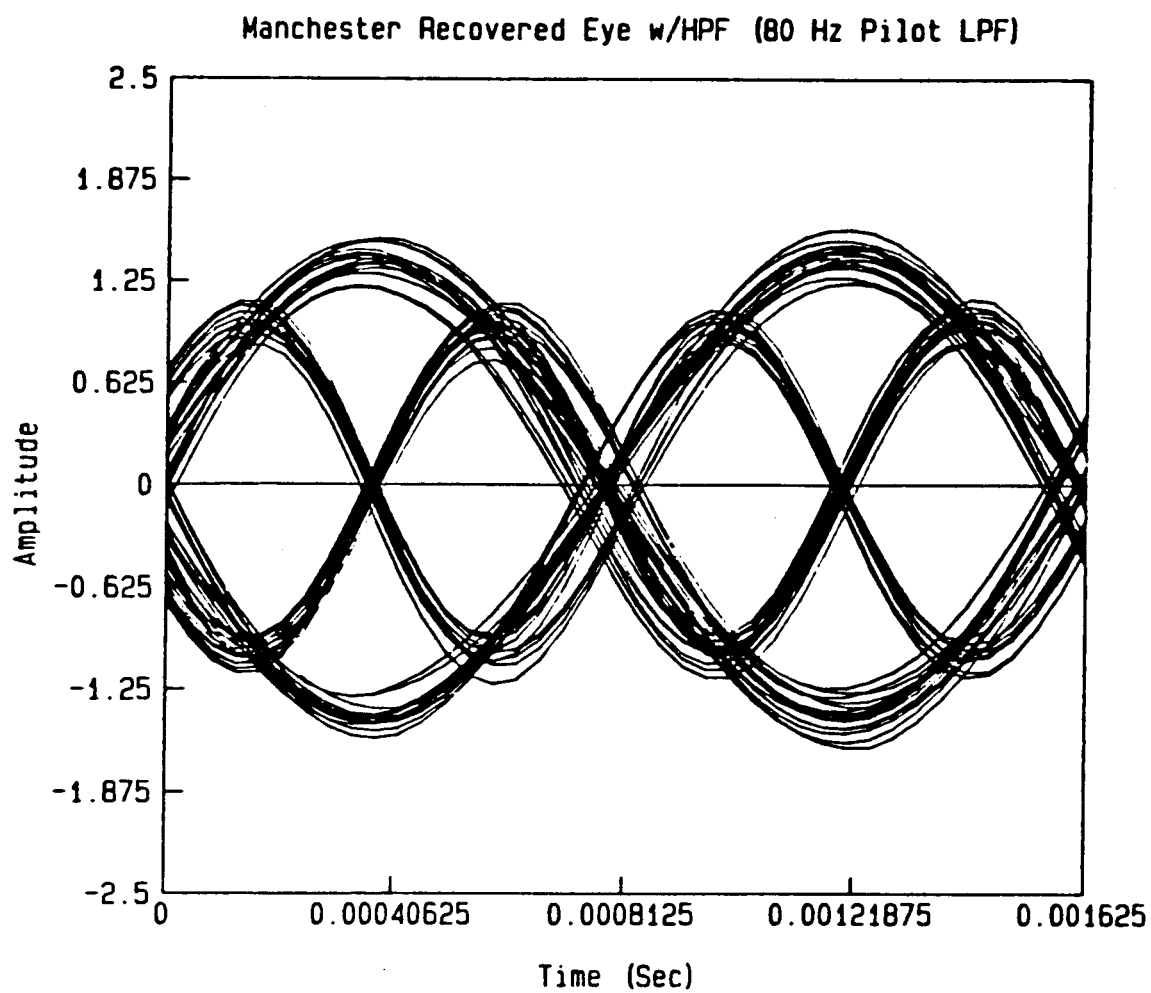


FIGURE 3.9(b) MTCT RECOVERED EYE FOR THE PILOT OF FIGURE 3.9(a)

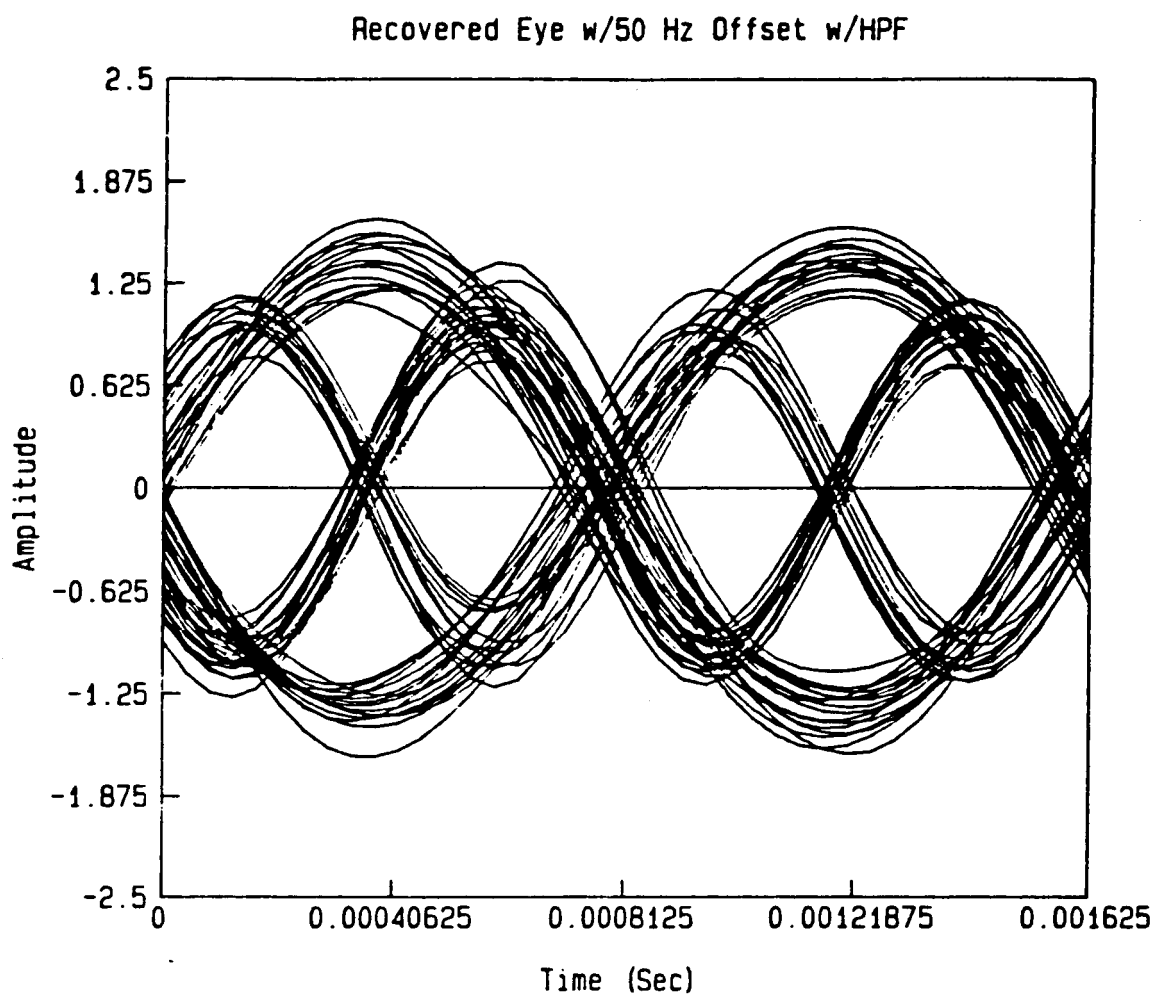


FIGURE 3.10(a) MTCT RECOVERED EYE FOR A 50 HZ FREQUENCY OFFSET AND  
A 150 HZ PILOT LOWPASS FILTER

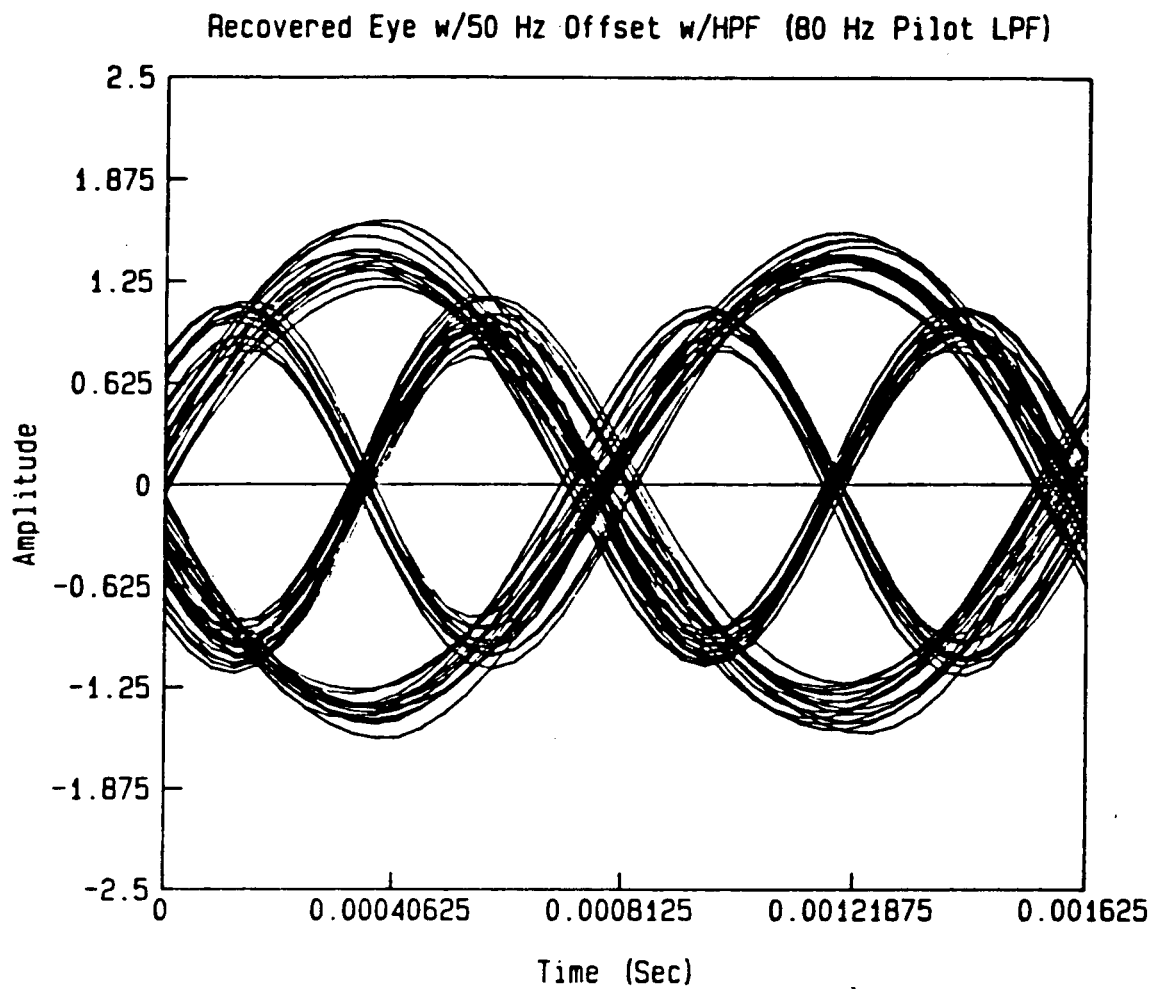


FIGURE 3.10(b) MTCT RECOVERED EYE FOR A 50 HZ FREQUENCY OFFSET AND  
AN 80 HZ LOWPASS FILTER



would result in a recovered pilot with slightly more variance than the one of Figure 3.9(a); however, the data eye should display less ISI since a significant part of the data spectrum (80-150 Hz) is left intact.

The demodulator performance was also examined after introducing a 50 Hz frequency offset to the modulated signal. Figures 3.10(a-b) show the detected data eyes obtained with the 150 Hz and 80 Hz lowpass filters respectively. The performance exhibited by the MTCT configuration indicates the ability to correct for a considerable frequency displacement.

### 3.2 Subcarrier TCT

#### 3.2.1 Modulator

As an alternative to the MTCT transmitter, the STCT modulator of Figure 2.4 was fully simulated. The STCT modulator relies on the subcarrier modulation to create the spectral null for pilot insertion; therefore, its design is considerably simplified by omitting both the Manchester encoding and the highpass filters. Frequency domain raised-cosine pulse shaping is again used in the STCT system. An excess bandwidth fraction of 0.4 is employed for pulse shaping and a 960 Hz subcarrier, for QPSK modulation in order to meet the single-sided spectral occupancy requirement of a 40 dB attenuation at 1.8 kHz from the center frequency. The modulator output is a 48 kHz sampled stream translated to a 12 kHz IF.

The baseband data eye is shown in Figure 3.11(a) and 3.11(b) shows the corresponding spectrum. Figure 3.12 shows both the QPSK modulated data onto the subcarrier and the spectral null. Since no energy has been removed from the data signal, unlike the MTCT system, the transmitted data is free of ISI.

#### 3.2.2 Demodulator

The translation process from IF to baseband in the STCT demodulator was changed slightly from the one used in the MTCT system. Demodulation was achieved without a local reference by taking advantage of the fact that the data bandwidth is small in comparison to the sampling frequency. In the STCT

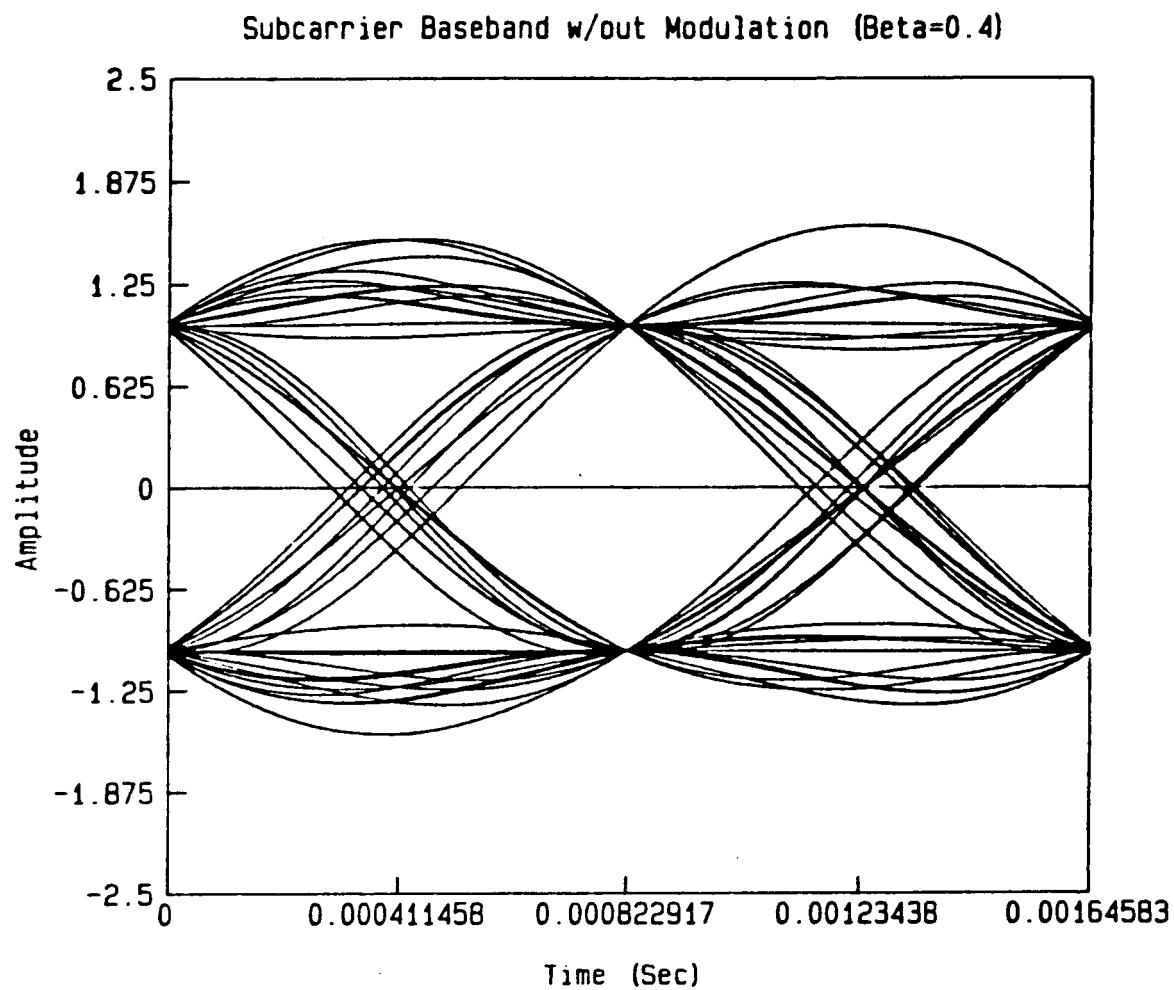


FIGURE 3.11(a) STCT TRANSMIT DATA EYE

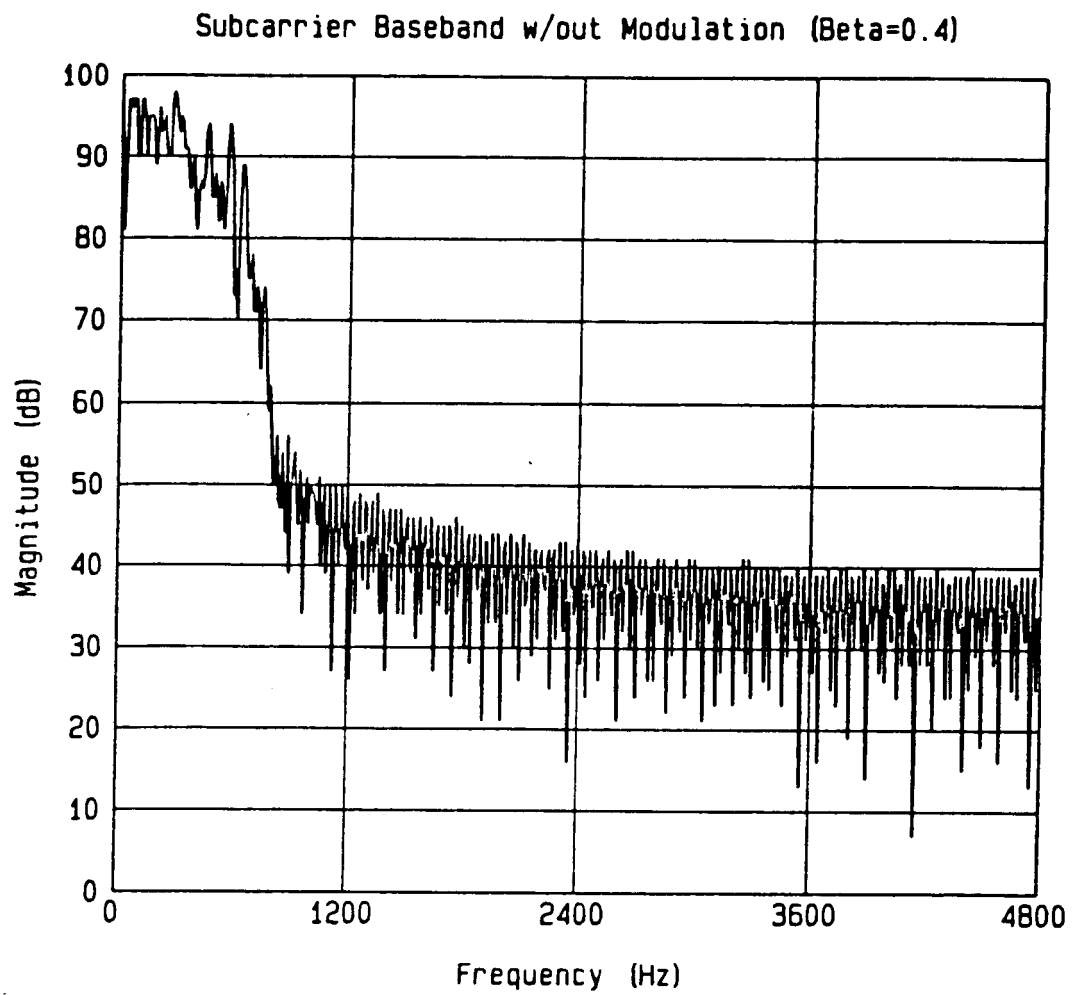


FIGURE 3.11(b) FREQUENCY SPECTRUM OF FIGURE 3.11(a)

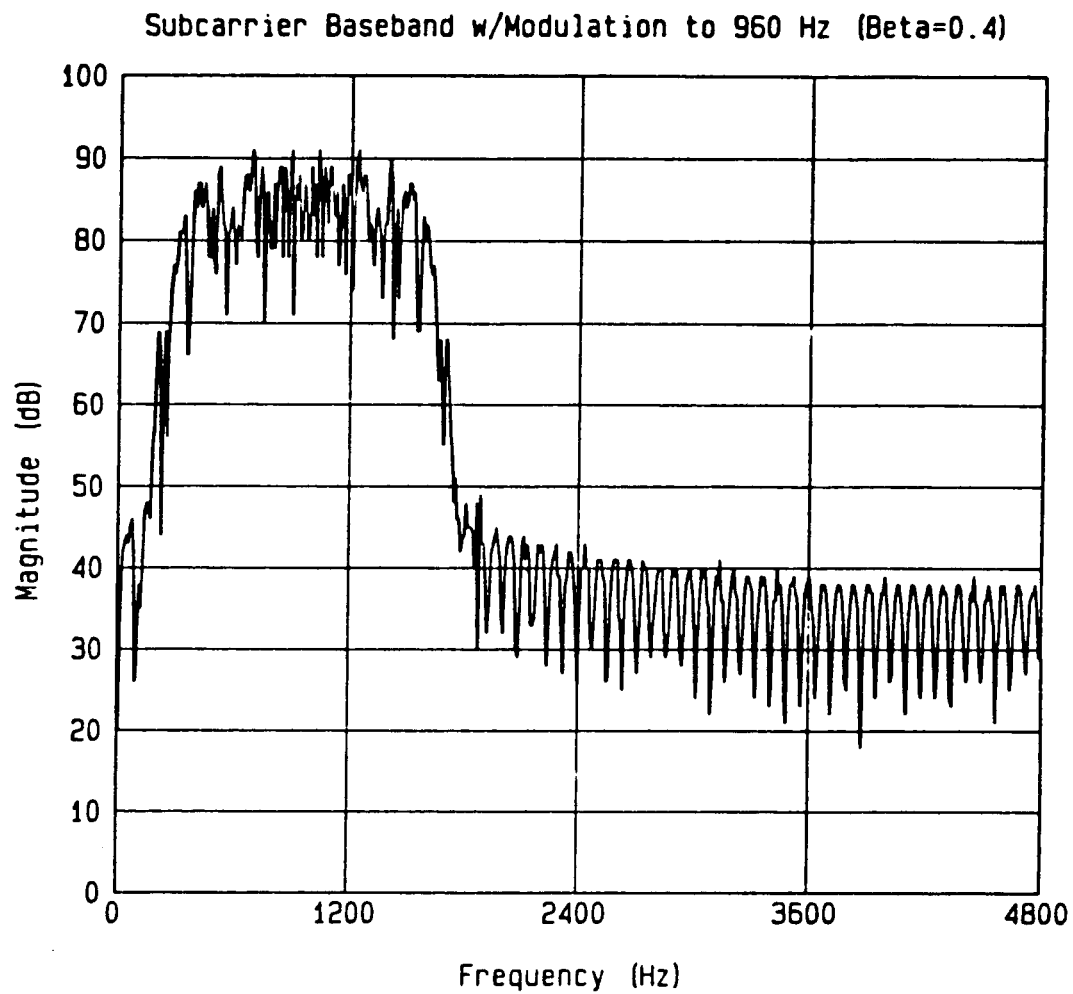


FIGURE 3.12 SUB-CARRIER QPSK FREQUENCY SPECTRUM

simulation, a ratio of 4:1 was employed and adjacent IF input sample pairs were translated to 12 kHz in-phase and quadrature baseband components. Figures 3.13(a-c) detail the demodulation process. A further decimation of 5:1 in the signal paths leading to the pilot recovery lowpass filters was used causing aliasing in the data but not in the pilot. The aliased portion of the spectrum is located in the stopband of the recovery filter and contributes no negative effects, see Figures 3.14(a-b). The final processing rates in the STCT simulation were 12 kHz for the data arms and 2.4 kHz for the pilot channels (these rates can be applied to the MTCT simulation as well).

The results of the subcarrier demodulator simulation are summarized in Figures 3.15(a-b) and 3.16. Figure 3.15(a) shows a recovered pilot with virtually no data modulation corrupting it, resulting in the corresponding recovered eye pattern of Figure 3.15(b) which shows no ISI. A frequency offset test was also performed with the subcarrier simulation. Figure 3.16 shows the recovered data eye which displays noticeable distortion. Some preliminary investigation seemed to indicate that ISI is produced by imperfect cancellation of the frequency offset double term product in the detection algorithm. The distortion introduced by this term is assumed also to be present in the MTCT demodulator.

Table 3.2 compares the recovered pilot variances for both the MTCT and STCT systems. All variances are referenced to the recovered subcarrier pilot variance level.

#### 4. MODEM HARDWARE IMPLEMENTATION

##### 4.1 Manchester Encoded TCT

The Manchester encoded TCT was the method chosen by JPL to be followed through to a hardware realization. Consequently, the MTCT modem is the major topic of this section. To date a stand-alone board that serves as the digital modulator for both the MTCT and STCT systems has been completed and is fully tested and functional. The required RF circuitry for the modulator and demodulator has also been designed and tested. The transmitter RF portion has

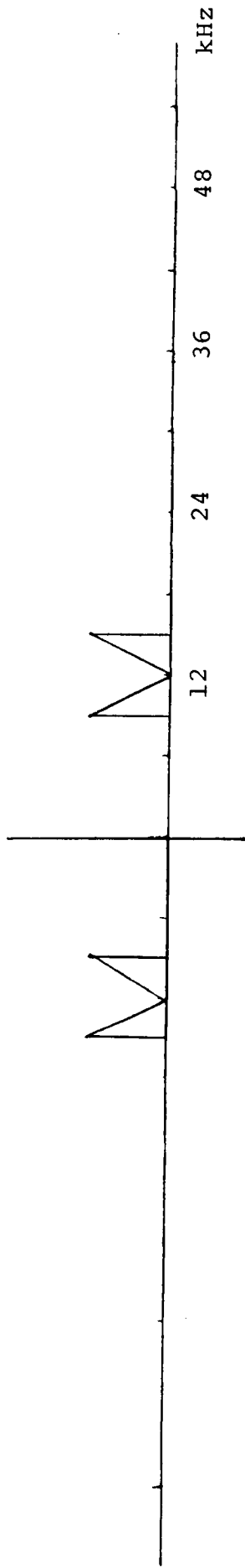


Figure 3.13(a) Analog IF Spectrum

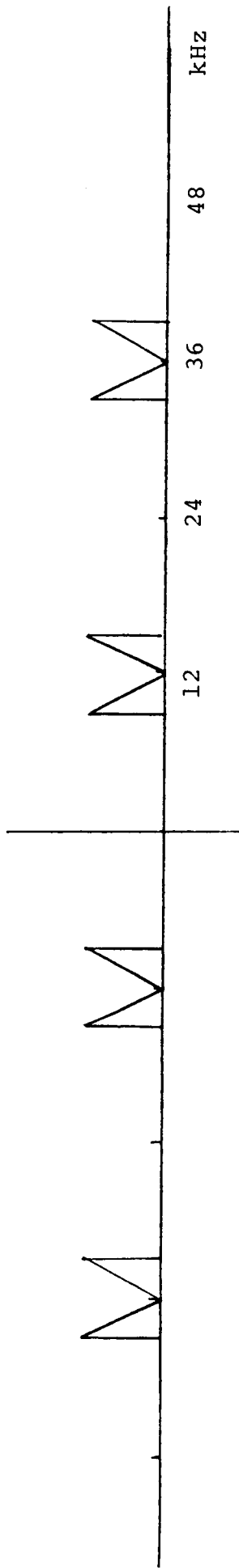


Figure 3.13(b) Spectrum Sampled at 48 kHz

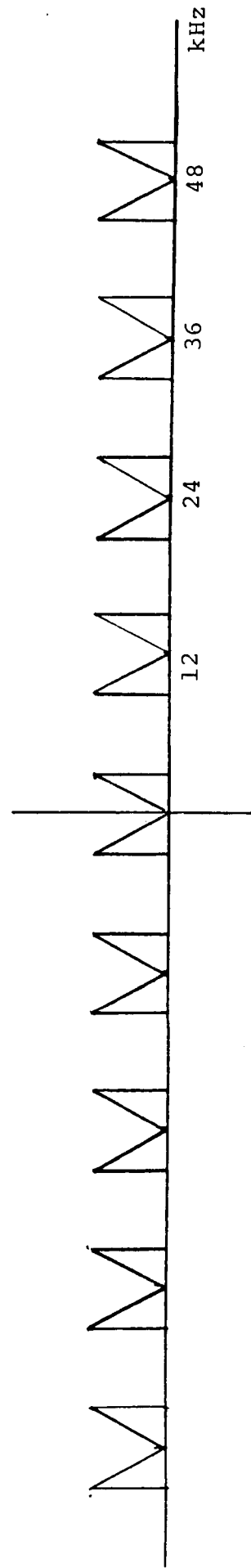


Figure 3.13(c) Demodulated Spectrum Through 4:1 Decimation

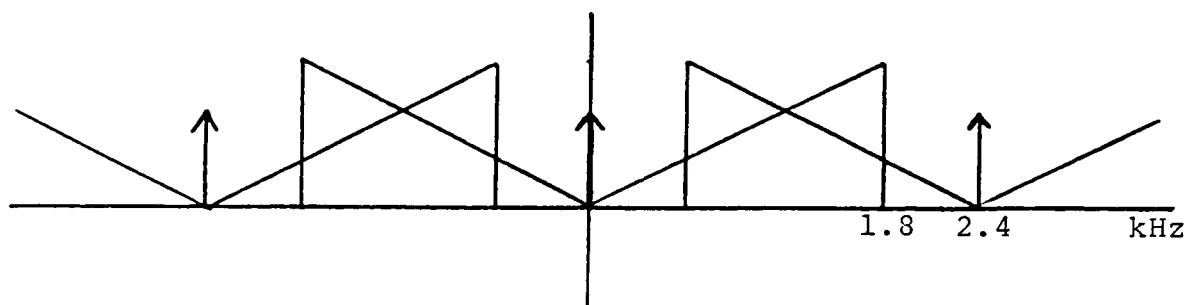


Figure 3.14(a) Aliased Baseband Spectrum

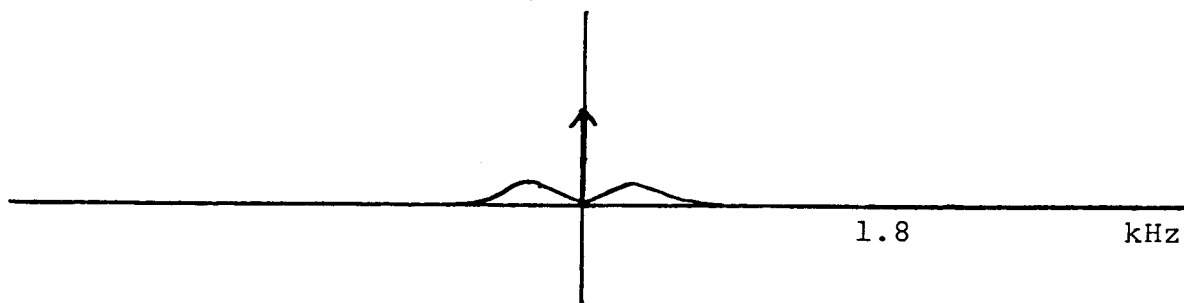


Figure 3.14(b) Recovered Pilot After Lowpass Filtering

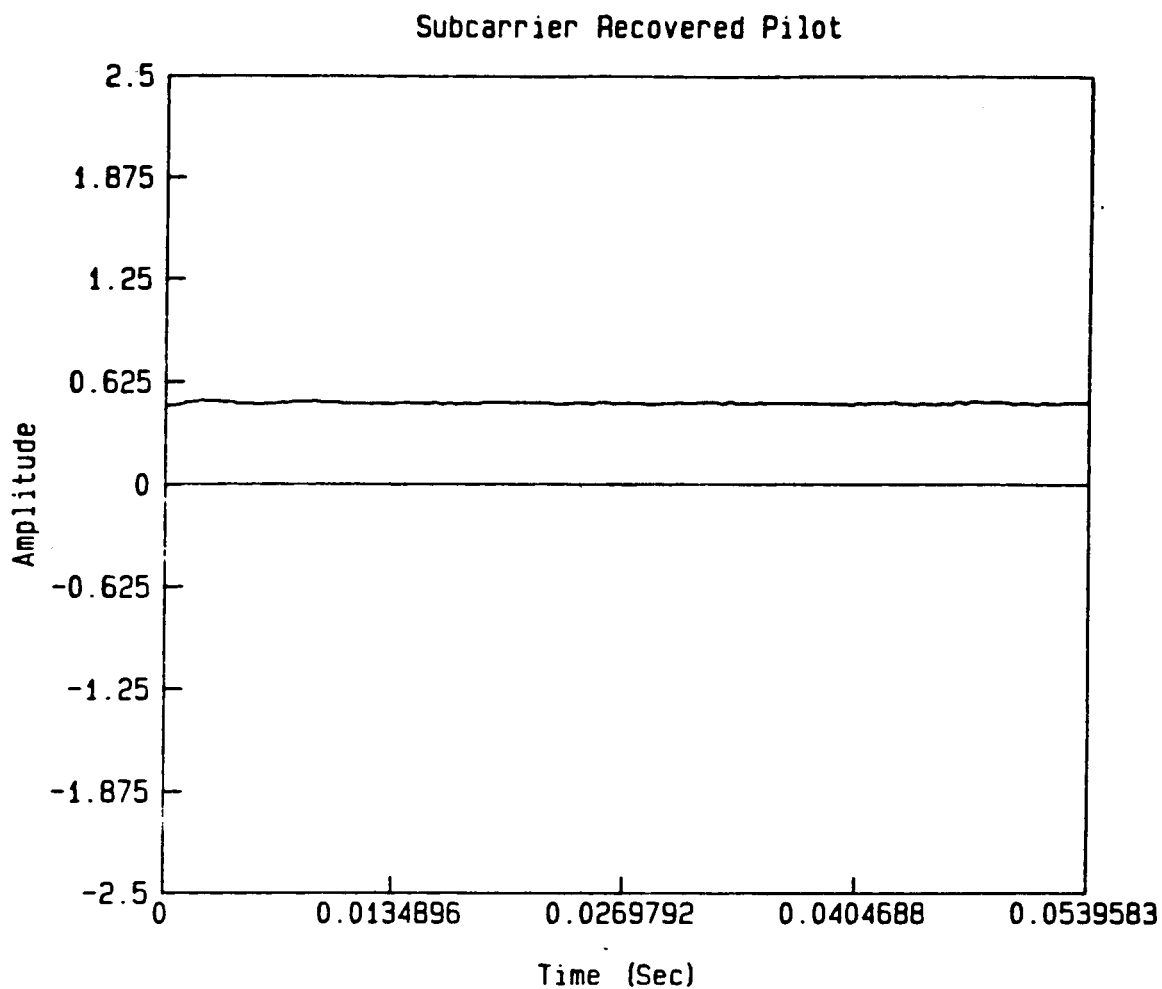


FIGURE 3.15(a) STCT RECOVERED PILOT, 150 HZ PILOT LOWPASS FILTER



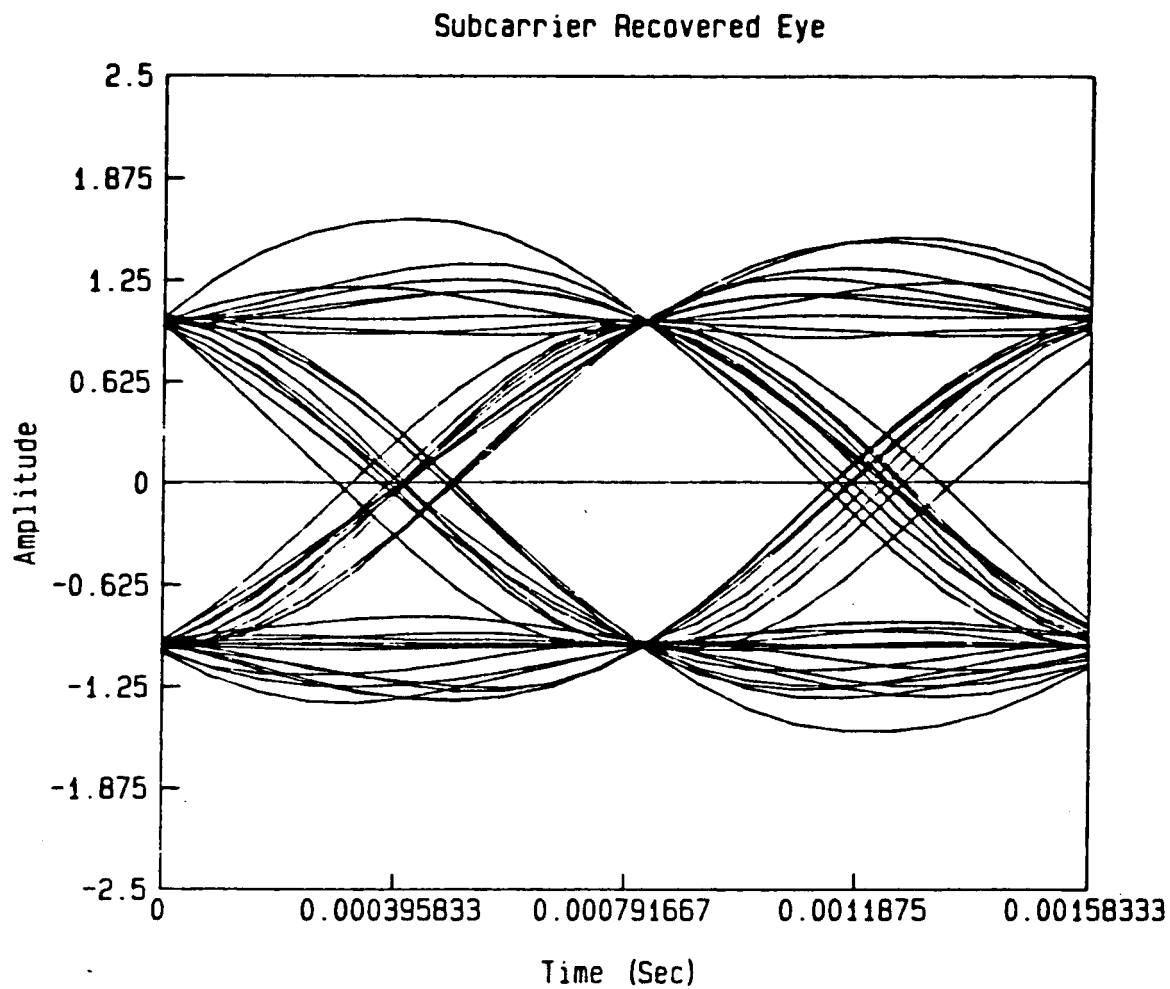


FIGURE 3.15 STCT RECOVERED EYE FOR THE PILOT OF FIGURE 3.15(b)

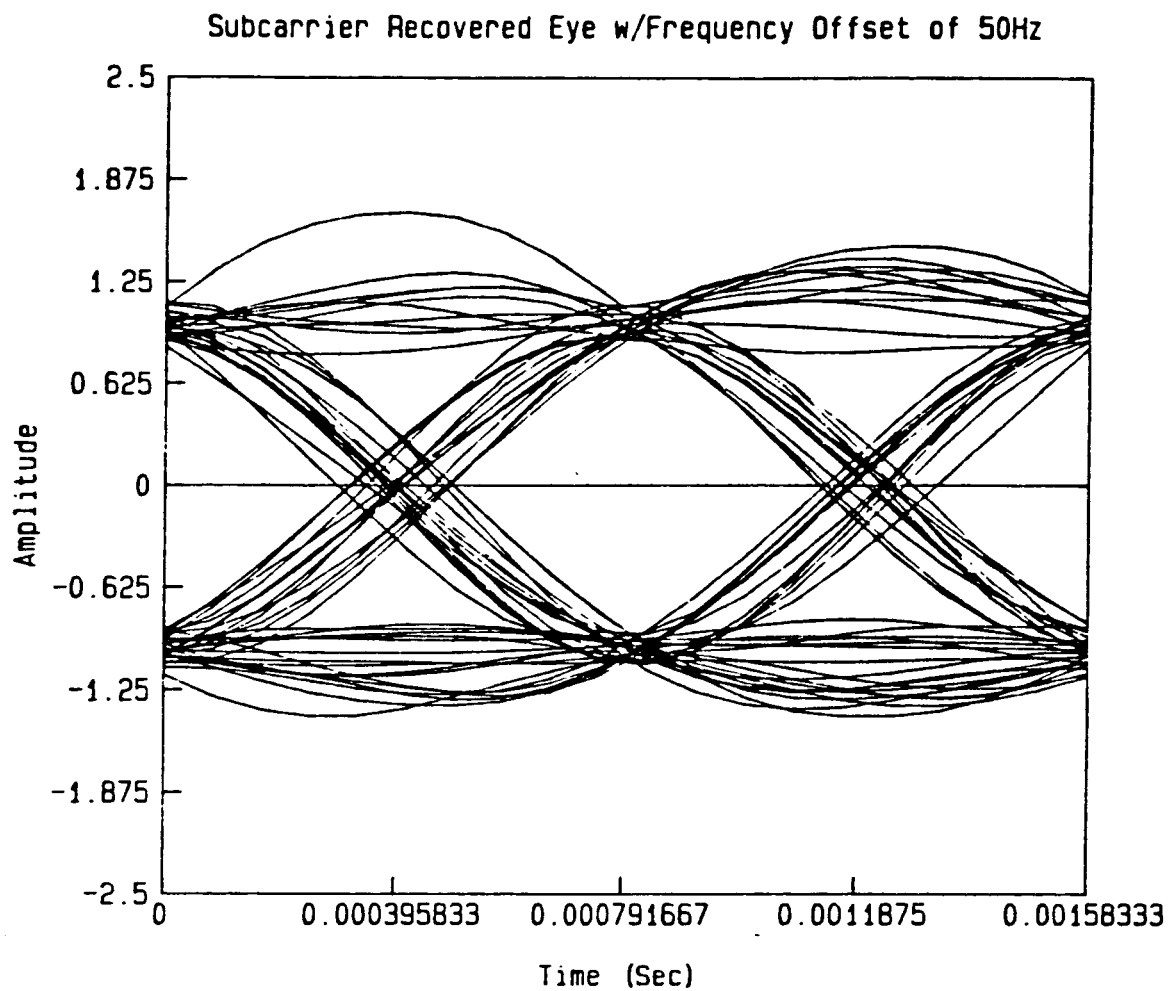


FIGURE 3.16 STCT RECOVERED EYE FOR A 50 HZ FREQUENCY OFFSET

### MANCHESTER TCT

TX HPF -----	PILOT REC. LPF -----	RELATIVE PILOT LEVEL -----
NO	150 HZ	22.8 DB
YES	150 HZ	17.5 DB
NO	80 HZ	16.1 DB
YES	80 HZ	6.2 DB

### SUB-CARRIER TCT

NO	150 HZ	0.0 DB
----	--------	--------

Table 3.2 Recovered Pilot Variances in dBs

been integrated with the stand-alone modulator board and is operative, as will be shown later. A circuit board design had been initiated for the MTCT demodulator and the TMS320 code is written, however, due to insufficient time to complete construction within the project schedule, it was decided by JPL not to follow it through to completion. The MTCT TMS320 software used in the premodulation processing is included in Appendix II.

Since the hardware implementation of the modulator was discussed previously in both the first and second interim reports, only the salient features will be presented in the following section.

#### 4.1.1 MTCT Modulator Implementation

A block diagram of the final stand-alone digital modulator is shown in Figure 4.1. All processing tasks are performed by the Texas Instruments TMS320, the remaining components of the board are necessary for the proper function of the TMS320. The program code is held in the 2K of EPROM and is read into the 2K of RAM upon the booting of the system. In this way, a slow access time, UV erasable PROM can be used in conjunction with fast RAM to avoid usage of once-only programmable bipolar PROM. The I/O block consists of three latches which control the two system outputs and single system input. The two remaining blocks pertain to the control timing of the processing. The Master Timing block includes a 20 MHz clock for the TMS32010 processor chip, while the other I/O timer strobes the TMS320 at a rate of 9.6 kHz., indicating that it is time for the system to release an inphase and quadrature sample pair to the QPSK modulator. Also, on every fourth set of outputs, a new data bit is read in.

The details of the modulator code were presented in the First Interim report [1] and will only be briefly summarized here. The TMS320 accepts a binary input at a rate of 2.4 kbps. These input bits are split into even and odd data streams prior to Manchester encoding. Encoding is performed only after two data bits have been input which has the effect of synchronizing the inphase and quadrature streams. The next step in the modulation process is to shape these encoded bits.

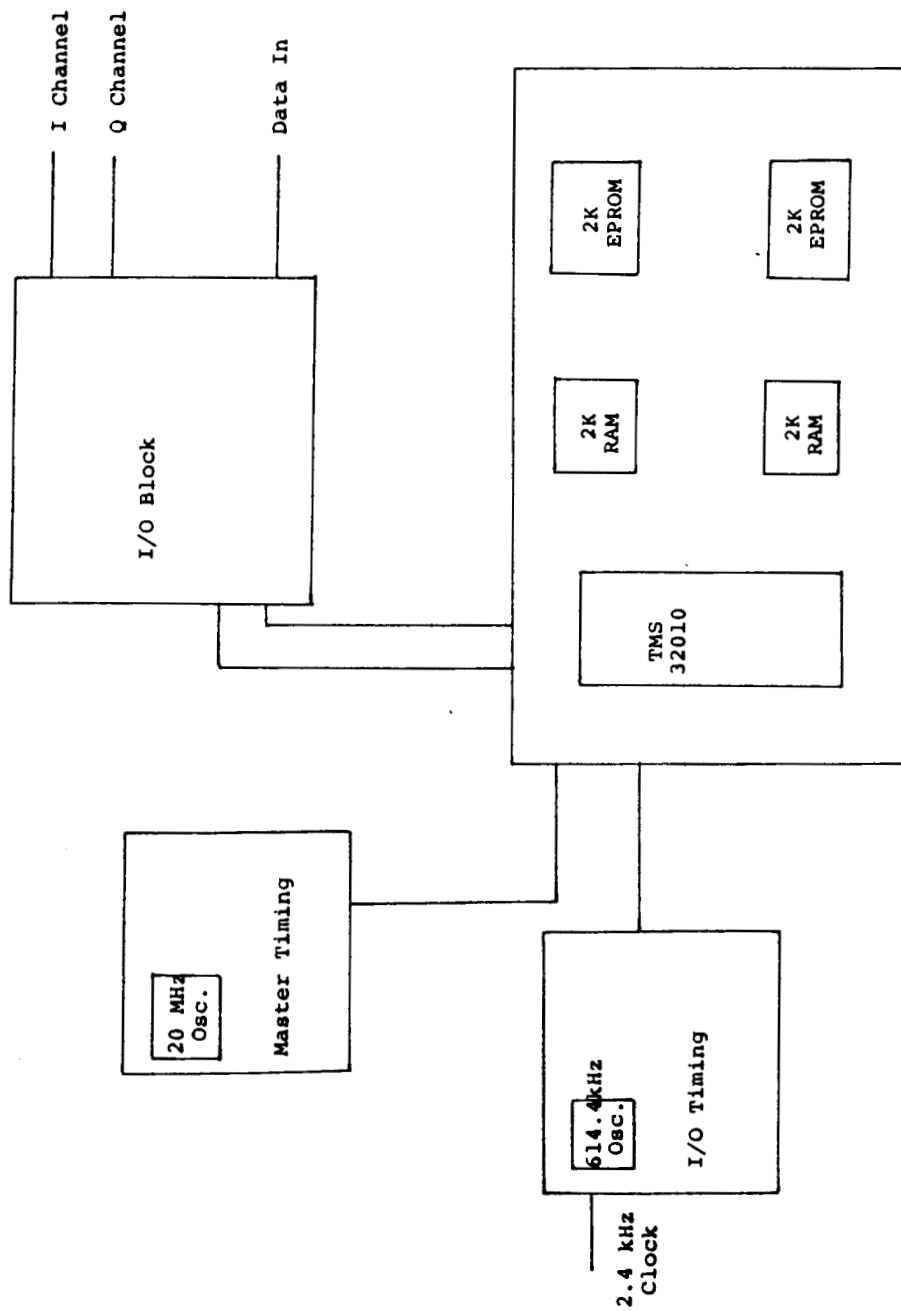


FIGURE 4.1 MTCT MODULATOR BOARD CONFIGURATION

The pulse-shaping chosen for implementation is the raised-cosine shape with an excess bandwidth fraction,  $\beta$ , of 0.5, as discussed in section 2.1. The raised-cosine pulse-shape is truncated such that it spans eight Manchester encoded data bits and is represented digitally by four evenly spaced samples per bit, for a total of thirty-two samples per pulse waveform. As will be shown presently, this representation of the raised-cosine pulse is sufficient to produce a transmit data 'eye' of the desired quality and spectral occupancy.

These thirty-two pulse-shape coefficients are stored in ROM and listed in Table 4.1. This table includes both the actual values of the coefficients as well as the scaled values used in the TMS320 implementation. The encoded data bits are pulse-shaped by simply multiplying these coefficients by the code bit in question. Therefore, a +1 is represented by the thirty-two coefficients that appear in Table 4.1, a -1 by their inverse. At any point in time, the output of the pulse-shaping section is simply the sum of the samples from all waveshapes that are non-zero at that instant in time. Due to the truncation of the pulse-shape, only the waveforms representing the eight most recent Manchester bits are non-zero and, hence, taken into consideration. Since there are four samples of the pulse-shape per Manchester bit period, there will be four outputs per I/Q stream from the processor chip per Manchester bit. The inphase and quadrature shaping is identical and operates independently on the separated even and odd data bit streams. Hence the I and Q shaping can be represented by the general equation:

$$s(t_i + j) = \sum_{n=t_i-7}^{t_i} cb_n * P(4(n-t_i + 8) + j) \quad j = 1,2,3,4 \quad (4.1)$$

where  $t_i$  is the time index of the most recent Manchester bit,  $cb_n$  refers to the encoded data bits (even or odd), the index  $j$  is an output pointer which indicates which of the four outputs for this particular set of code bits is under consideration, and the  $P(.)$  terms are the raised-cosine pulse-shape samples listed in table 4.1. After all four output samples have been generated, a new code bit enters into play, and the oldest bit of the last nine is

**Table 4.1**  
**Pulse Shaping Coefficients**

	<u>Actual Value</u>	<u>Scaled Value</u>
P(1) = P(32)	.00219	36
P(2) = P(31)	.00555	91
P(3) = P(30)	.00464	76
P(4) = P(29)	.000867	14
P(5) = P(28)	.00114	19
P(6) = P(27)	.01056	173
P(7) = P(26)	.0221	363
P(8) = P(25)	.01599	262
P(9) = P(24)	-.02533	-415
P(10) = P(23)	-.09172	-1503
P(11) = P(22)	-.1334	-2186
P(12) = P(21)	-.07953	-1303
P(13) = P(20)	.1159	1899
P(14) = P(19)	.4289	7028
P(15) = P(18)	.7587	12431
P(16) = P(17)	.9709	15908

discarded. Figure 4.2(a) shows the resulting eye diagram after Manchester encoding and raised-cosine pulse shaping. Note that at the sampling instants there is no intersymbol interference. Figure 4.2(b) shows the shaped spectrum corresponding to the eye diagram of Figure 4.2(a). Observe that, due to the addition of the Manchester coding, a shallow notch in the spectrum has appeared at d.c. In the next section of the modulator, this notch will be enlarged to facilitate pilot insertion and pilot processing at the receiver.

After the pulse-shaping has been completed, the shaped I and Q streams are sent on to be highpass filtered. This is done to accentuate the notch at d.c., which was initialized by the Manchester coding. Two FIR highpass filters were considered for implementation: one with 91 taps and the other with 45. Close inspection of the resulting eye diagrams and spectra indicated that the 45 tap filter was sufficient for the desired purposes and was implementable within the DSP chip. The actual and scaled values of the 45 tap weights used in the TMS320 implementation are listed in table 4.2. The filter design specifications used in the computer-aided design of this filter are as follows:

Stopband:            0 to 100 Hz  
 Passband:           >=250 Hz  
 3 dB Point:        150 Hz  
 0.5 dB Ripple:    >=250 Hz  
 20 dB Attenuation at d.c.

Linear Phase Response

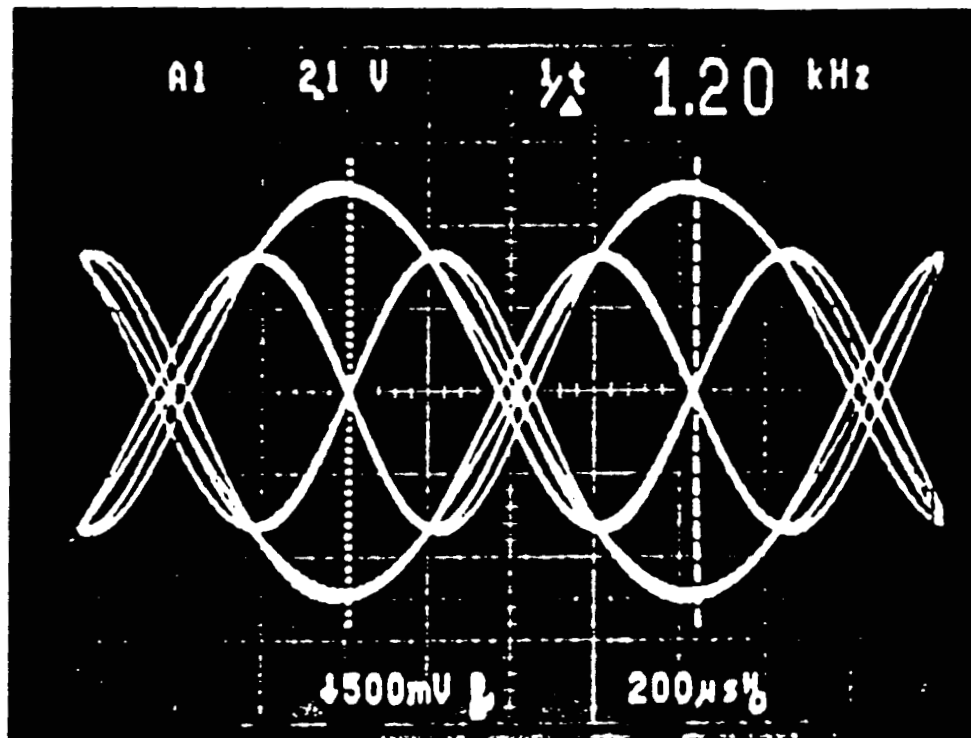
The impulse response of the TMS320 version of this high pass filter is shown in Figure 4.3.

The pre-modulation processor output can be represented by the following constant coefficient difference equation:

$$x(k) = \sum_{l=0}^{44} s_k z^{-l} H(l) \quad (4.2)$$



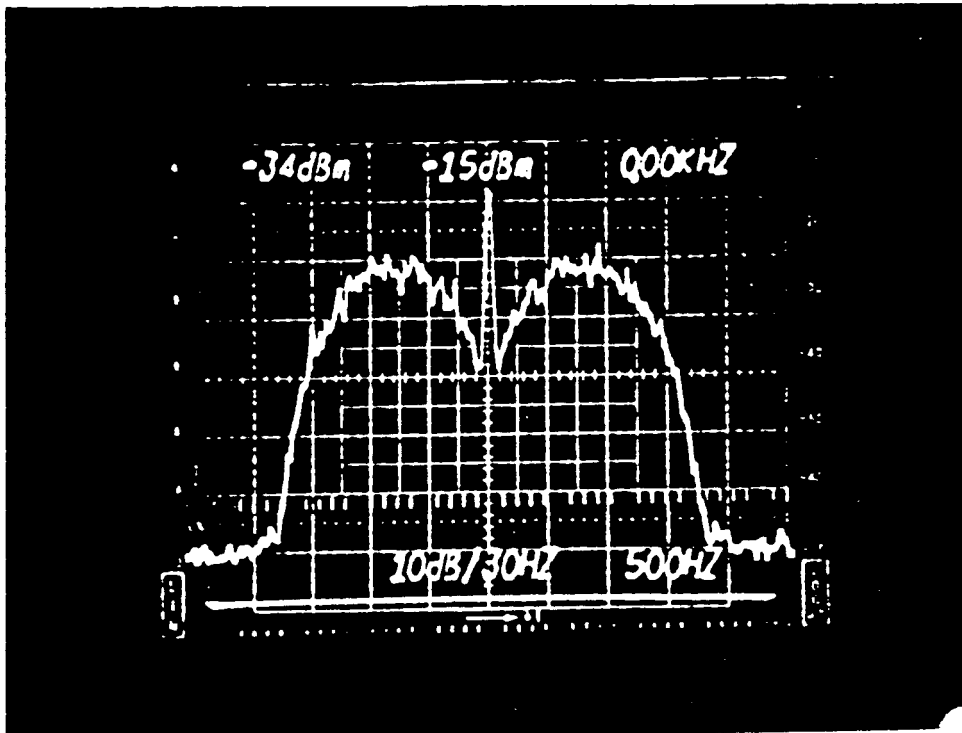
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EYE DIAGRAM - 1.2 kbps  
MANCHESTER CODING, 4 SAMPLES PER BIT SHAPING,  
8-BIT DAC, BETA = 0.5

FIGURE 4.2(a)

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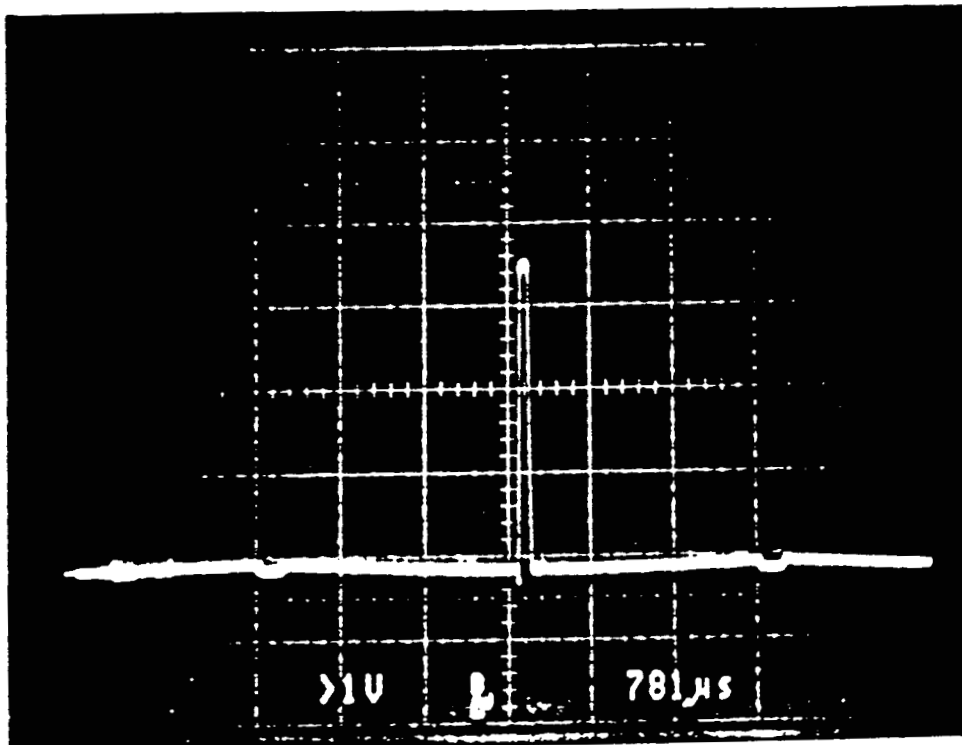
PULSE SHAPED SPECTRUM - 1.2 kbps  
MANCHESTER CODING, 4 SAMPLES PER BIT SHAPING,  
8-BIT DAC, BETA = 0.5

FIGURE 4.2(b)

Table 4.2  
Tap Weights - 45 Order Filter

	<u>Actual Value</u>	<u>Scaled Value</u>
H(0) = H(44)	-.0281	-115
H(1) = H(43)	-.0083	-34
H(2) = H(42)	-.0094	-39
H(3) = H(41)	-.0106	-43
H(4) = H(40)	-.0118	-48
H(5) = H(39)	-.0130	-53
H(6) = H(38)	-.0142	-58
H(7) = H(37)	-.0155	-63
H(8) = H(36)	-.0167	-68
H(9) = H(35)	-.0179	-73
H(10) = H(34)	-.0191	-78
H(11) = H(33)	-.0202	-83
H(12) = H(32)	-.0213	-87
H(13) = H(31)	-.0223	-92
H(14) = H(30)	-.0232	-95
H(15) = H(29)	-.0241	-99
H(16) = H(28)	-.0249	-102
H(17) = H(27)	-.0255	-104
H(18) = H(26)	-.0261	-107
H(19) = H(25)	-.0265	-109
H(20) = H(24)	-.0268	-110
H(21) = H(23)	-.0270	-111
H(22)	.9829	3985

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IMPULSE RESPONSE  
45 TAP HIGH PASS FILTER

FIGURE 4.3

where  $x(k)$  is the system output,  $s_k = s(t_i + j)$  are the shaped samples from equation 4.1, and the  $H(\text{scripl})$  terms are the high pass filter coefficients listed in Table 4.2. Highpass filtered inphase and quadrature samples are output simultaneously at a rate of 9.6 ksps. To generate the data staggering of OQPSK, the odd stream output is delayed by two output sample periods, or one-half of a Manchester bit period. Figure 4.4(a) shows the highpass filtered Manchester eye diagram. Note that intersymbol interference has been introduced at the sampling instants by the action of the highpass filter, as predicted in the software simulation. The frequency spectrum of the processed data for a random data input source is shown in Figure 4.4(b), and shows that the notch at d.c. has in fact been accentuated. However, this technique removes low frequency data energy as well, which results in the introduction of ISI into the transmit eye diagram.

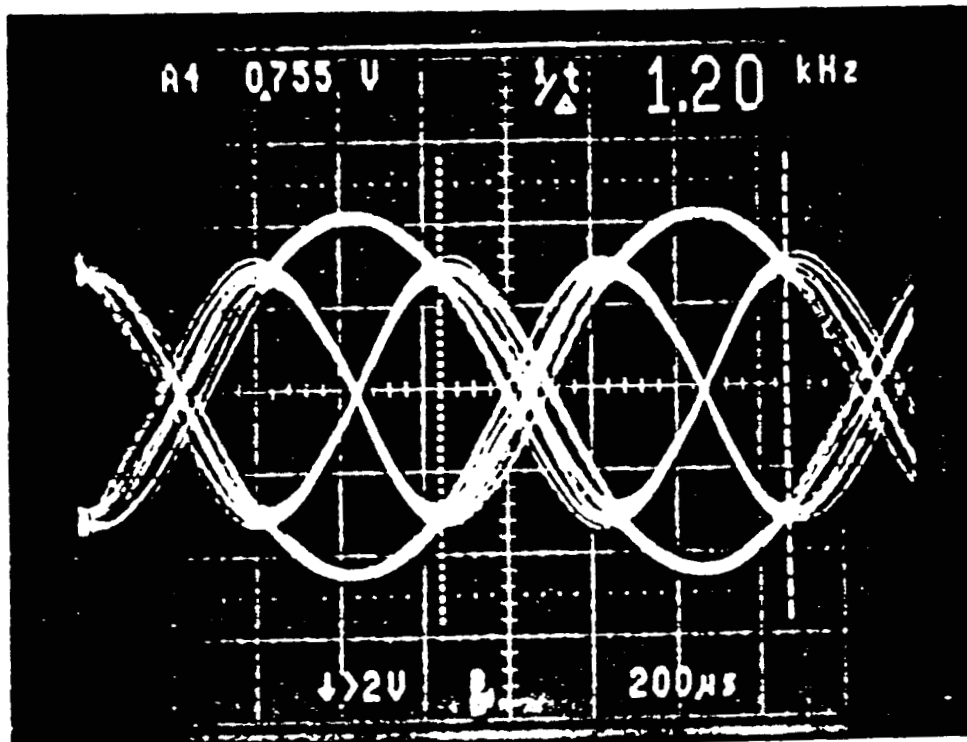
#### 4.1.2 Demodulator

This section describes the final state of the hardware implementation of the MTCT baseband demodulator. As with the modulator, the main processing element in the demodulator is the TMS32010 DSP chip. The stand-alone digital demodulator circuitry has been designed at the schematic level and requires two TMS320 processor chips to implement in its entirety. The RF receiver circuitry, see [7], has been designed, built and tested. The demodulator code has been written for both TMS320 processors, and has been debugged to the extent possible with the available software simulation packages. The TMS320 demodulator software has been included in Appendix III.

A block diagram of the digital MTCT demodulator appears in Figure 4.5. It is necessary to employ two TMS320 processors due to the complexity of the demodulation scheme; the partitioning of the signal processing requirements between the two processors is as indicated in Figure 4.5.

The received signal is translated to a suitable IF frequency by the RF circuitry and then converted to a digital signal prior to demodulation. The RF circuitry includes a step attenuator and bandpass filter which are used to accurately set carrier-to-noise ratios. The bandpass filter is also used to reject unwanted mixer products.

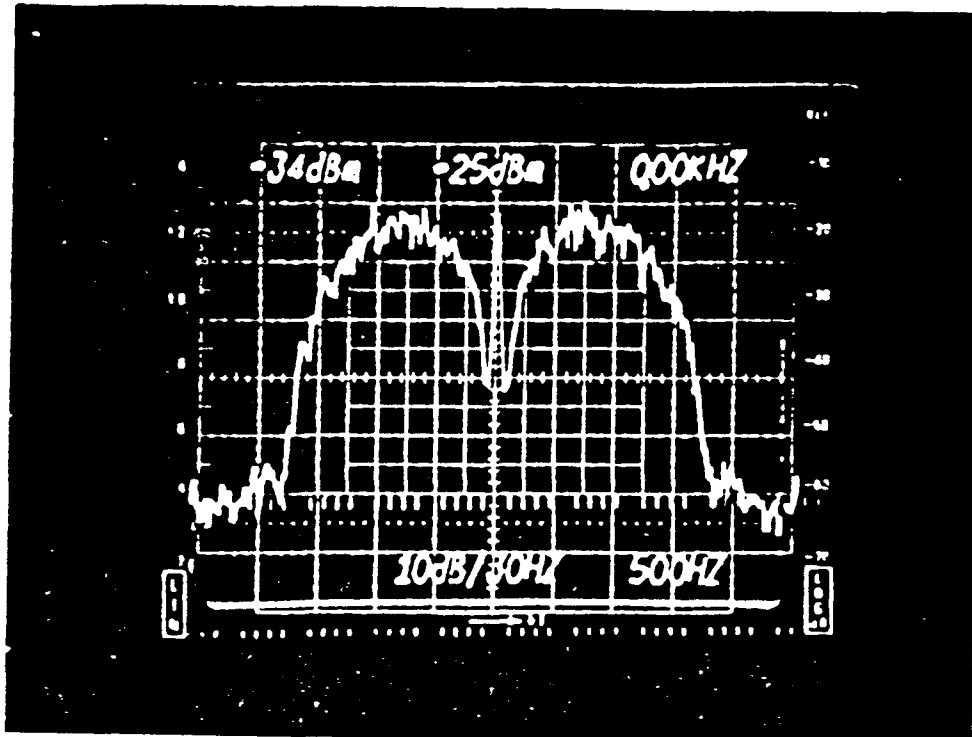
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FILTERED EYE DIAGRAM - 1.2 kbps  
MANCHESTER CODING, 4 SAMPLES PER BIT SHAPING,  
8-BIT DAC, BETA = 0.5,  
FOLLOWED BY A 45 TAP HIGH PASS FILTER

FIGURE 4.4(a)

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FILTERED PULSE SHAPED SPECTRUM - 1.2 kbps  
MANCHESTER CODING, 4 SAMPLES PER BIT SHAPING,  
8-BIT DAC, BETA = 0.5,  
FOLLOWED BY A 45 TAP HIGH PASS FILTER

FIGURE 4.4 (b)

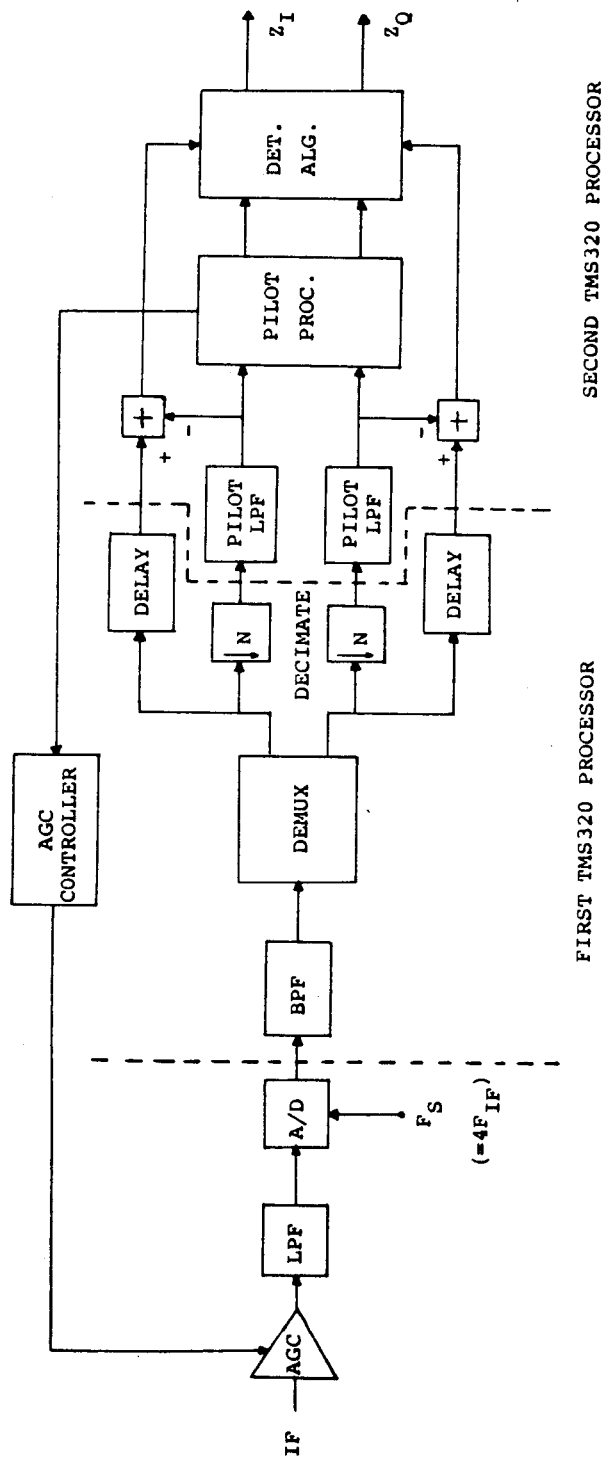


FIGURE 4.5 MTCT DEMODULATOR



The received signal is fed to the RF port of a double balanced mixer where it is mixed with the LO signal. A low-side mix arrangement is used with a 149.999988 MHz LO, producing an intermediate frequency of 12 kHz. The resulting IF signal is filtered and amplified by a fixed gain stage. Automatic Gain Control has not been considered in this implementation, due to its added complexity, however, if it was to be included, it would be introduced after the IF filtering as part of the IF gain stage. The output of the gain stage is then fed to the input of a 14-bit A/D converter, operating at 48 ksamples/second, i.e. four times the IF frequency, to generate the digital input to the baseband MTCT demodulator. This sample rate will eventually produced 10 samples per Manchester code bit or 20 per raw data bit, which, as shown by computer simulation, is more than sufficient for the demodulation and detection processes.

Due to this particular choice of sampling frequency, four times the intermediate frequency, it is apparent that quadrature sample pairs have been produced. This can be directly compared to the conventional generation of I and Q signals which employs quadrature analog mixing. As a direct result of the  $4 \cdot \text{IF}$  sampling frequency, the sampled IF signal emanating from the A/D is such that every other pair of samples are phase inverted. Translation to baseband is accomplished by simply changing the sign of these inverted quadrature pairs. This is equivalent to mixing the IF signal with a square wave of the same frequency.

The amount of processing necessary for implementation of the digital demodulator cannot be performed at a rate of 48 ksamples per second by a single TMS320. To ease the implementation requirements, multirate processing has been used. This requires that the input signal be bandpass filtered to meet the Nyquist criterion for the maximum decimation signal processing path to avoid adjacent channel and noise aliasing (foldover). The bandpass filter meeting these requirements has the following specifications:

Passband Center: 12 kHz.  
-3 dB points: 10.2 and 13.8 kHz.  
-45 dB points: 6.24 and 17.74 kHz.

#### Linear Phase Response

The filter coefficients are listed in Table 4.3 along with the scaled values which are used in the TMS320 implementation. The bandpass filter code was tested using the TI TMS320 EVM (Evaluation Module) board; however, due to the limitation of the on-board A/D, the filter was implemented with a sample rate of 39 kHz. The amplitude and phase responses of the 39 kHz version of this bandpass filter are shown in Figures 4.6 and 4.7. These correspond to the desired 48 kHz sample rate filter when the above specifications are scaled by the factor (39/48).

The next step undertaken following the bandpass filter is to split the input data stream into inphase and quadrature channels. Recall that the I and Q streams are generated by sampling the IF signal at four times the IF frequency and processing the samples as discussed above. However, in the implementation considered, only every other sample pair is used thus avoiding the need for the inversion of alternate sample pairs without any loss of information. The remaining pairs are demultiplexed, with the first sample of each pair being placed in the I channel and the second in the Q channel. As a result of this demodulation and subsequent splitting of the received data stream, the rate of each of these channels is 12 ksamples per second, or 5 samples per Manchester code bit.

The remainder of the processing in the first TMS32010 is the same for both the inphase and quadrature channels and, therefore, only one channel will be described. The I (or Q) signal is first reproduced to form two duplicate streams. One of these duplicate streams is decimated by five, which reduces the sampling rate to 2.4 kHz, and is immediately sent on to the second TMS320 processor, where it will be low pass filtered as part of the pilot processing. It is important to note that this decimation does not cause aliasing in the

Table 4.3  
Bandpass Filter Coefficients

	<u>Actual Value</u>	<u>Scaled Value</u>
H(1) = H(31)	-.1193 E-5	0
H(2) = H(30)	-.5156 E-3	-34
H(3) = H(29)	-.3013 E-6	0
H(4) = H(28)	-.01183	-775
H(5) = H(27)	-.2559 E-6	0
H(6) = H(26)	.0304	1994
H(7) = H(25)	-.7395 E-6	0
H(8) = H(24)	-.0302	-1980
H(9) = H(23)	.8667 E-6	0
H(10) = H(22)	-.0237	-1551
H(11) = H(21)	.1482 E-5	0
H(12) = H(20)	.1346	8822
H(13) = H(19)	-.8743 E-6	0
H(14) = H(18)	-.2524	-16544
H(15) = H(17)	.1010 E-5	0
H(16) =	.3035	19888

REF LEVEL /DIV MARKER 9 750.000Hz  
20.000dB 10.000dB MAG (A/R) 7.302dB

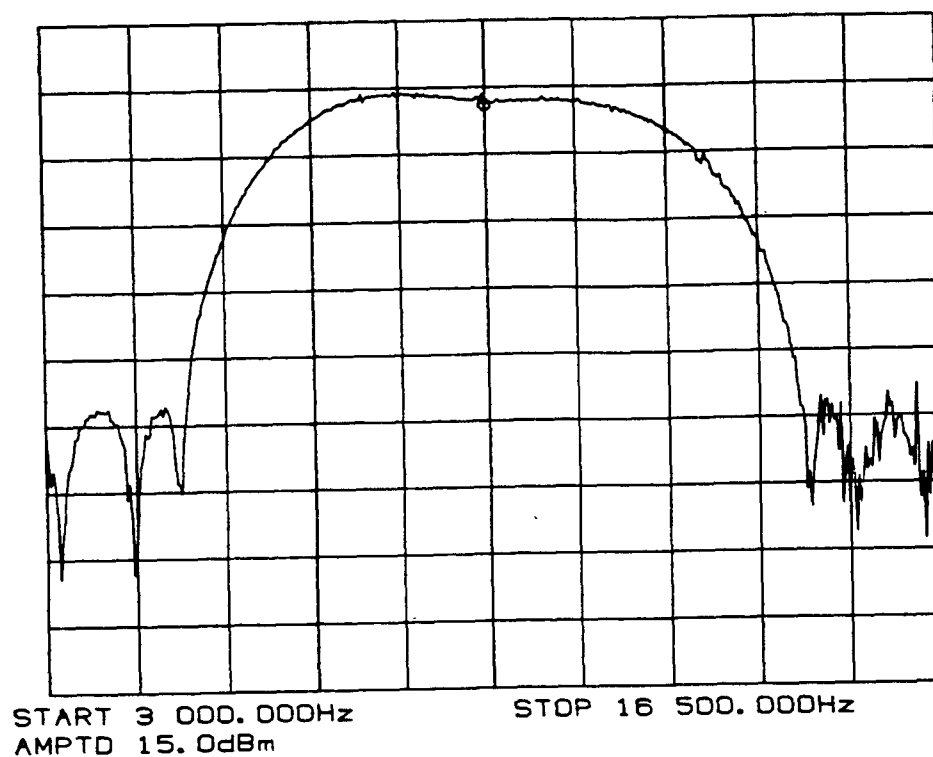


FIGURE 4.6 MAGNITUDE RESPONSE OF BANDPASS FILTER, 16 BIT  
COEFFICIENTS, SAMPLING FREQUENCY = 39 kHz

REF LEVEL     /DIV     MARKER 9 750.000Hz  
0.0deg     45.000deg     PHASE (A/R) 45.312deg

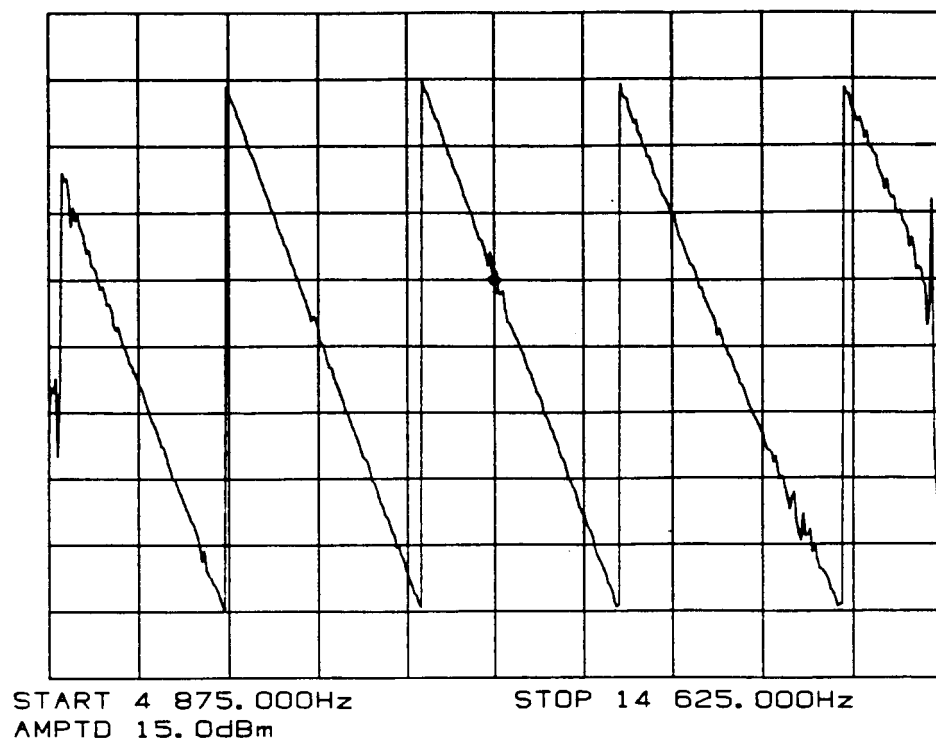


FIGURE 4.7     PHASE RESPONSE OF BANDPASS FILTER IN FIGURE 4.6

pilot filter passband but does improve the filter cut-off to sampling ratio, making it possible to use a lower order filter.

The other sample stream is placed into an external RAM, which functions as a delay buffer to compensate for the pilot processing input/output delay, thereby maintaining synchronization between the two streams. The external RAM stores the samples until it is time to send them on to the second TMS320 processor, where the pilot tone component will be removed from these appropriately delayed samples. The remaining functions of the demodulator are performed in the second processor which, conceptually, consists of two parallel paths, one dedicated to the pilot processing and the other to the delayed data. These paths converge at the detection algorithm, where fade compensation and synchronous data detection are performed. As stated above, the I and Q data streams undergo identical processing, as do the inphase and quadrature baseband pilot components.

The first operation performed in the processing of the pilot is to lowpass filter the undelayed, decimated I and Q sample trains in order to recover the pilot tone components. Assuming an expected worst case fading frequency of 80 Hz at the receiver, the lowpass filter design specifications are as follows:

-3 dB at 80 Hz.

-39 dB at 160 Hz.

#### Linear Phase Response

The pilot lowpass filter coefficients are listed in table 4.4. Included are the 13 bit scaled integer values used in the TMS320 software. The pilot digital filter was designed to operate at 2.4 kHz to achieve its desired frequency response; however, it was tested on the TMS320 EVM board at a 39 kHz sampling rate for better frequency resolution. The resulting magnitude and phase responses, of Figures 4.8 and 4.9, are therefore scaled by the factor (39/2.4). Responses are not shown to zero frequency due to leakage from the local oscillator of the network analyzer.

Table 4.4

## Pilot Lowpass Filter Coefficients

	<u>Actual Value</u>	<u>Scaled Value</u>
H(0) = H(64)	-.00623	-204
H(1) = H(63)	-.00079	-26
H(2) = H(62)	-.00031	-10
H(3) = H(61)	.00052	17
H(4) = H(60)	.00164	54
H(5) = H(59)	.00294	96
H(6) = H(58)	.00426	139
H(7) = H(57)	.00538	176
H(8) = H(56)	.00609	200
H(9) = H(55)	.00619	203
H(10) = H(54)	.00550	180
H(11) = H(53)	.00393	129
H(12) = H(52)	.00148	49
H(13) = H(51)	-.00173	-57
H(14) = H(50)	-.00550	-179
H(15) = H(49)	-.00936	-307
H(16) = H(48)	-.01297	-425
H(17) = H(47)	-.01578	-517
H(18) = H(46)	-.01728	-566
H(19) = H(45)	-.01696	-556
H(20) = H(44)	-.01443	-473
H(21) = H(43)	-.00945	-310
H(22) = H(42)	-.00193	-63

Table 4.4  
Pilot Lowpass Filter Coefficients

	<u>Actual Value</u>	<u>Scaled Value</u>
H(23) = H(41)	.00799	262
H(24) = H(40)	.01994	654
H(25) = H(39)	.03338	1094
H(26) = H(38)	.04758	1559
H(27) = H(37)	.06169	2021
H(28) = H(36)	.07483	2452
H(29) = H(35)	.08613	2822
H(30) = H(34)	.09480	3107
H(31) = H(33)	.10028	3286
H(32)	.10215	3347



REF LEVEL    /DIV    MARKER 997.000Hz  
30.000dB    10.000dB    MAG (A/R)    10.529dB

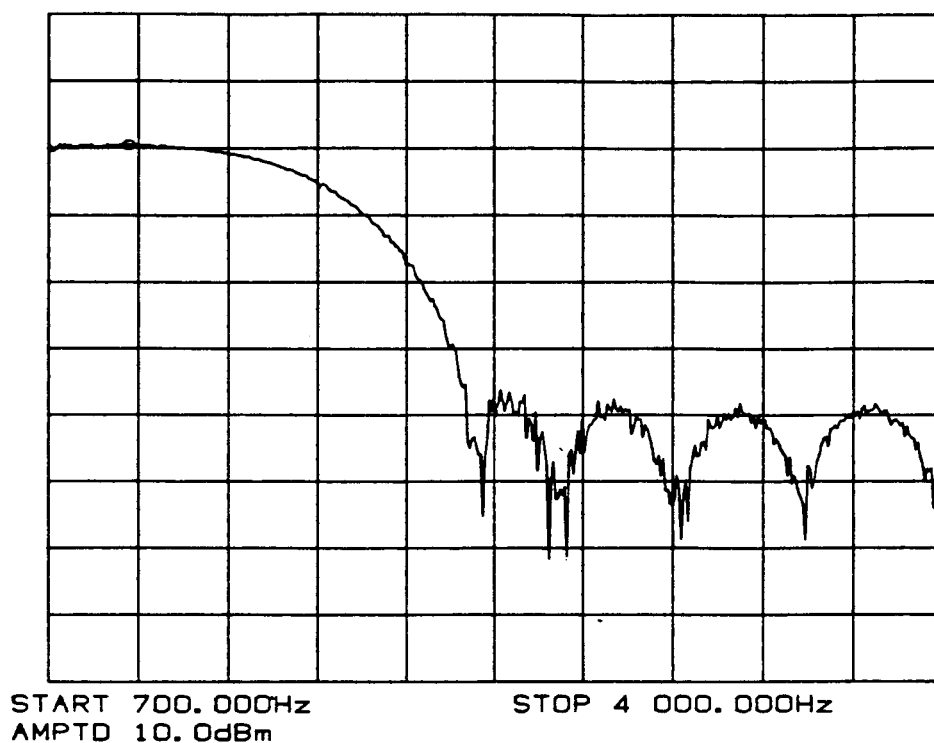


FIGURE 4.8    MAGNITUDE RESPONSE OF THE PILOT LOWPASS FILTER,  
13 BIT COEFFICIENTS, SAMPLING FREQUENCY = 39 kHz

REF LEVEL      /DIV      MARKER 754.000Hz  
 0.0deg      45.000deg      PHASE (A/R) -97.500deg

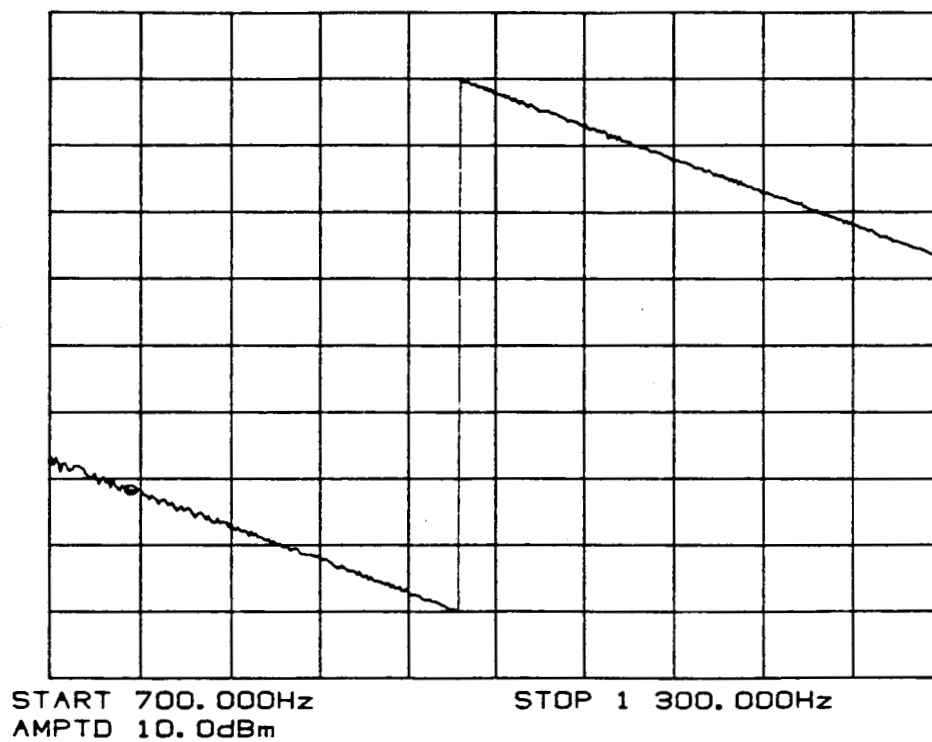


FIGURE 4.9      PHASE RESPONSE OF THE PILOT LOWPASS FILTER IN  
 FIGURE 4.8

The filtered I and Q streams are utilized in two ways: (1) they are passed on to the pilot processor and (2) they are subtracted from their respective delayed I/Q sample train. The latter operation removes the pilot from the unfiltered 12 kHz sample stream and the result is sent to the detection algorithm.

The subtraction of the lowpass filtered signal from the delayed sample stream may at first appear to be straightforward, however it is complicated by the multirate processing. Specifically, the unfiltered stream has a sample rate of 12 kHz, while the filtered stream, having been decimated by five, has a sample rate of only 2.4 kHz. In order to perform the subtraction, a linear interpolation of the sample values of the 2.4 kHz stream is used to raise the sample rate. Linear interpolation was selected over the less complex zero-order hold method because the software simulation of this demodulator indicated that the additional accuracy afforded by the interpolation method is necessary.

The I and Q recovered pilot components, at 2.4 ksamples/sec, are passed onto the pilot processor block which extracts the fading phase information. This, in turn, is passed onto the detection algorithm where it is used to mitigate the fading effects on the data sidebands. This process is based on the assumption that the pilot has been exposed to the same channel perturbations as the data, e.g. Rician or Rayleigh multipath fading. The I and Q outputs of the the pilot processor are used in the detection algorithm as coherent phase references. The pilot processing function is detailed in equation 4.3.

$$\tan^{-1}(\varphi) = Q_p / I_p = \cos(\varphi) / \sin(\varphi) \quad (4.3)$$

In the actual implementation, the inverse tangent is not evaluated, rather, the result of the  $Q_p / I_p$  division is used to determine the corresponding sine and cosine values via a look-up table. The periodicity and symmetry of the trigonometric functions are exploited to minimize the size of this look-up table, only  $\cos(\varphi)$  and  $\sin(\varphi)$  values for  $\varphi$  in the range  $[0, \pi/4]$  need be stored in order to implement this function. Therefore, this processing block will

first divide a quadrature sample by its corresponding inphase sample, then simply use this look-up table to locate the appropriate cosine and sine values. The  $[0, \pi/4]$  angle range is subdivided into 128 levels. Software simulations have shown that this is of sufficient accuracy. These cosine and sine terms are sent on to the next phase in the demodulator, the detection algorithm.

The last section of the demodulator is the detection algorithm. This function block uses the sine and cosine of the pilot angle, which at this point should consist of the pilot tone with amplitude variations removed, as coherent phase references for the simultaneous operations of data recovery and the removal of channel phase perturbations. The algorithm is as follows:

$$Z_I = 2I_D \cos(\varphi) + 2Q_D \sin(\varphi) \quad (4.4)$$

and

$$Z_Q = 2Q_D \cos(\varphi) - 2I_D \sin(\varphi) \quad (4.5)$$

where  $I_D$  and  $Q_D$  are the inphase and quadrature samples from the 12 kHz streams. The demodulated signals,  $Z_I$  and  $Z_Q$ , are then fed off chip to analog integrate-and-dump data detectors to produce an estimate of the transmitted data.

As in the case of the removal of the pilot signal from the received signal, the detection process is complicated by the multirate processing. Here, the I and Q streams are sampled at 12 kHz while the cosine and sine signals are sampled at only 2.4 kHz. As before, linear interpolation is employed to match the rates of the two streams. The outputs of the detector consist of one inphase and one quadrature data channel, which are filtered to remove out-of-band noise before they are sent on to the detector/decoder board. The specifications for this final data filter are

-3 dB at 2.0 kHz.  
-30 dB at 2.4 kHz.

#### Linear Phase Response

The coefficients and their scaled integer values for the data lowpass filter are listed in table 4.5. The designed sampling frequency is 12 kHz. The tested sampling frequency is 19.52 kHz, yielding a scaling factor of (19.52/12) for the magnitude and phase frequency responses of Figures 4.10 and 4.11.

#### 4.2 Subcarrier TCT Modulator

In section 2, the subcarrier method of TCT was presented, and proved to be similar, in many respects, to the Manchester encoded TCT. The basic difference between the two approaches is the way in which they create the spectral null at d.c. The STCT version creates this null by simply modulating the data onto a very low frequency subcarrier. The similarities between the two approaches carry through to their hardware implementation. A hardware version of the STCT modulator was also completed. It utilizes the same stand-alone board and RF circuitry employed in the MTCT modulator. In order to change modulation methods, it is only necessary to replace the two EPROM's used for program memory with those containing the subcarrier code.

The TMS320 implementation of the STCT modulator, outlined previously in Figure 2.3, is quite similar to the MTCT version described previously. The data is input at the same rate, 2.4 kbps, and is immediately split into separate inphase and quadrature channels. The Manchester coding is replaced here by a simpler bipolar coding scheme, and the code bits are then sent on at a rate of 1.2 kbps to the pulse shaping section.

The pulse shape used for the STCT modulator is the same as that employed in the MTCT modulator, a raised-cosine waveform with a  $\beta$  of 0.5, truncated to eight code bits. The subcarrier version, however, represents this waveform in the digital domain by eight samples per bit, instead of the four which were

Table 4.5  
Data Lowpass Filter Coefficients

	<u>Actual Value</u>	<u>Scaled Value</u>
H(0) = H(40)	-.00453	-37
H(1) = H(39)	-.00306	-25
H(2) = H(38)	.01315	108
H(3) = H(37)	-.00009	-1
H(4) = H(36)	-.00535	-44
H(5) = H(35)	-.01099	-90
H(6) = H(34)	-.00104	-8
H(7) = H(33)	.01268	104
H(8) = H(32)	.01460	120
H(9) = H(31)	-.00315	-26
H(10) = H(30)	-.02296	-188
H(11) = H(29)	-.01866	-153
H(12) = H(28)	.01308	107
H(13) = H(27)	.03960	324
H(14) = H(26)	.02212	181
H(15) = H(25)	-.03587	-294
H(16) = H(24)	-.07452	-610
H(17) = H(23)	-.02444	-200
H(18) = H(22)	.12216	1001
H(19) = H(21)	.28662	2348
H(20)	.35858	2937

REF LEVEL      /DIV      MARKER 1 960.000Hz  
 33.000dB      10.000dB      MAG (A/R)      10.313dB

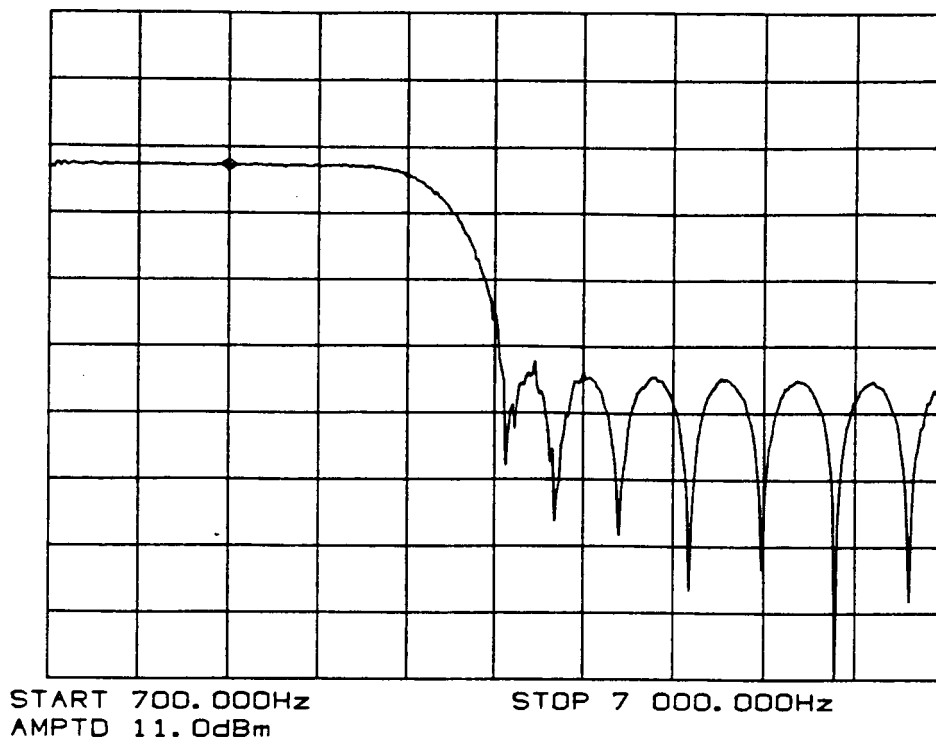


FIGURE 4.10      MAGNITUDE RESPONSE OF THE DATA LOWPASS FILTER  
 13 BIT COEFFICIENTS, SAMPLING FREQUENCY = 19.52 kHz

REF LEVEL     /DIV     MARKER 1 146.000Hz  
0.0deg     45.000deg     PHASE (A/R) 93.158deg

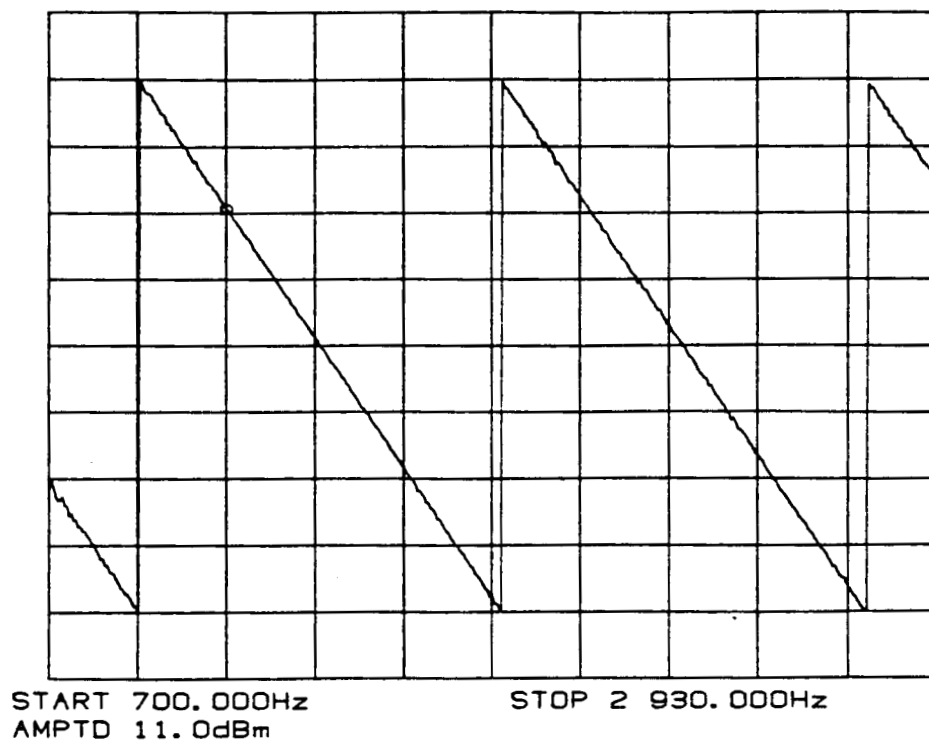


FIGURE 4.11 PHASE RESPONSE OF THE DATA LOWPASS FILTER IN

FIGURE 4.10



used earlier. This doubling of the number of samples per bit insures that the output of the pulse shaping section has a rate of 9.6 ksamples per second, the same rate the output waveform has in the MTCT implementation.

The eye diagram produced by the STCT pulse shaping section is shown in Figure 4.12(a). Note, once more, that at the sampling instants there is negligible intersymbol interference. The spectrum of this waveform is shown in the following illustration, Figure 4.12(b), and is the required 40 dBc at 1.8 kHz.

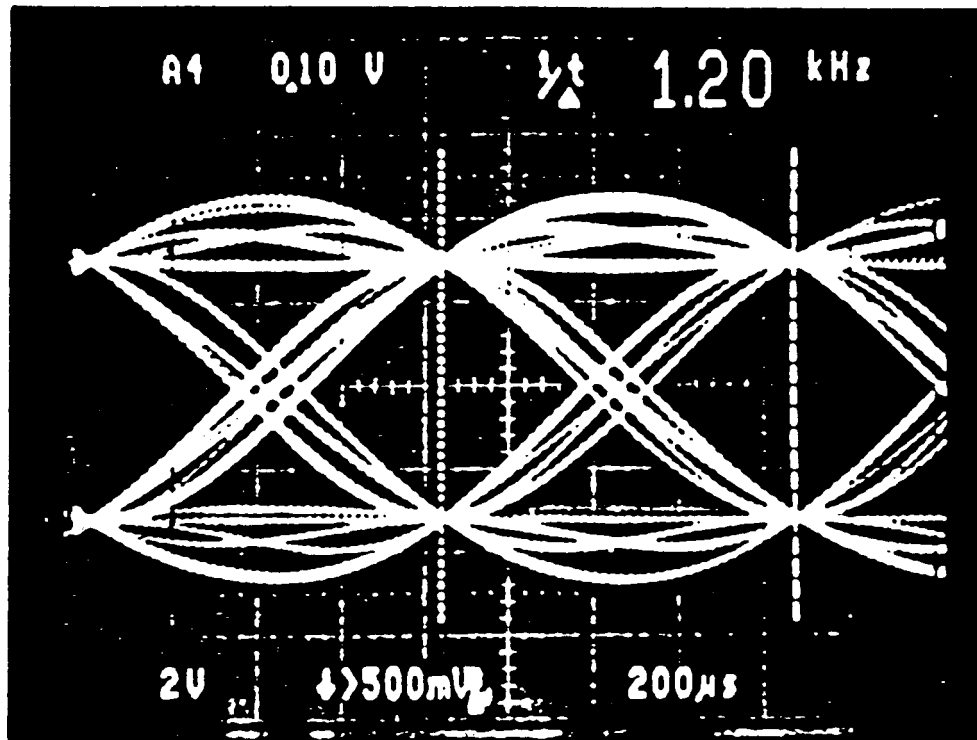
The final block of the STCT processor is the modulation section. Here, the shaped even stream is multiplied by a cosine term, the odd stream by a sine term, they are summed and then passed to the RF circuitry. The subcarrier frequency of these sine and cosine terms was chosen to be 960 Hz because it is an integer submultiple of the data rate 9.6 kHz. This means that only ten sample values of each sinusoid need to be stored in order to implement the modulator. The result of this modulation is then sent on to the D/A on the RF board.

The spectrum produced by the STCT modulator is shown in Figure 4.13. The modulation has produced a deep null at zero frequency, where the pilot would be placed. This null is deeper than that created by the MTCT modulator, as expected. The null width could be increased and the bandwidth reduced to the specified 3.6 kHz by simply changing the pulse shape to have a  $\beta$  value of 0.4.

## 5. CONCLUSIONS

The two major goals of this program were the design of an improved, all digital, Manchester encoded based TCT modulator as well as the investigation of a baseband I/Q demodulator and detector. It is believed that both of these goals were achieved and, in addition, a viable alternative to the Manchester system, the subcarrier technique, was derived.

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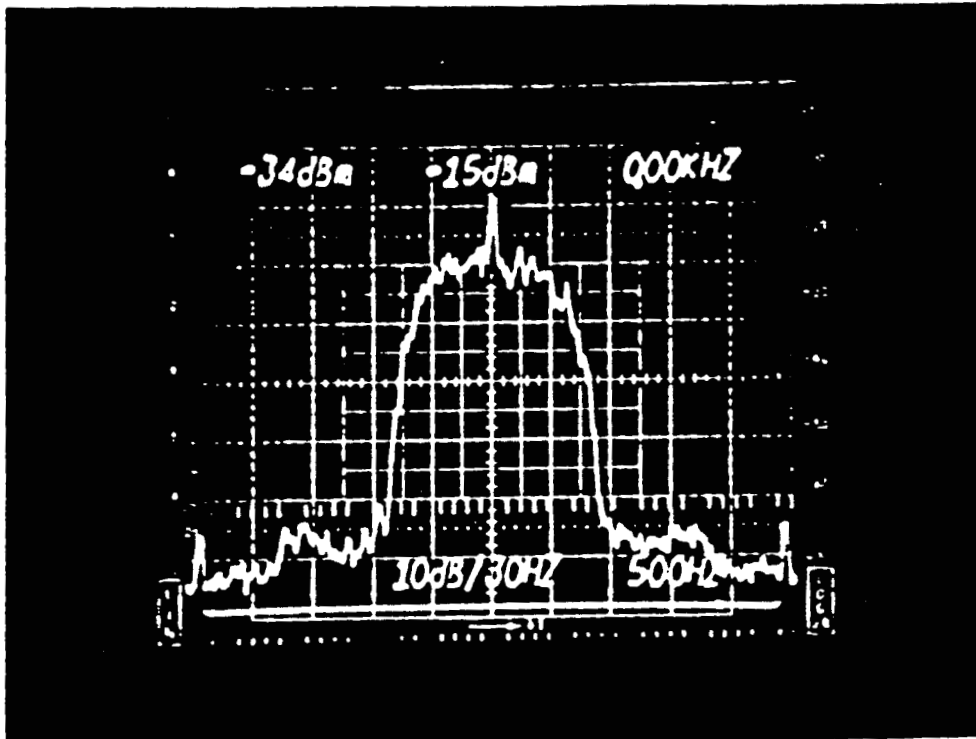


EYE DIAGRAM - 1.2 Kbps

NRZ CODING, 8 SAMPLES PER BIT SHAPING,  
8 BIT DAC, BETA = .5

FIGURE 4.12(a)

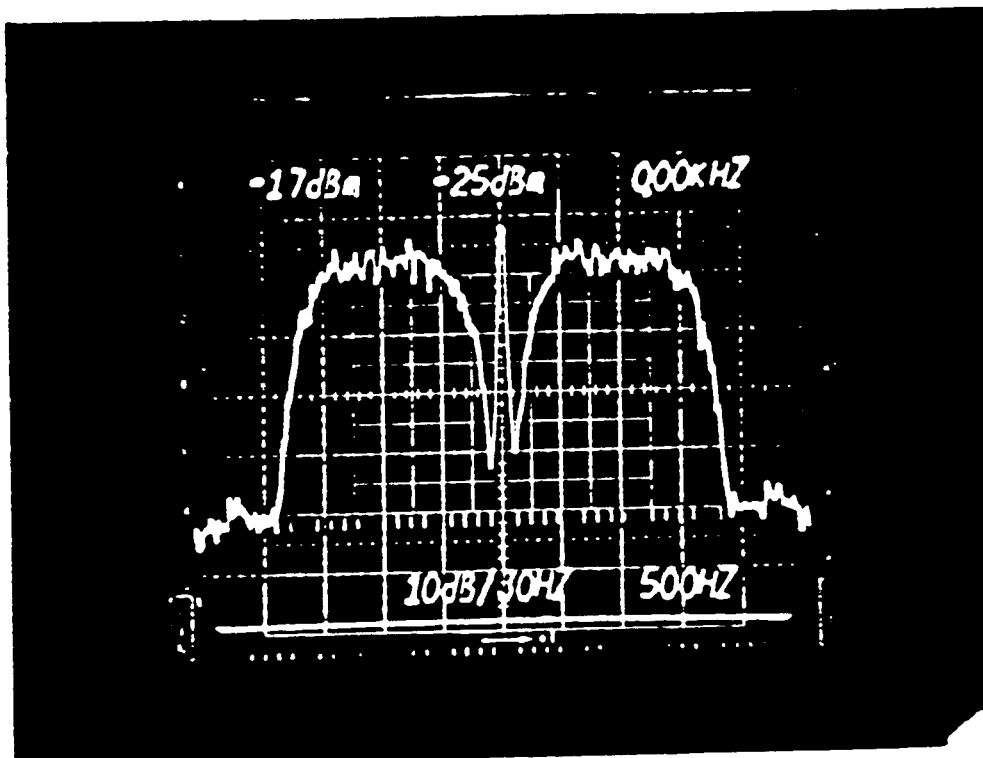
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PULSE SHAPED SPECTRUM - 1.2 Kbps  
NRZ CODING, 8 SAMPLES PER BIT SHAPING,  
8 BIT DAC, BETA = .5

FIGURE 4.12(b)

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MODULATED PULSE SHAPED SPECTRUM - 1.2 Kbps

NRZ CODING, 8 SAMPLES PER BIT SHAPING,  
8 BIT DAC, BETA = .5

FIGURE 4.13

Computer simulation and hardware implementation were employed to investigate the Manchester TCT modulator proposed by Davarian [2] which included a highpass filter to improve the spectral null created by the Manchester source encoding. The results obtained showed that the spectral null at zero frequency could be enlarged by the filtering, however, the removal of the low frequency data energy introduced intersymbol interference of approximately 18% into the transmit data eye. This was considered to be a significant disadvantage given the amount of additional filtering that was required in both the inphase and quadrature paths. It is apparent that this technique is less than optimum especially since no advantage was being derived from the raised-cosine shaping in the critical area of the spectral null.

To gain the advantage of the pulse-shaping and simultaneously remove the need for the highpass filters, it was clear that a subcarrier modulation technique should be explored. This would permit the arbitrary location of the upper and lower data sidebands at a point where they would be symmetrical around the transmit band center. This would also allow for equal sideband roll-off without incurring an ISI penalty, by virtue of the excess bandwidth fraction. In this way the shape of the data spectrum around zero frequency can be easily controlled. In addition, the premodulation processing is simplified, as was shown in section 2.2.1. It has also been demonstrated that, using the STCT processor, it is now possible to perform fully digital QPSK modulation with all the attendant advantages, such as improved carrier suppression, pilot insertion and adjustment free operation. The subcarrier TCT modulator was simulated and constructed, and demonstrated superior performance to that of the MTCT counterpart. The use of the subcarrier, however, slightly complicates the demodulator arrangement over that of the MTCT system but this is not considered to be a serious problem, as has been borne out by computer simulation.

Considerable effort was directed towards the design, computer simulation and implementation of a baseband TCT compatible demodulator. The salient features of the selected configuration are: a pilot phase-recovery-only scheme, used to reduce implementation complexity; inband pilot components in the I and Q data paths, removed by a simple subtraction process; multi-rate

processing, also for reduced complexity; and a provision for a long term AGC function.

Computer simulation of both the Manchester and subcarrier demodulators, in conjunction with their respective modulators, revealed no conceptual problems, however, neither system was tested with either simulated noise or fading. The results of the software simulation did show that for a 16 bit processor architecture, the demodulator processing should not significantly degrade the overall system performance. This was confirmed by preliminary results of the real-time implementation. Direct comparisons of digital filter frequency responses between the simulation and the hardware indicated little difference in both magnitude and phase. As a result, the increase in complexity for floating point arithmetic processing is not considered an acceptable alternative. The same reasoning applies to any discrete hardware approach. The TMS320 provides sufficient processing power and the shortest critical path time in system development.

The additional processing required by the subcarrier demodulator, the remodulation and phase estimation processes, do not appear to impact the system performance and are readily implementable in the DSP chip. The simulations show that the subcarrier phase estimation loop acquires synchronization rapidly, as would be expected from a first order loop, and, consequently, would have little impact on the system throughput.

Given the RF channel allocation and eventual data rate of 4.8 kbps in 5 kHz, it would appear that neither Manchester nor the subcarrier techniques offer a viable solution. Even with expected performance gain of the subcarrier technique, it is clear that the system is very wasteful in terms of bandwidth and as a result requires excessively large M-ary signalling schemes for data transmission.

A potential candidate TCT scheme which approaches the system bandwidth goals is the dual-pilot method proposed by General Electric [8], and subsequently analyzed by Simon [9]. In this scheme, the bandwidth requirements can be reduced by a factor of two, however, there is a power performance penalty incurred due to the use of two pilots. This penalty may tend to ultimately

balance out the performances of the single and dual pilot schemes.

The dual-pilot scheme is slightly more complicated than either single pilot scheme but is still amenable to digital implementation using similar techniques to those developed during this program. Consequently, this scheme would be a worthwhile subject for future work in an attempt to derive the optimum TCT transceiver for the satellite fading mobile communication link.

## 6. REFERENCES

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- [2] F. Davarian, "High Performance Communication in Mobile Channels", IEEE 34th Vehicular Technology Conference, Pittsburgh, Pa. Session C5, May 1984.
- [3] J. McGeehan, A. Bateman, "Theoretical and Experimental Investigation of Feedforward Signal Regeneration", IEEE Trans. Vehicular Technology, Vol. VT-32, pp. 106-120, Feb. 1983.
- [4] F. Davarian, M. Simon, J. Sumida, "DMSK: A Practical 2400 bps Satellite Receiver for Mobile Satellite Service", JPL Publication 85-51, MSAT-X Report No. 111, June 15, 1985.
- [5] General Electric Corporate Research and Development, "An Additional Study and Implementation of Tone Calibrated Technique of Modulation - First Interim Report", Prepared for JPL Contract No. 957190, August 1985.
- [6] Jet Propulsion Lab, "Baseband Implementation of a Tone Calibrated Receiver", Exhibit I, JPL Contract No. 957190, June 1985.

- [7] General Electric Corporate Research and Development, "An Additional Study and Implementation of Tone Calibrated Technique of Modulation - Second Interim Report", Prepared for JPL Contract No. 957190, August 1985.
  
- [8] General Electric Corporate Research and Development, "Design of a MSAT-X Mobile Transceiver and Related Ground Segment Technology", Technical Proposal to JPL, GE No. 1C-6-0357-215, September 1984.
  
- [9] M. K. Simon, "Dual Pilot Tone Calibration Technique (DPTCT)", Internal JPL Document.



## APPENDIX I

### TMS320 BANDPASS FILTER SOFTWARE

```

0001          ICT      "BPF"
0002          *****
0003          *
0004          *      SOFTWARE FOR BOARD 1 OF THE REAL TIME
0005          *      IMPLEMENTATION OF THE MANCHESTER TCT
0006          *      DEMODULATOR
0007          *
0008          *      Written by - Norman E. Lay
0009          *      Last Updated : 8/30/85
0010          *
0011          *      General Electric Company
0012          *      Corporate Research & Development
0013          *      Schenectady, N.Y.
0014          *
0015          *-----*
0016          *
0017          *      The following TMS-320 assembler code
0018          *      implements a bandpass filter at a samp-
0019          *      ling frequency of 48kHz with a center
0020          *      frequency of 12kHz and a passband width
0021          *      of 3.6kHz. Additional overhead functions
0022          *      are also performed, including decimation
0023          *      by 4:1 (data) and by 20:1 (pilot) and de-
0024          *      lay equalization to compensate for the
0025          *      pilot lowpass filter in the demodulator.
0026          *      The output of this board will be 2 12kHz
0027          *      data streams, 2 2.4kHz pilot streams and
0028          *      a synchronization pulse to align the pilot
0029          *      and data streams.
0030          *
0031          *-----*
0032          *
0033          0000 INPUT EQU >0 )
0034          0001 Z1 EQU >1 ) Beginning of Ram
0035          0002 Z2 EQU >2 ) for Delay Storage
0036          0003 Z3 EQU >3 )
0037          0004 Z4 EQU >4 )
0038          0005 Z5 EQU >5 )
0039          0006 Z6 EQU >6 )
0040          0007 Z7 EQU >7 )
0041          0008 Z8 EQU >8 )
0042          0009 Z9 EQU >9 )
0043          000A Z10 EQU >A )
0044          000B Z11 EQU >B )
0045          000C Z12 EQU >C )
0046          000D Z13 EQU >D )
0047          000E Z14 EQU >E )
0048          000F Z15 EQU >F )
0049          0010 Z16 EQU >10 )
0050          0011 Z17 EQU >11 )
0051          0012 Z18 EQU >12 )
0052          0013 Z19 EQU >13 )
0053          0014 Z20 EQU >14 )
0054          0015 Z21 EQU >15 )
0055          0016 Z22 EQU >16 )
0056          0017 Z23 EQU >17 )
0057          0018 Z24 EQU >18 )

```

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0058 0019 225 EQU >19 )  
0059 001A 226 EQU >1A )  
0060 001B 227 EQU >1B )  
0061 001C 228 EQU >1C )  
0062 001D 229 EQU >1D ) End of Ram for  
0063 001E 230 EQU >1E ) Delay Storage  
0064 \*  
0065 001F TAP2 EQU >1F ) Beginning of Ram  
0066 0020 TAP4 EQU >20 ) Storage for Coeffs.  
0067 0021 TAP6 EQU >21 )  
0068 0022 TAP8 EQU >22 )  
0069 0023 TAP10 EQU >23 )  
0070 0024 TAP12 EQU >24 )  
0071 0025 TAP14 EQU >25 ) Half of the filters  
0072 0026 TAP16 EQU >26 ) coefficients are  
0073 0027 TAP18 EQU >27 ) coded as zeros  
0074 0028 TAP20 EQU >28 )  
0075 0029 TAP22 EQU >29 )  
0076 002A TAP24 EQU >2A )  
0077 002B TAP26 EQU >2B )  
0078 002C TAP28 EQU >2C ) End of Ram Storage  
0079 002D TAP30 EQU >2D ) for Coefficients  
0080 \*  
0081 003E BPF1 EQU >3E ) Input Buffer to  
0082 003F BPF2 EQU >3F ) Delay.  
0083 0040 PILOT2 EQU >40 )  
0084 0041 PILOT1 EQU >41 ) Output Buffers to 2nd  
0085 0042 CBPF1 EQU >42 ) Demodulator Board  
0086 0043 CBPF2 EQU >43 )  
0087 0044 TWC EQU >44 ) Constants = 1,2  
0088 0045 CNE EQU >45 )  
0089 0046 OUTFLG EQU >46 ) Decimation and Sync.  
0090 0047 SNCF LG EQU >47 ) Flags  
0091 0048 CLYACK EQU >48 ) External Ram Address Pointer  
0092 0049 DLYBEG EQU >49 )  
0093 004A FIFOND EQU >4A ) Stored Address Constants  
0094 \*  
0095 007E IACH EQU >7E ) Accumulator Storage  
0096 007F IACL EQU >7F ) During an Interrupt  
0097 \*  
0098 0340 CLYSIZ EQU >340 ) MPYK Constant  
0099 0200 BUF8EG EQU >200 ) Definitions  
0100 0400 CDEFFS EQU >400 )  
0101 \*  
0102 \* Begin TMS-320 Code  
0103 \*  
0104 0000 ADRG >0  
0105 \*  
0106 0000 F900 B BOOT  
0001 0700  
0107 \*  
0108 \* Begin Interrupt Routine  
0109 \*  
0110 0002 4000 INTRPT IN INPUT,0  
0111 0003 587E SACH IACH ) Store only the  
0112 0004 507F SACL IACL ) accumulator.  
0113 0005 693E DMQV BPF1

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0114      *
0115      *      Begin 31-tap FIR BPF
0116      *
0117      *      Only 15 multiplies are
0118      *      needed because 16 of
0119      *      the coefficients are
0120      *      coded as zeros.
0121      *
0122 0006 7F89      ZAC
0123 0007 6A10      LT      Z29
0124 0008 6D2D      MPY      TAP30
0125 0009 691C      DMOV      Z28
0126 000A 6B18      LTD      Z27
0127 000B 6D2C      MPY      TAP28
0128 000C 691A      DMOV      Z26
0129 000C 6B19      LTD      Z25
0130 000E 6D28      MPY      TAP26
0131 000F 6918      DMOV      Z24
0132 0010 6B17      LTD      Z23
0133 0011 6D2A      MPY      TAP24
0134 0012 6916      DMOV      Z22
0135 0013 6B15      LTD      Z21
0136 0014 6D29      MPY      TAP22
0137 0015 6914      DMOV      Z20
0138 0016 6B13      LTD      Z19
0139 0017 6D28      MPY      TAP20
0140 0018 6912      DMOV      Z18
0141 0019 6B11      LTD      Z17
0142 001A 6D27      MPY      TAP18
0143 001B 6910      DMOV      Z16
0144 001C 6B0F      LTD      Z15
0145 001D 6D26      MPY      TAP16
0146 001E 690E      DMOV      Z14
0147 001F 6B0D      LTD      Z13
0148 0020 6D25      MPY      TAP14
0149 0021 690C      DMOV      Z12
0150 0022 6B0B      LTD      Z11
0151 0023 6D24      MPY      TAP12
0152 0024 690A      DMOV      Z10
0153 0025 6B09      LTD      Z9
0154 0026 6D23      MPY      TAP10
0155 0027 6908      DMOV      Z8
0156 0028 6B07      LTD      Z7
0157 0029 6D22      MPY      TAP8
0158 002A 6906      DMOV      Z6
0159 002B 6B05      LTD      Z5
0160 002C 6D21      MPY      TAP6
0161 002D 6904      DMOV      Z4
0162 002E 6B03      LTD      Z3
0163 002F 6D20      MPY      TAP4
0164 0030 6902      DMOV      Z2
0165 0031 6B01      LTD      Z1
0166 0032 6D1F      MPY      TAP2
0167 0033 6B00      LTD      INPUT
0168 0034 0F45      ACD      ONE,15
0169 0035 5B3E      SACH      BPF1,0
0170      *

```

ORIGINAL PAGE IS  
OF POOR QUALITY

) Add for roundoff.

```

0171      *      End of BPF Code
0172      *
0173 0036
0174 0036 6880  CONT  LARP  0
0175 0037 F400      BANZ  RETURN
      0038 0043
0176 0039 7003      LARK  0,3
0177 003A 6945      DMOV  ONE          } Set OUTFLG.
0178      *
0179 0038 6881      LARP  1
0180 003C F400      BANZ  RETURN
      003D 0043
0181 003E 7104      LARK  1,4
0182 003F 693F      DMOV  BPF2
0183 0040 203E      LAC   BPF1
0184 0041 5041      SACL  PILOT1
0185 0042 6946      DMOV  OUTFLG          } Set SNCFLG.
0186      *
0187      *      Restore Accumulator for
0188      *      Return from Interrupt
0189      *
0190 0043 657E  RETURN ZALH  IACH
0191 0044 617F      ACDS  IACL
0192 0045 7F82      EINT
0193 0046 7F8D      RET
0194      *
0195      *      Start of Non-Interrupt Code for
0196      *      Modifying Delay Buffer Pointers
0197      *      and Transmitting Data to Main
0198      *      Processing Board.
0199      *
0200 0047 2046  WAIT  LAC   OUTFLG          } Test for time to send.
0201 0048 FF00      BZ    WAIT
      0049 0047
0202 004A 2048      LAC   DLYADX
0203 004B 6742      TBLR  DBPF1          }
0204 004C 7D3E      TBLW  BPF1          } Read in delayed data
0205 004D 0045      ADD   ONE          } and read out present
0206 004E 6743      TBLR  DBPF2          } filter output.
0207 004F 7D3F      TBLW  BPF2          }
0208 0050 0045      ADD   ONE
0209 0051 5048      SACL  DLYADX
0210      *
0211 0052 7F89      ZAC
0212 0053 5046      SACL  OUTFLG          } Clear flag.
0213 0054 2047      LAC   SNCFLG          } Test for time to send
0214 0055 FF00      BZ    NOSYNC          } pilot.
      0056 005E
0215      *
0216 0057 4B47      OUT   SNCFLG,3          }
0217 0058 4F42      OUT   DBPF1,7          } Output pilot/data
0218 0059 4E41      OUT   PILOT1,6          } sync, data & pilot
0219 005A 4D43      OUT   DBPF2,5          } streams.
0220 005B 4C40      OUT   PILOT2,4          }
0221 005C F900      B     MODPTR
      005D 0060
0222      *

```

```

0223 005E 4F42 NOSYNC OUT DBPF1,7      ) Output only data
0224 005F 4D43      OUT DBPF2,5      ) streams.
0225 *
0226 0060 2048 MOCPTR LAC DLYADX      ) Wrap delay buffer
0227 0061 104A      SUB FIFOND      ) pointer if needed.
0228 0062 FE00      BNZ WAIT
      0063 0047
0229 *
0230 0064 2049      LAC DLYBEG
0231 0065 5048      SACL DLYADX
0232 0066 F900      B WAIT
      0067 0047
0233 *
0234 *      Reset Code for Initialization
0235 *      of Constants and Pointers
0236 *
0237 0068 7F81 RESET DINT
0238 0069 6E00      LDPK 0
0239 006A 4000      IN 0,0
0240 006E 7F8B      SOVM
0241 006C 707F      LARK 0,>7F
0242 006D 6880      LARP 0
0243 006E 7F89      ZAC
0244 006F 5088 CLRRAM SACL *      ) Zero internal
0245 0070 F400      BANZ CLRRAM      ) ram.
      0071 006F
0246 0072 7E01      LACK >1
0247 0073 5045      SACL ONE      )
0248 0074 6A45      LT ONE      )
0249 0075 8340      MPYK DLYSIZ      )
0250 0076 7F8E      PAC      ) Store constants.
0251 0077 504A      SACL FIFOND      )
0252 0078 8200      MPYK BUFBEG      )
0253 0079 7F8E      PAC      )
0254 007A 5049      SACL DLYBEG      )
0255 *
0256 007B 8400      MPYK CGEFS
0257 007C 7F8E      PAC
0258 007D 700E      LARK 0,14
0259 007E 711F      LARK 1,>1F
0260 007F 6881 LOAD LARP 1      ) Load BPF
0261 0080 67A0      TBLR *+,0      ) coefficients.
0262 0081 0045      ADD ONE
0263 0082 F400      BANZ LOAD
      0083 007F
0264 *
0265 0084 7003      LARK 0,3      ) Initialize
0266 0085 7104      LARK 1,4      ) AR's.
0267 *
0268 0086 7F82      EINT
0269 0087 F900      B WAIT
      0088 0047
0270 *
0271 *      Filter Coefficients for 48kHz BPF
0272 *      Coded into 16 bits.
0273 *
0274 0400      AORG >400

```

```

0275      *
0276 0400 FFDE      DATA      -34,-775,1994,-1980,-1551,8822,-16544,19888
      0401 FCF9
      0402 07CA
      0403 F844
      0404 F9F1
      0405 2276
      0406 BF60
      0407 4D80
0277 0408 BF60      DATA      -16544,8822,-1551,-1980,1994,-775,-34
      0409 2276
      040A F9F1
      040B F844
      040C 07CA
      040D FCF9
      040E FFDE
0278      *
0279      *      Boot Routine for Loading Program
0280      *      Memory from EPROM to RAM
0281      *
0282 0700      AORG      >700
0283      *
0284 0700 7E01      BOOT   LACK      >1
0285 0701 5000      SACL     >0
0286 0702 6A00      LT       >0
0287 0703 87FF      MPYK     >7FF
0288 0704 7F8E      PAC
0289 0705 670A      NOTDUN  TBLR     >A
0290 0706 7D0A      TBLW     >A
0291 0707 1000      SUB       >0
0292 0708 FD00      BGEZ     NOTDUN
      0709 0705
0293 070A 8068      MPYK     RESET
0294 070B 7F8E      PAC
0295 070C 500A      SACL     >A
0296 070D 7E01      LACK     >1
0297 070E 7D0A      TBLW     >A
0298 070F F900      B         RESET
      0710 0068
0299      *
0300      END
NO ERRORS, NO WARNINGS

```

## APPENDIX II

TMS320 MCTT PREMODULATION PROCESSING SOFTWARE



```

0001          IDT      "MODUL"
0002          *
0003 0000          AORG      >0
0004          *
0005 0000 F900      B          BOOT
          0001 020E
0006          *
0007          *      PROGRAM TO IMPLEMENT TCT TRANSMIT BASEBAND PROCESSING.
0008          *      THIS CONTAINS THE TWO PATHS NEEDED TO
0009          *      IMPLEMENT THE ENTIRE SYSTEM. DATA IS INPUT AS 0 OR 1,
0010          *      IS THEN MANCHESTER ENCODED, RAISED COSINE PULSE SHAPED,
0011          *      AND FINALLY HIGH PASS FILTERED. WE ASSUME HERE THAT
0012          *      DATA IS BEING RECEIVED INTO TRANSMITTER AT 2.4 KBPS.
0013          *      THE DATA IS SPLIT INTO ODD AND EVEN STREAM, AND THEN
0014          *      MANCHESTER ENCODED, SO THE RATE STAYS AT 2.4 KBPS.
0015          *      RAISED COSINE PULSE SHAPING IS DONE USING LAST EIGHT
0016          *      CODE BITS, WITH 4 SAMPLES BEING OUTPUT FOR EACH CODE
0017          *      BIT. THE OUTPUT IS THEREFORE CLOCKING OUT AT 9.6 KPBS,
0018          *      AND A NEW INPUT IS TAKEN ONCE EVERY FOUR OUTPUTS.
0019          *
0020          *      INPUT COEFFICIENTS NEEDED FOR PULSE SHAPING, CLOCK, ETC.
0021          *
0022 0010          AORG      >10
0023          *
0024 0010 0024      C1          DATA      36          * PULSE SHAPING COEFFICIENT P(1)
0025 0011 0058      C2          DATA      91          * P(2)  ALL PULSE SHAPING COEFFICIEN
0026 0012 004C      C3          DATA      76          * P(3)  ARE SCALED BY 16384
0027 0013 000E      C4          DATA      14          * P(4)
0028 0014 0013      C5          DATA      19          * P(5)
0029 0015 00AD      C6          DATA      173         * P(6)
0030 0016 0168      C7          DATA      363         * P(7)
0031 0017 0106      C8          DATA      262         * P(8)
0032 0018 FE61      C9          DATA      -415        * P(9)
0033 0019 FA21      C10         DATA      -1503       * P(10)
0034 001A F776      C11         DATA      -2186       * P(11)
0035 001B FAE9      C12         DATA      -1303       * P(12)
0036 001C 0768      C13         DATA      1899        * P(13)
0037 001D 1B74      C14         DATA      7028        * P(14)
0038 001E 308F      C15         DATA      12431       * P(15)
0039 001F 3E24      C16         DATA      15908       * P(16)
0040 0020 FFFF      C17         DATA      -1          * HOLDS -1 FOR MANCHESTER CODING
0041 0021 8000      C18         DATA      >8000       * BIAS TERM FOR INTERFACE TO BIPOLAR
0042 0022 000A      C19         DATA      10          * AIB BOARD CLOCK PARAMETER
0043 0023 0200      C20         DATA      512         * AIB BOARD CLOCK PARAMETER
0044          *
0045          *      WRITE CONSTANTS TO DATA MEMORY
0046          *
0047          *
0048          *
0049 0024 7F80      RESET      NOP
0050 0025 7F80      NOP
0051 0026 7F81      DINT
0052 0027 7F83      SOVM
0053 0028 6E00      LDPK      0
0054 0029 7E10      LACK      C1          * P(1)
0055 002A 6700      TBLR      0
0056 002B 7E11      LACK      C2          * P(2)

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0057 002C 6701      TBLR      1
0058 002D 7E12      LACK      C3      * P(3)
0059 002E 6702      TBLR      2
0060 002F 7E13      LACK      C4      * P(4)
0061 0030 6703      TBLR      3
0062 0031 7E14      LACK      C5      * P(5)
0063 0032 6704      TBLR      4
0064 0033 7E15      LACK      C6      * P(6)
0065 0034 6705      TBLR      5
0066 0035 7E16      LACK      C7      * P(7)
0067 0036 6706      TBLR      6
0068 0037 7E17      LACK      C8      * P(8)
0069 0038 6707      TBLR      7
0070 0039 7E18      LACK      C9      * P(9)
0071 003A 6708      TBLR      8
0072 003B 7E19      LACK      C10     * P(10)
0073 003C 6709      TBLR      9
0074 003D 7E1A      LACK      C11     * P(11)
0075 003E 670A      TBLR      10
0076 003F 7E1B      LACK      C12     * P(12)
0077 0040 670B      TBLR      11
0078 0041 7E1C      LACK      C13     * P(13)
0079 0042 670C      TBLR      12
0080 0043 7E1D      LACK      C14     * P(14)
0081 0044 670D      TBLR      13
0082 0045 7E1E      LACK      C15     * P(15)
0083 0046 670E      TBLR      14
0084 0047 7E1F      LACK      C16     * P(16)
0085 0048 670F      TBLR      15
0086 0049 6E01      LDPK      1
0087 004A 7E20      LACK      C17     * -1
0088 004B 6705      TBLR      5
0089 004C 7E21      LACK      C18     * BIAS
0090 004D 6706      TBLR      6
0091 004E 7E22      LACK      C19     * CLOCK CONSTANT
0092 004F 6708      TBLR      8
0093 0050 7E23      LACK      C20     * CLOCK CONSTANT
0094 0051 6709      TBLR      9
0095                *
0096 0052 7E00      LACK      0
0097 0053 5003      SACL      3
0098 0054 5004      SACL      4
0099 0055 F900      B          MAN
0056 0057
0100                *
0101                *   MAIN CODE LOOP
0102                *   MANCHESTER CODING SECTION
0103                *
0104                *   CODE ODD BIT.
0105                *
0106 0057 6E01      MAN      LDPK      1
0107 0058 2003      LAC      3          *LOAD ODD DATA BIT INTO ACCUMULATOR
0108 0059 FF00      BZ      ZERO      *BRANCH TO ZERO SECTION IF ZERO
005A 0062
0109                *
0110                *   HERE, A 1 BECOMES -1,1
0111                *

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0112 0058 2005          LAC      5          *LOAD ACCUM. WITH -1
0113 005C 6E00          LDPK      0
0114 005D 5070          SACL     112        *STORE FIRST MANCHESTER BIT,OMB(N) I
0115                      *             HERE, IT WILL BE READY FOR PULSE SH
0116 005E 7E01          LACK      1          *LOAD ACCUM. WITH 1, SECOND MANCHEST
0117 005F 6E01          LDPK      1
0118                      *
0119 0060 F900          B          DONE
      0061 0067
0120                      *
0121                      *   HERE, A 0 BECOMES 1,-1
0122                      *
0123 0062 7E01  ZERO    LACK      1          *LOAD ACCUM. WITH 1
0124 0063 6E00          LDPK      0
0125 0064 5070          SACL     112        *STORE OMB(N) IN 112, WHERE IT WILL
0126 0065 6E01          LDPK      1          *BE USED IMMEDIATELY FOR PULSE SHAPI
0127 0066 2005          LAC      5          *LOAD ACCUM. WITH -1, SECOND MANCHES
0128                      *
0129 0067 5000  DONE    SACL      0          *STORE SECOND MAN. BIT, OMB(N+1) IN
0130                      *             THIS WILL BE USED IN NEXT PULSE SHA
0131                      *
0132                      *   NOW CODE EVEN BIT
0133                      *
0134 0068 2004          LAC      4          *LOAD DATA BIT INTO ACCUMULATOR
0135 0069 FF00          BZ        ZERO1     *BRANCH TO ZERO SECTION IF ZERO
      006A 0072
0136                      *
0137                      *   HERE, A 1 BECOMES -1,1
0138                      *
0139 006B 2005          LAC      5          *LOAD ACCUM. WITH -1
0140 006C 6E00          LDPK      0          *STORE FIRST MANCHESTER BIT,EMB(N) I
0141 006D 5078          SACL     120        *WHERE IT WILL BE USED IMMEDIATELY F
0142 006E 6E01          LDPK      1          *PULSE SHAPING.
0143                      *
0144 006F 7E01          LACK      1          *LOAD ACCUM. WITH 1, SECOND MANCHEST
0145                      *
0146 0070 F900          B          DONE1
      0071 0077
0147                      *
0148                      *   HERE, DATA BIT 0 BECOMES 1,-1
0149                      *
0150 0072 7E01  ZERO1   LACK      1          *LOAD ACCUM. WITH 1
0151 0073 6E00          LDPK      0
0152 0074 5078          SACL     120        *STORE EMB(N) IN 120 FOR PULSE SHAPI
0153 0075 6E01          LDPK      1
0154 0076 2005          LAC      5          *LOAD ACCUM. WITH -1, SECOND MANCHES
0155                      *
0156 0077 5001  DONE1   SACL      1          *STORE SECOND MAN. BIT, EMB(N+1) IN
0157                      *             THIS WILL BE STORED FOR ONE CYCLE.
0158                      *
0159 0078 7E01          LACK      1          *INITIALIZE MAN. BIT COUNTER (MCOUNT
0160 0079 5007          SACL      7          *COUNTER STORE IN 135.
0161                      *
0162                      *   FIND FIRST OF FOUR ODD OUTPUTS CORRESPONDING TO ONE MANCHE
0163                      *   PULSE SHAPING IS DONE CHRONOLOGICALLY. THE LAST EIGHT ODD
0164                      *   OMB(N-7) TO OMB(N), ARE STORED IN DMA'S 112-119, WITH 112
0165                      *   THE MOST RECENT.

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```

0166      *
0167      *
0168 007A 6E00 MAIN1  LDPK  0
0169      *
0170 007B 7F89      ZAC
0171 007C 6A77      LT    119
0172 007D 6D03      MPY   3      * OMB(N-7)*P(4)
0173      *
0174 007E 6C76      LTA   118
0175 007F 6D07      MPY   7      * + OMB(N-6)*P(8)
0176      *
0177 0080 6C75      LTA   117
0178 0081 6D08      MPY   11     * + OMB(N-5)*P(12)
0179      *
0180 0082 6C74      LTA   116
0181 0083 6D0F      MPY   15     * + OMB(N-4)*P(16)
0182      *
0183 0084 6C73      LTA   115
0184 0085 6D0C      MPY   12     * + OMB(N-3)*P(13)
0185      *
0186 0086 6C72      LTA   114
0187 0087 6D08      MPY   8      * + OMB(N-2)*P(9)
0188      *
0189 0088 6C71      LTA   113
0190 0089 6D04      MPY   4      * + OMB(N-1)*P(5)
0191      *
0192 008A 6C70      LTA   112
0193 0088 6D00      MPY   0      * + OMB(N)*P(1)
0194 008C 7F8F      APAC
0195      *
0196 008D 5010      SACL   16     * STORE RESULT, DRC(M), IN DMA 16
0197 008E 7007      LARK   0,7   * STORE FLAG IN AUX0, TO KEEP TRACK
0198      *                               OUTPUT WE'RE ON.
0199 008F 713C      LARK   1,60  * INITIALIZE POINTER AUX1 TO OLDEST
0200      *                               IN ODD FILTER BUFFER FOR HI PASS F
0201      *                               WHICH IS THE NEXT STEP.
0202 0090 6881      LARP   1      * AUX1 POINTER PUT IN USE NOW.
0203      *
0204 0091 F900      B        FILTER * BRANCH TO HIGH PASS FILTER SECTION
0205      *
0206      * NOW DO FIRST EVEN BIT. SAME PULSE SHAPING AS DONE FOR
0207      * PREVIOUS ODD BIT. MANCHESTER BIT BUFFER IS IN DMA'S
0208      * 120-127, WITH 120 HOLDING MOST RECENT BIT.
0209      *
0210 0093 690C SEVEN  DMOV   12     * MOVE ODD OUTPUTS THROUGH DELAY BUFF
0211 0094 6908      DMOV   11     * THIS BUFFER DELAYS ODD OUTPUT BY
0212 0095 690A      DMOV   10     * TWO CLOCK CYCLES.
0213      *
0214 0096 6E00      LDPK   0
0215 0097 7F89      ZAC
0216 0098 6A7F      LT    127
0217 0099 6D03      MPY   3      * EMB(N-7)*P(4)
0218      *
0219 009A 6C7E      LTA   126
0220 009B 6D07      MPY   7      * + EMB(N-6)*P(8)
0221      *

```

```

0222 009C 6C7D      LTA      125
0223 009D 6D0B      MPY      11      * + EMB(N-5)*P(12)
0224                *
0225 009E 6C7C      LTA      124
0226 009F 6D0F      MPY      15      * + EMB(N-4)*P(16)
0227                *
0228 00A0 6C7B      LTA      123
0229 00A1 6D0C      MPY      12      * + EMB(N-3)*P(13)
0230                *
0231 00A2 6C7A      LTA      122
0232 00A3 6D08      MPY      8       * + EMB(N-2)*P(9)
0233                *
0234 00A4 6C79      LTA      121
0235 00A5 6D04      MPY      4       * + EMB(N-1)*P(5)
0236                *
0237 00A6 6C78      LTA      120
0238 00A7 6D00      MPY      0       * + EMB(N)*P(1)
0239 00A8 7F8F      APAC
0240                *
0241 00A9 503D      SACL      61      *STORE RESULT, ERC(N) IN 61
0242 00AA 7006      LARK      0,6    *SET FLAG AUX0 TO MARK OUTPUT WE'RE
0243 00AB 7169      LARK      1,105  *SET POINTER TO LAST ENTRY IN FILTER
0244 00AC 6881      LARP      1      *CHOOSE POINTER.
0245                *
0246 00AD F900      B          FILTER *BRANCH TO HI PASS FILTER SECTION.
0247 00AE 0195
0247                *
0248                *
0249                *
0250 00AF F600      SIX      BIOZ    LOOP2  * WAIT UNTIL READY FOR OUTPUT
0251 0080 00B3
0251 00B1 F900      B          SIX
0251 00B2 00AF
0252                *
0253 00B3 4A0D      LOOP2    OUT      13,2  *OUTPUT DELAYED ODD SAMPLE TO PORT 2
0254 00B4 4B0A      OUT      10,3  *OUTPUT EVEN SAMPLE TO PORT 3.
0255                *
0256 00B5 6E00      LDPK      0
0257 00B6 7F89      ZAC
0258 00B7 6A77      LT        119
0259 00B8 6D02      MPY      2      * OMB(N-7)*P(3)
0260                *
0261 00B9 6C76      LTA      118
0262 003A 6D06      MPY      6      * + OMB(N-6)*P(7)
0263                *
0264 00B8 6C75      LTA      117
0265 00BC 6D0A      MPY      10     * + OMB(N-5)*P(11)
0266                *
0267 00BD 6C74      LTA      116
0268 00BE 6D0E      MPY      14     * + OMB(N-4)*P(15)
0269                *
0270 00BF 6C73      LTA      115
0271 00C0 6D0D      MPY      13     * + OMB(N-3)*P(14)
0272                *
0273 00C1 6C72      LTA      114
0274 00C2 6D09      MPY      9      * + OMB(N-2)*P(10)
0275                *

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0276 00C3 6C71      LTA      113
0277 00C4 6D05      MPY      5      * + OMB(N-1)*P(6)
0278                *
0279 00C5 6C70      LTA      112
0280 00C6 6D01      MPY      1      * + OMB(N)*P(2)
0281 00C7 7F8F      APAC
0282                *
0283 00C8 5010      SACL      16      * STORE RESULT ORC(M) IN DMA 16
0284 00C9 7005      LARK      0,5    *SET FLAG TO MARK OUTPUT.
0285 00CA 713C      LARK      1,60   *SET POINTER TO LAST SPOT IN FILTER
0286 00CB 6881      LARP      1      *CHOOSE POINTER.
0287                *
0288 00CC F900      B          FILTER * BRANCH TO HIGH PASS FILTER.
      00CD 0195
0289                *
0290                * SECOND OUTPUT - EVEN BIT
0291                *
0292 00CE 690C      FIVE      DMOV      12      *SHIFT ODD OUTPUTS THRU DELAY BUFFER
0293 00CF 690B      DMOV      11
0294 00D0 690A      DMOV      10
0295 00D1 6E00      LDPK      0
0296 00D2 7F89      ZAC
0297 00D3 6A7F      LT        127
0298 00D4 6D02      MPY      2      * EMB(N-7)*P(3)
0299                *
0300 00D5 6C7E      LTA      126
0301 00D6 6D06      MPY      6      * + EMB(N-6)*P(7)
0302                *
0303 00D7 6C7D      LTA      125
0304 00D8 6D0A      MPY      10     * + EMB(N-5)*P(11)
0305                *
0306 00D9 6C7C      LTA      124
0307 00DA 6D0E      MPY      14     * + EMB(N-4)*P(15)
0308                *
0309 00DB 6C78      LTA      123
0310 00DC 6D0D      MPY      13     * + EMB(N-3)*P(14)
0311                *
0312 00DD 6C7A      LTA      122
0313 00DE 6D09      MPY      9      * + EMB(N-2)*P(10)
0314                *
0315 00DF 6C79      LTA      121
0316 00E0 6D05      MPY      5      * + EMB(N-1)*P(6)
0317                *
0318 00E1 6C78      LTA      120
0319 00E2 6D01      MPY      1      * + EMB(N)*P(2)
0320 00E3 7F8F      APAC
0321                *
0322 00E4 503D      SACL      61      *STORE EVEN PULSE SAMPLE IN DMA 61
0323 00E5 7004      LARK      0,4    *SET FLAG SO WE KNOW WHERE WE ARE IN
0324 00E6 7169      LARK      1,105  *SET POINTER TO LAST VALUES IN FILTE
0325 00E7 6881      LARP      1      *SELECT POINTER.
0326                *
0327 00E8 F900      B          FILTER *BRANCH TO HI PASS FILTER.
      00E9 0195
0328                *
0329                *
0330                * THIRD OUTPUT OF FOUR ODD OUTPUTS

```

```

0331      *
0332 00EA F600 FOUR      BIOZ      LOOP3      * WAIT UNTIL READY FOR OUTPUT
      00EB 00EE
0333 00EC F900          B          FOUR
      00ED 00EA
0334      *
0335 00EE 4A0D LOOP3      OUT      13,2      *OUTPUT DELAYED ODD SAMPLE TO PORT 2
0336 00EF 4B0A OUT      10,3      *OUTPUT EVEN SAMPLE TO PORT 3.
0337      *
0338 00F0 6E00          LDPK      0
0339 00F1 7F89          ZAC
0340 00F2 6A77          LT      119
0341 00F3 6D01          MPY      1      * OMB(N-7)*P(2)
0342      *
0343 00F4 6C76          LTA      118
0344 00F5 6D05          MPY      5      * + OMB(N-6)*P(6)
0345      *
0346 00F6 6C75          LTA      117
0347 00F7 6D09          MPY      9      * + OMB(N-5)*P(10)
0348      *
0349 00F8 6C74          LTA      116
0350 00F9 6D0D          MPY      13     * + OMB(N-4)*P(14)
0351      *
0352 00FA 6C73          LTA      115
0353 00FB 6D0E          MPY      14     * + OMB(N-3)*P(15)
0354      *
0355 00FC 6C72          LTA      114
0356 00FD 6D0A          MPY      10     * + OMB(N-2)*P(11)
0357      *
0358 00FE 6C71          LTA      113
0359 00FF 6D06          MPY      6      * + OMB(N-1)*P(7)
0360      *
0361 0100 6C70          LTA      112
0362 0101 6D02          MPY      2      * + OMB(N)*P(3)
0363 0102 7F8F          APAC
0364      *
0365 0103 5010          SACL      16     * STORE RESULT ORC(M) IN DMA 16
0366 0104 7003          LARK      0,3   *SET FLAG TO MARK WHERE WE ARE IN PU
0367 0105 713C          LARK      1,60  *SET POINTER TO LAST VALUE IN FILTER
0368 0106 6881          LARP      1     *SELECT POINTER.
0369      *
0370 0107 F900          B          FILTER * BRANCH TO HIGH PASS FILTER
      0108 0195
0371      *
0372      * THIRD OUTPUT OUT OF FOUR EVEN OUTPUTS
0373      *
0374 0109 690C THIRD     DMOV      12     *SHIFT ODD OUTPUTS THRU DELAY BUFFER
0375 010A 6908          DMOV      11
0376 010B 690A          DMOV      10
0377 010C 6E00          LDPK      0
0378 010D 7F89          ZAC
0379 010E 6A7F          LT      127
0380 010F 6D01          MPY      1      * EMB(N-7)*P(2)
0381      *
0382 0110 6C7E          LTA      126
0383 0111 6D05          MPY      5      * + EMB(N-6)*P(6)
0384      *

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```

0385 0112 6C7D      LTA      125
0386 0113 6D09      MPY      9      * + EMB(N-5)*P(10)
0387                *
0388 0114 6C7C      LTA      124
0389 0115 6D0D      MPY      13      * + EMB(N-4)*P(14)
0390                *
0391 0116 6C78      LTA      123
0392 0117 6D0E      MPY      14      * + EMB(N-3)*P(15)
0393                *
0394 0118 6C7A      LTA      122
0395 0119 6D0A      MPY      10      * + EMB(N-2)*P(11)
0396                *
0397 011A 6C79      LTA      121
0398 011B 6D06      MPY      6      * + EMB(N-1)*P(7)
0399                *
0400 011C 6C78      LTA      120
0401 011D 6D02      MPY      2      * + EMB(N)*P(3)
0402 011E 7F8F      APAC
0403                *
0404 011F 503D      SACL      61      *STORE EVEN PULSE SAMPLE IN 61
0405 0120 7002      LARK      0,2      *SET FLAG TO MARK WHERE WE ARE IN PU
0406 0121 7169      LARK      1,105      *SET POINTER TO LAST VALUE IN FILTER
0407 0122 6881      LARP      1      *SELECT POINTER.
0408                *
0409 0123 F900      B          FILTER *BRANCH TO HI PASS FILTER SECTION.
0410 0124 0195
0410                *
0411                *
0412                *      FOURTH ODD OUTPUT OF FOUR.
0413                *
0414 0125 F600      TWO      BICZ      LOOP4      *WAIT UNTIL READY FOR OUTPUT
0415 0126 0129
0416 0127 F900      B          TWO
0417 0128 0125
0416                *
0417 0129 4A0D      LOOP4      OUT      13,2      *OUTPUT DELAYED ODD SAMPLE TO PORT 2
0418 012A 480A      OUT      10,3      *OUTPUT EVEN SAMPLE TO PORT 3.
0419                *
0420 012B 6E00      LDPK      0
0421 012C 7F89      ZAC
0422 012D 6A77      LT      119
0423 012E 6D0D      MPY      0      * OMB(N-7)*P(1)
0424                *
0425 012F 6C76      LTA      118
0426 0130 6D04      MPY      4      * + OMB(N-6)*P(5)
0427                *
0428 0131 6C75      LTA      117
0429 0132 6D08      MPY      8      * + OMB(N-5)*P(9)
0430                *
0431 0133 6C74      LTA      116
0432 0134 6D0C      MPY      12      * + OMB(N-4)*P(13)
0433                *
0434 0135 6C73      LTA      115
0435 0136 6D0F      MPY      15      * + OMB(N-3)*P(16)
0436                *
0437 0137 6C72      LTA      114
0438 0138 6D0B      MPY      11      * + OMB(N-2)*P(12)

```



```

0439      *
0440 0139 6C71      LTA      113
0441 013A 6D07      MPY      7      * + DMB(N-1)*P(8)
0442      *
0443 0138 6C70      LTA      112
0444 013C 6D03      MPY      3      * + DMB(N)*P(4)
0445 013D 7F8F      APAC
0446      *
0447 013E 5010      SACL      16      * STORE RESULT ORC(M) IN DMA 16
0448 013F 7001      LARK      0,1      *SET FLAG TO MARK WHERE WE ARE IN PU
0449 0140 713C      LARK      1,60      *SET POINTER TO LAST VALUE IN FILTER
0450 0141 6881      LARP      1      *SELECT POINTER.
0451      *
0452 0142 F900      B      FILTER      * BRANCH TO HIGH PASS FILTER.
      0143 0195
0453      *
0454      * FOURTH EVEN OUTPUT OUT OF FOUR.
0455      *
0456 0144 690C      ONE      DMOV      12      *SHIFT ODD OUTPUTS THRU DELAY BUFFER
0457 0145 6908      DMOV      11
0458 0146 690A      DMOV      10
0459 0147 6E00      LDPK      0
0460 0148 7F89      ZAC
0461 0149 6A7F      LT      127
0462 014A 6D00      MPY      0      * EMB(N-7)*P(1)
0463      *
0464 0148 6C7E      LTA      126
0465 014C 6D04      MPY      4      * + EMB(N-6)*P(5)
0466      *
0467 014D 6C7D      LTA      125
0468 014E 6D08      MPY      8      * + EMB(N-5)*P(9)
0469      *
0470 014F 6C7C      LTA      124
0471 0150 6D0C      MPY      12      * + EMB(N-4)*P(13)
0472      *
0473 0151 6C78      LTA      123
0474 0152 6D0F      MPY      15      * + EMB(N-3)*P(6)
0475      *
0476 0153 6C7A      LTA      122
0477 0154 6D0B      MPY      11      * + EMB(N-2)*P(12)
0478      *
0479 0155 6C79      LTA      121
0480 0156 6D07      MPY      7      * + EMB(N-1)*P(8)
0481      *
0482 0157 6C78      LTA      120
0483 0158 6D03      MPY      3      * + EMB(N)*P(4)
0484 0159 7F8F      APAC
0485      *
0486 015A 503D      SACL      61      *STORE EVEN SAMPLE ERC(N) IN DMA 61
0487 015B 7000      LARK      0,0      *SET FLAG TO MARK WHERE WE ARE IN PU
0488 015C 7169      LARK      1,105      *SET POINTER TO LAST VALUE IN FILTER
0489 015D 6881      LARP      1      *SELECT POINTER.
0490      *
0491 015E F900      B      FILTER      *BRANCH TO HI PASS FILTER.
      015F 0195
0492      *
0493      *

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0494      * NOW, MOVE INPUT BUFFER TO PREPARE FOR NEXT INCOMING MAN. B
0495      *
0496 0160 6E00      PREP      LDPK      0
0497 0161 6976      DMOV      118      * MOVE FIRST SEVEN VALUES OF MANCHES
0498 0162 6975      DMOV      117      * BIT BUFFERS UP ONE MEMORY LOCATION
0499 0163 6974      DMOV      116      * MAKE ROOM FOR MOST RECENT CODE BIT
0500 0164 6973      DMOV      115      * FOR NEXT PULSE SHAPING SEQUENCE.
0501 0165 6972      DMOV      114
0502 0166 6971      DMOV      113
0503 0167 6970      DMOV      112
0504 0168 697E      DMOV      126
0505 0169 697D      DMOV      125
0506 016A 697C      DMOV      124
0507 016B 6978      DMOV      123
0508 016C 697A      DMOV      122
0509 016D 6979      DMOV      121
0510 016E 6978      DMOV      120
0511      *
0512      *
0513      * WE ARE READY FOR NEXT ITERATION OF FOUR OUTPUTS CORRESPON
0514      * TO NEXT MANCHESTER BIT. CHECK COUNTER TO SEE IF WE NEED N
0515      * DATA BIT.
0516      *
0517 016F 6E01      LDPK      1
0518 0170 2007      LAC      7      *CHECK MCOUNT. ADD -1 TO COUNTER.
0519 0171 0005      ADD      5      * STORE RESULT AS MCOUNT
0520 0172 5007      SACL      7
0521      *
0522      * IF WE HAVE LOOPED ONCE, WE NEED TO LOAD SECOND MAN. BIT.
0523      * IF WE HAVE LOOPED TWICE, WE NEED TO INPUT A NEW DATA BIT.
0524      *
0525 0173 FF00      BZ      LOAD      *IF MCOUNT IS NOW ZERO, WE HAVE MOST
0526      0174 0181      RECENT MAN. BITS ALREADY,
0527      * SO SKIP FOLLOWING INPUT SEQUENCE
0528      *
0529 0175 F600      WAIT5     BIOZ      LOOPS      * WAIT FOR CLOCK
0530      0176 0179      B      WAIT5
0531      0177 F900
0532      0178 0175      *
0533 0179 4A0D      LOOPS5     OUT      13,2      * OUTPUT DELAYED ODD SAMPLE TO PORT 2
0534 017A 4B0A      OUT      10,3      * OUTPUT EVEN SAMPLE TO PORT 3.
0535      *
0536 017B 4104      IN      4,1      * INPUT NEXT EVEN DATA BIT FROM PORT
0537 017C 7E01      LACK      1
0538 017D 7904      AND      4      * AND WITH +1 TO OBTAIN 0 OR 1 FOR D
0539 017E 5004      SACL      4      * STORE DATA BIT IN DMA 132.
0540      *
0541 017F F900      B      MAN      * BRANCH TO MANCHESTER CODING SECTIO
0542      0180 0057
0543      *
0544      * IF ZERO, THEN LOAD NEXT MANCHESTER BITS INTO BUFFER,
0545      * INPUT NEXT ODD DATA BIT,
0546      * AND LOOP BACK TO BEGIN PULSE SHAPING AGAIN.
0547      *
0548 0181 2000      LOAD      LAC      0      * MOVE DM5(N+1) TO DMA 112

```

```

0547 0182 6E00      LDPK      0      * WHERE IT WILL BE READY FOR
0548 0183 5070      SACL      112    * NEXT PASS THRU PULSE SHAPING.
0549 0184 6E01      LDPK      1
0550 0185 2001      LAC        1      * MOVE EMB(N+1) TO DMA 120
0551 0186 6E00      LDPK      0      * WHERE IT WILL BE READY FOR
0552 0187 5078      SACL      120    * NEXT PASS THRU PULSE SHAPING.
0553 0188 6E01      LDPK      1
0554
0555 0189 F600      * WAIT6      BIODZ  LOOP6  * WAIT FOR CLOCK
      018A 018D
0556 0188 F900      B          WAIT6
      018C 0189
0557
0558 018D 4A0D      * LOOP6      OUT      13,2  * OUTPUT DELAYED ODD SAMPLE TO PORT 2
0559 018E 480A      OUT      10,3  * OUTPUT EVEN SAMPLE TO PORT 3
0560
0561 018F 4103      *          IN      3,1  * INPUT FROM PORT 1.
0562 0190 7E01      LACK      1
0563 0191 7903      AND      3      * AND WITH 1 TO PRODUCE A 1 OR A 0.
0564 0192 5003      SACL      3      * STORE RESULTING DATA BIT IN DMA 131
0565
0566 0193 F900      *          B          MAIN1  * BRANCH TO BEGINNING OF PULSE SHAPI
      0194 007A
0567
0568
0569
0570
0571
0572
0573
0574
0575
0576
0577 0195 7F89      * FILTER      ZAC
0578 0196 6A98      LT          *-
0579 0197 9F8D      MPYK      -115    * RC(M-44)*-115
0580
0581 0198 6898      *          LTD      *-
0582 0199 9FD2      MPYK      -34      * + RC(M-43)*-34
0583
0584 019A 6898      *          LTD      *-
0585 019B 9FD9      MPYK      -39      * + RC(M-42)*-39
0586
0587 019C 6898      *          LTD      *-
0588 019D 9FD5      MPYK      -43      * + RC(M-41)*-43
0589
0590 019E 6898      *          LTD      *-
0591 019F 9FD0      MPYK      -48      * + RC(M-40)*-48
0592
0593 01A0 6898      *          LTD      *-
0594 01A1 9FC8      MPYK      -53      * + RC(M-39)*-53
0595
0596 01A2 6898      *          LTD      *-
0597 01A3 9FC6      MPYK      -58      * + RC(M-38)*-58
0598
0599 01A4 6898      *          LTD      *-
0600 01A5 9FC1      MPYK      -63      * + RC(M-37)*-63

```

0601		*			
0602	01A6 6898		LTD	*-	
0603	01A7 9FBC		MPYK	-68	* + RC(M-36)*-68
0604		*			
0605	01A8 6898		LTD	*-	
0606	01A9 9FB7		MPYK	-73	* + RC(M-35)*-73
0607		*			
0608	01AA 6898		LTD	*-	
0609	01AB 9FB2		MPYK	-78	* + RC(M-34)*-78
0610		*			
0611	01AC 6898		LTD	*-	
0612	01AD 9FAD		MPYK	-83	* + RC(M-33)*-83
0613		*			
0614	01AE 6898		LTD	*-	
0615	01AF 9FA9		MPYK	-87	* + RC(M-32)*-87
0616		*			
0617	01B0 6898		LTD	*-	
0618	01B1 9FA4		MPYK	-92	* + RC(M-31)*-92
0619		*			
0620	01B2 6898		LTD	*-	
0621	01B3 9FA1		MPYK	-95	* + RC(M-30)*-95
0622		*			
0623	01B4 6898		LTD	*-	
0624	01B5 9F9D		MPYK	-99	* + RC(M-29)*-99
0625		*			
0626	01B6 6898		LTD	*-	
0627	01B7 9F9A		MPYK	-102	* + RC(M-28)*-102
0628		*			
0629	01B8 6898		LTD	*-	
0630	01B9 9F98		MPYK	-104	* + RC(M-27)*-104
0631		*			
0632	01BA 6898		LTD	*-	
0633	01BB 9F95		MPYK	-107	* + RC(M-26)*-107
0634		*			
0635	01BC 6898		LTD	*-	
0636	01BD 9F93		MPYK	-109	* + RC(M-25)*-109
0637		*			
0638	01BE 6898		LTD	*-	
0639	01BF 9F92		MPYK	-110	* + RC(M-24)*-110
0640		*			
0641	01C0 6898		LTD	*-	
0642	01C1 9F91		MPYK	-111	* + RC(M-23)*-111
0643		*			
0644	01C2 6898		LTD	*-	
0645	01C3 8F91		MPYK	3985	* + RC(M-22)*3985
0646		*			
0647	01C4 6898		LTD	*-	
0648	01C5 9F91		MPYK	-111	* + RC(M-21)*-111
0649		*			
0650	01C6 6898		LTD	*-	
0651	01C7 9F92		MPYK	-110	* + RC(M-20)*-110
0652		*			
0653	01C8 6898		LTD	*-	
0654	01C9 9F93		MPYK	-109	* + RC(M-19)*-109
0655		*			
0656	01CA 6898		LTD	*-	
0657	01CB 9F95		MPYK	-107	* + RC(M-18)*-107

0658		*			
0659	01CC 6898		LTD	*-	
0660	01CD 9F98		MPYK	-104	* + RC(M-17)*-104
0661		*			
0662	01CE 6898		LTD	*-	
0663	01CF 9F9A		MPYK	-102	* + RC(M-16)*-102
0664		*			
0665	01D0 6898		LTD	*-	
0666	01D1 9F9D		MPYK	-99	* + RC(M-15)*-99
0667		*			
0668	01D2 6898		LTD	*-	
0669	01D3 9FA1		MPYK	-95	* + RC(M-14)*-95
0670		*			
0671	01D4 6898		LTD	*-	
0672	01D5 9FA4		MPYK	-92	* + RC(M-13)*-92
0673		*			
0674	01D6 6898		LTD	*-	
0675	01D7 9FA9		MPYK	-87	* + RC(M-12)*-87
0676		*			
0677	01D8 6898		LTD	*-	
0678	01D9 9FAD		MPYK	-83	* + RC(M-11)*-83
0679		*			
0680	01DA 6898		LTD	*-	
0681	01DB 9FB2		MPYK	-78	* + RC(M-10)*-78
0682		*			
0683	01DC 6898		LTD	*-	
0684	01DD 9FB7		MPYK	-73	* + RC(M-9)*-73
0685		*			
0686	01DE 6898		LTD	*-	
0687	01DF 9FBC		MPYK	-68	* + RC(M-8)*-68
0688		*			
0689	01E0 6898		LTD	*-	
0690	01E1 9FC1		MPYK	-63	* + RC(M-7)*-63
0691		*			
0692	01E2 6898		LTD	*-	
0693	01E3 9FC6		MPYK	-58	* + RC(M-6)*-58
0694		*			
0695	01E4 6898		LTD	*-	
0696	01E5 9FC8		MPYK	-53	* + RC(M-5)*-53
0697		*			
0698	01E6 6898		LTD	*-	
0699	01E7 9FD0		MPYK	-48	* + RC(M-4)*-48
0700		*			
0701	01E8 6898		LTD	*-	
0702	01E9 9FD5		MPYK	-43	* + RC(M-3)*-43
0703		*			
0704	01EA 6898		LTD	*-	
0705	01EB 9FD9		MPYK	-39	* + RC(M-2)*-39
0706		*			
0707	01EC 6898		LTD	*-	
0708	01ED 9FDE		MPYK	-34	* + RC(M-1)*-34
0709		*			
0710	01EE 6898		LTD	*-	
0711	01EF 9F8D		MPYK	-115	* + RC(M)*-115
0712	01F0 7F8F		APAC		
0713		*			
0714	01F1 6E01		LDPK	1	

```
0715 01F2 5C0A          SACH      10,4      *STORE FILTER OUTPUT IN 138
0716                  *              SHIFTED 4 SPOTS TO TAKE INTO ACCOUNT
0717                  *              MULT. OF 13 BIT NO. BY 16 BIT NO.
0718 01F3 200A          LAC        10
0719 01F4 0006          ADD        6          * ADD BIAS TERM TO READY FOR OUTPUT
0720                  *              AND      15
0721 01F5 500A          SACL       10          * STORE FILTER OUT + BIAS IN 138
0722                  *
0723                  *      CHECK OCOUNT TO SEE WHICH OUTPUT WE SHOULD BRANCH BACK
0724                  *
0725 01F6 300E          SAR        0,14
0726 01F7 200E          LAC        14
0727                  *
0728                  * IF ACC. IS ZERO, WE ARE DONE AND READY FOR NEXT ITERATION
0729                  *
0730 01F8 FF00          BZ          PREP
0731 01F9 0160
0732                  *
0732 01FA 0005          ADD        5
0733                  *
0734                  *      IF ZERO NOW, READY FOR FOURTH EVEN OUTPUT
0735                  *
0736 01FB FF00          BZ          ONE
0737 01FC 0144
0738                  *
0738 01FD 0005          ADD        5
0739                  *
0740                  *      IF ZERO, READY FOR FOURTH ODD OUTPUT
0741                  *
0742 01FE FF00          BZ          TWO
0743 01FF 0125
0744                  *
0744 0200 0005          ADD        5
0745                  *
0746                  *      IF ZERO, READY FOR THIRD EVEN OUTPUT
0747                  *
0748 0201 FF00          BZ          THIRD
0749 0202 0109
0750                  *
0750 0203 0005          ADD        5
0751                  *
0752                  *      IF ZERO, READY FOR THIRD ODD OUTPUT
0753                  *
0754 0204 FF00          BZ          FOUR
0755 0205 00EA
0756                  *
0756 0206 0005          ADD        5
0757                  *
0758                  *      IF ZERO, READY FOR SECOND EVEN OUTPUT
0759                  *
0760 0207 FF00          BZ          FIVE
0761 0208 00CE
0762                  *
0762 0209 0005          ADD        5
0763                  *
0764                  *      IF ZERO, READY FOR SECOND ODD OUTPUT
0765                  *
```

```
0766 020A FF00          BZ      SIX
      020B 00AF
0767          *
0768          *   IF ONE, READY FOR FIRST EVEN OUTPUT
0769          *
0770 020C FC00          BGZ     SEVEN
      020D 0093
0771          *
0772          *
0773          *   BOOT ROUTINE FOR LOADING PROGRAM
0774          *   MEMORY FROM EPROM TO RAM
0775          *
0776 020E 7E01  BOOT      LACK      >1
0777 020F 5000          SACL      >0
0778 0210 6A00          LT       >0
0779 0211 8700          MPYK      >700
0780 0212 7F8E          PAC
0781          *
0782 0213 670A  NOTDUN    TBLR      >A
0783 0214 7D0A          TBLW      >A
0784 0215 1000          SUB       >0
0785 0216 FD00          BGEZ     NOTDUN
      0217 0213
0786          *
0787 0218 8024          MPYK      RESET
0788 0219 7F8E          PAC
0789 021A 500A          SACL      >A
0790 021B 7E01          LACK      >1
0791 021C 7D0A          TBLW      >A
0792 021D F900          S        RESET
      021E 0024
0793          *
0794          END
0 ERRORS, NO WARNINGS
```

## APPENDIX III

TMS320 MICT DEMODULATOR PROCESSING SOFTWARE



```
0001          ICT      "DEMPROC"
0002          *****
0003          *
0004          *      SOFTWARE FOR BOARD 2 OF THE REAL TIME
0005          *      IMPLEMENTATION OF THE MANCHESTER TCT
0006          *      DEMODULATOR
0007          *
0008          *      Written by - Norman E. Lay
0009          *      Last Updated : 8/30/85
0010          *
0011          *      General Electric Company
0012          *      Corporate Research & Development
0013          *      Schenectady, N.Y.
0014          *
0015          *-----*
0016          *
0017          *      The following TMS-320 assembler code
0018          *      implements the pilot processing and
0019          *      correction to the data channels of phase
0020          *      irregularities caused by the fading chan-
0021          *      nel. The principal processing intensive
0022          *      functions implemented by this code consist
0023          *      of 4 lowpass filters -- 2 for pilot reco-
0024          *      very in each channel and 2 for filtering
0025          *      excess noise from the data band. The pilot
0026          *      processor consists of determining sine &
0027          *      cosine of the phase angle between the I & Q
0028          *      channels of the recovered pilot. One octant
0029          *      of sine and cosine values are stored as a
0030          *      lookup table in program memory. Linear in-
0031          *      terpolation is used at different processing
0032          *      rate boundaries (i.e. where the pilot is
0033          *      removed from the data and where sin & cos
0034          *      are used to correct for phase errors in the
0035          *      data). The data filters operate at a 12kHz
0036          *      rate and the pilot processing is done at a
0037          *      2.4kHz rate.
0038          *
0039          *-----*
0040          *
0041          *      1st Data Page Ram
0042          *
0043          0000  ILPF  EQU      >0      )
0044          0001  IZ1   EQU      >1      ) Beginning of Ram for
0045          0002  IZ2   EQU      >2      ) Delay Storage of Filter
0046          0003  IZ3   EQU      >3      ) States of the I Channel
0047          0004  IZ4   EQU      >4      )      Data LPF
0048          0005  IZ5   EQU      >5      )      .
0049          0006  IZ6   EQU      >6      )      .
0050          0007  IZ7   EQU      >7      )      .
0051          0008  IZ8   EQU      >8      )      .
0052          0009  IZ9   EQU      >9      )      .
0053          000A  IZ10  EQU      >A      )      .
0054          000B  IZ11  EQU      >B      )      .
0055          000C  IZ12  EQU      >C      )      .
0056          000D  IZ13  EQU      >D      )      .
0057          000E  IZ14  EQU      >E      )      .
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0058	000F	I215	EQU	>F	}	.
0059	0010	I216	EQU	>10	}	.
0060	0011	I217	EQU	>11	}	.
0061	0012	I218	EQU	>12	}	.
0062	0013	I219	EQU	>13	}	.
0063	0014	I220	EQU	>14	}	.
0064	0015	I221	EQU	>15	}	.
0065	0016	I222	EQU	>16	}	.
0066	0017	I223	EQU	>17	}	.
0067	0018	I224	EQU	>18	}	.
0068	0019	I225	EQU	>19	}	.
0069	001A	I226	EQU	>1A	}	.
0070	001B	I227	EQU	>1B	}	.
0071	001C	I228	EQU	>1C	}	.
0072	001D	I229	EQU	>1D	}	.
0073	001E	I230	EQU	>1E	}	.
0074	001F	I231	EQU	>1F	}	.
0075	0020	I232	EQU	>20	}	.
0076	0021	I233	EQU	>21	}	.
0077	0022	I234	EQU	>22	}	.
0078	0023	I235	EQU	>23	}	.
0079	0024	I236	EQU	>24	}	.
0080	0025	I237	EQU	>25	}	.
0081	0026	I238	EQU	>26	}	.
0082	0027	I239	EQU	>27	}	End of I Data LPF
0083	0028	I240	EQU	>28	}	Delay Storage
0084		*				
0085	0029	Q1PF	EQU	>29	}	
0086	002A	Q21	EQU	>2A	}	Beginning of Ram for
0087	002B	Q22	EQU	>2B	}	Delay Storage of Filter
0088	002C	Q23	EQU	>2C	}	States of the Q Channel
0089	002D	Q24	EQU	>2D	}	Data LPF
0090	002E	Q25	EQU	>2E	}	.
0091	002F	Q26	EQU	>2F	}	.
0092	0030	Q27	EQU	>30	}	.
0093	0031	Q28	EQU	>31	}	.
0094	0032	Q29	EQU	>32	}	.
0095	0033	Q210	EQU	>33	}	.
0096	0034	Q211	EQU	>34	}	.
0097	0035	Q212	EQU	>35	}	.
0098	0036	Q213	EQU	>36	}	.
0099	0037	Q214	EQU	>37	}	.
0100	0038	Q215	EQU	>38	}	.
0101	0039	Q216	EQU	>39	}	.
0102	003A	Q217	EQU	>3A	}	.
0103	003B	Q218	EQU	>3B	}	.
0104	003C	Q219	EQU	>3C	}	.
0105	003D	Q220	EQU	>3D	}	.
0106	003E	Q221	EQU	>3E	}	.
0107	003F	Q222	EQU	>3F	}	.
0108	0040	Q223	EQU	>40	}	.
0109	0041	Q224	EQU	>41	}	.
0110	0042	Q225	EQU	>42	}	.
0111	0043	Q226	EQU	>43	}	.
0112	0044	Q227	EQU	>44	}	.
0113	0045	Q228	EQU	>45	}	.
0114	0046	Q229	EQU	>46	}	.

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0115 0047 CZ30 EQU >47 } .  
0116 0048 CZ31 EQU >48 } .  
0117 0049 CZ32 EQU >49 } .  
0118 004A CZ33 EQU >4A } .  
0119 004B CZ34 EQU >4B } .  
0120 004C CZ35 EQU >4C } .  
0121 004D CZ36 EQU >4D } .  
0122 004E CZ37 EQU >4E } .  
0123 004F CZ38 EQU >4F } .  
0124 0050 CZ39 EQU >50 } End of C Data LPF  
0125 0051 CZ40 EQU >51 } Delay Storage  
0126 \*  
0127 0052 IDATA EQU >52 } Ram for storing I & Q  
0128 0053 CDATA EQU >53 } input data  
0129 \*  
0130 0054 IBUFF EQU >54 } Input data buffer to  
0131 0059 CBUFF EQU >59 } permit pilot processing  
0132 \*  
0133 005E SIN EQU >5E } Sine calculation  
0134 005F PRESIN EQU >5F } Save for sine lin. interp.  
0135 0060 GLDSIN EQU >60 } Use as sine in interrupt  
0136 0061 COS EQU >61 } Cosine calculation  
0137 0062 PRECCS EQU >62 } Save for cosine lin. interp.  
0138 0063 GLDCCS EQU >63 } Use as cosine in interrupt  
0139 0064 SINSTP EQU >64 } Sine step size calc.  
0140 0065 OSSTP EQU >65 } Use in intrpt. as step size  
0141 0066 COSSTP EQU >66 } Cosine step size calc.  
0142 0067 CCSTP EQU >67 } Use in intrpt. as step size  
0143 \*  
0144 0068 IPILCT EQU >68 } Input I pilot  
0145 0069 OLDIF EQU >69 } Save for I lin. interp.  
0146 006A DIPIL EQU >6A } Use as I pilot in interrupt  
0147 006B CPILCT EQU >6B } Input Q pilot  
0148 006C OLDQF EQU >6C } Save for Q pilot lin. interp.  
0149 006D OQPIL EQU >6D } Use as Q pilot in intrpt.  
0150 006E IPSTP EQU >6E } I pilot step size calc.  
0151 006F DIPSTP EQU >6F } Use in intrpt. as step size  
0152 0070 QPSTP EQU >70 } Q pilot step size calc.  
0153 0071 OQPSTP EQU >71 } Use in intrpt. as step size  
0154 \*  
0155 0072 ONE EQU >72 } Constant = 5  
0156 0073 SNCFLG EQU >73 } Flag for pilot/data alignment  
0157 0074 TEMP1 EQU >74 } Temp ram used in background  
0158 0075 TEMP2 EQU >75 }  
0159 0076 SINMI EQU >76 } Temp ram used in interrupt  
0160 0077 SINMC EQU >77 }  
0161 0078 IDOUT EQU >78 } I data output  
0162 0079 QDOUT EQU >79 } Q data output  
0163 007A SNQFST EQU >7A } Table offset for stored sine  
0164 007A CSCFST EQU >7A } and cosine values  
0165 007B ISIGN EQU >7B } Temp ram used in background  
0166 007C QSIGN EQU >7C }  
0167 \*  
0168 \* Ram for Saving Registers  
0169 \* During an Interrupt  
0170 \*  
0171 007D IACH EQU >7D } Save high accumulator

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0172	007E	IACL	EQU	>7E	) Save low accumulator	
0173	007F	ITREG	EQU	>7F	) Save T register	
0174		●				
0175		*		Address Constant for Sine		
0176		●		and Cosine Lookup Table		ORIGINAL PAGE IS
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0178	0500	GFFSET	EQU	>500		
0179		*				
0180		*		Data LPF Constants		
0181		*				
0182		●		Only half the coefficients are coded because		
0183		*		the filter is symmetrical.		
0184		*				
0185	FFDB	CLPF1	EQU	-37		
0186	FFE7	DLPF2	EQU	-25		
0187	006C	DLPF3	EQU	103		
0188	FFFF	DLPF4	EQU	-1		
0189	FFD4	DLPF5	EQU	-44		
0190	FFA6	DLPF6	EQU	-90		
0191	FFF8	DLPF7	EQU	-8		
0192	0068	DLPF8	EQU	104		
0193	0078	DLPF9	EQU	120		
0194	FFE0	DLPF10	EQU	-26		
0195	FF44	DLPF11	EQU	-188		
0196	FF67	DLPF12	EQU	-153		
0197	0068	DLPF13	EQU	107		
0198	0144	DLPF14	EQU	324		
0199	00B5	DLPF15	EQU	181		
0200	FEDA	DLPF16	EQU	-294		
0201	FD9E	DLPF17	EQU	-610		
0202	FF38	DLPF18	EQU	-200		
0203	03E9	DLPF19	EQU	1001		
0204	092C	DLPF20	EQU	2348		
0205	0B79	DLPF21	EQU	2937		
0206		*				
0207		*		Pilot LPF Constants		
0208		*				
0209		*		Only half the coefficients are coded because		
0210		*		the filter is symmetrical.		
0211		●				
0212	FF34	PLPF1	EQU	-204		
0213	FFE6	PLPF2	EQU	-26		
0214	FFF6	PLPF3	EQU	-10		
0215	0011	PLPF4	EQU	17		
0216	0036	PLPF5	EQU	54		
0217	0060	PLPF6	EQU	96		
0218	0088	PLPF7	EQU	139		
0219	0080	PLPF8	EQU	176		
0220	00C8	PLPF9	EQU	200		
0221	00C3	PLPF10	EQU	203		
0222	00B4	PLPF11	EQU	180		
0223	0081	PLPF12	EQU	129		
0224	0031	PLPF13	EQU	49		
0225	FFC7	PLPF14	EQU	-57		
0226	FF4D	PLPF15	EQU	-179		
0227	FECD	PLPF16	EQU	-307		
0228	FE57	PLPF17	EQU	-425		

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0229      FDFB      PLPF18 EQU      -517
0230      FJCA      PLPF19 EQU      -566
0231      FDD4      PLPF20 EQU      -556
0232      FE27      PLPF21 EQU      -473
0233      FECA      PLPF22 EQU      -310
0234      FFC1      PLPF23 EQU      -63
0235      0106      PLPF24 EQU      262
0236      028E      PLPF25 EQU      654
0237      0446      PLPF26 EQU      1094
0238      0617      PLPF27 EQU      1559
0239      07E5      PLPF28 EQU      2021
0240      0994      PLPF29 EQU      2452
0241      0B06      PLPF30 EQU      2822
0242      0C23      PLPF31 EQU      3107
0243      0CD6      PLPF32 EQU      3286
0244      0D13      PLPF33 EQU      3347
0245      *
0246      *          Begin TMS-320 Code
0247      *
0248 0000          ACRG      >0
0249      *
0250 0000 F900      B          800T
      0001 0700
0251      *
0252      *          Begin Interrupt Routine
0253      *
0254 0002 587D      INTRPT SACH      IACH          }
0255 0003 507E          SACL      IACL          } Save accumulator
0256 0004 8001          MPYK      >1          } and T register dur-
0257 0005 7F8E          PAC          } ing an interrupt.
0258 0006 507F          SACL      ITREG          }
0259      *
0260 0007 4873          OUT      IDOUT,0          } Output recovered I
0261 0008 4979          OUT      QCDUT,1          } and Q data.
0262 0009 F600          BIDZ      NCSYNC          } Check for time alignment.
      000A 0020
0263      *
0264 000B 6961          DMOV      COS          } Update sin, cos, I pilot
0265 000C 6962          DMOV      PRECOS          } and Q pilot and all cor-
0266 000D 6966          DMOV      CCSSTP          } responding step sizes.
0267 000E 695E          DMOV      SIN          }
0268 000F 695F          DMOV      PRESIN          }
0269 0010 6964          DMOV      SINSTP          }
0270 0011 6968          DMOV      IPILOT          }
0271 0012 6969          DMOV      OLDIP          }
0272 0013 696E          DMOV      IPSTP          }
0273 0014 696B          DMOV      QPILOT          }
0274 0015 696C          DMOV      OLDQP          }
0275 0016 6970          DMOV      QPSTP          } End of Update.
0276      *
0277 0017 6972          DMOV      ONE          } Set SNCFLG.
0278      *
0279 0018 4052          IN      ICATA,0          }
0280 0019 4153          IN      QCATA,1          } Input I & Q pilot and
0281 001A 4268          IN      IPILOT,2          } data streams.
0282 001B 436B          IN      QPILOT,3          }
0283      *

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0284 001C 7054      LARK      0,IBUFF      } Reset processing delay
0285 001C 7159      LARK      1,QBUFF      } buffer pointers.
0286                *
0287 001E F900      B          CONTNU
      001F 002E
0288                *
0289 0020 4052      NOSYNC IN      ICATA,0      } Input I & Q data
0290 0021 4153      IN          QDATA,1      } streams.
0291                *
0292 0022 656A      ZALH      OIPIL
0293 0023 606F      ADDH      OIPSTP      }
0294 0024 586A      SACH      OIPIL      } Update filtered pilot
0295 0025 656D      ZALH      OCPIL      } for linear interpolation.
0296 0026 6071      ADDH      OCPSTP      }
0297 0027 586D      SACH      OCPIL
0298 0028 6563      ZALH      OLDCOS
0299 0029 6067      ADDH      OCSTP      }
0300 002A 5863      SACH      OLDCOS      } Update sin & cos for
0301 002B 656D      ZALH      OLDSIN      } linear interpolation.
0302 002C 6065      ADDH      OSSTP      }
0303 002D 586D      SACH      OLDSIN
0304                *
0305                *      The following section of code
0306                *      implements the equations :
0307                *
0308                *      Zi = Id*cos(phi) + Qd*sin(phi)
0309                *      Zq = Qd*cos(phi) - Id*sin(phi)
0310                *
0311 002E 2088      CONTAU LAC      *          }
0312 002F 106A      SUB      OIPIL      } Remove pilot from I data.
0313 0030 5088      SACL      *          }
0314 0031 6A60      LT      OLDSIN
0315 0032 6D81      MPY      *,1
0316 0033 7F8E      PAC
0317 0034 5976      SACH      SINMI,1
0318 0035 2088      LAC      *          }
0319 0036 106D      SUB      OCPIL      } Remove pilot from Q data.
0320 0037 5088      SACL      *          }
0321 0038 6D80      MPY      *,0
0322 0039 7F8E      PAC
0323 003A 5977      SACH      SINMQ,1
0324 003B 6A63      LT      OLDCOS
0325 003C 6D81      MPY      *,1
0326 003D 7F8E      PAC
0327 003E 0F77      ADD      SINMQ,15
0328 003F 5800      SACH      ILPF,0
0329 0040 6D80      MPY      *,0
0330 0041 7F8E      PAC
0331 0042 1F76      SUB      SINMI,15
0332 0043 5829      SACH      QLPF,0
0333                *
0334 0044 2052      LAC      IDATA
0335 0045 50A1      SACL      **+,0,1      } Store Current Input
0336 0046 2053      LAC      QDATA      } I & Q Data.
0337 0047 50A0      SACL      **+,0,0
0338                *
0339                *      The following two LPFs are for

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```
0340      *      the removal of out of band noise
0341      *      in both the I & Q data channels.
0342      *
0343      *
0344      *      Data LPF Code I Channel
0345      *
0346 0048 7F89      ZAC
0347 0049 6A28      LT      IZ40
0348 004A 9FD8      MPYK      DLPF1
0349 004B 6B27      LTD      IZ39
0350 004C 9FE7      MPYK      DLPF2
0351 004D 6B26      LTD      IZ38
0352 004E 806C      MPYK      DLPF3
0353 004F 6B25      LTD      IZ37
0354 0050 9FFF      MPYK      DLPF4
0355 0051 6B24      LTD      IZ36
0356 0052 9FD4      MPYK      DLPF5
0357 0053 6B23      LTD      IZ35
0358 0054 9FA6      MPYK      DLPF6
0359 0055 6B22      LTD      IZ34
0360 0056 9FF8      MPYK      DLPF7
0361 0057 6B21      LTD      IZ33
0362 0058 806B      MPYK      DLPF8
0363 0059 6B20      LTD      IZ32
0364 005A 8078      MPYK      DLPF9
0365 005B 6B1F      LTD      IZ31
0366 005C 9FE6      MPYK      DLPF10
0367 005D 6B1E      LTD      IZ30
0368 005E 9F44      MPYK      DLPF11
0369 005F 6B1D      LTD      IZ29
0370 0060 9F67      MPYK      DLPF12
0371 0061 6B1C      LTD      IZ28
0372 0062 806B      MPYK      DLPF13
0373 0063 6B1B      LTD      IZ27
0374 0064 8144      MPYK      DLPF14
0375 0065 6B1A      LTD      IZ26
0376 0066 80B5      MPYK      DLPF15
0377 0067 6B19      LTD      IZ25
0378 0068 9EDA      MPYK      DLPF16
0379 0069 6B18      LTD      IZ24
0380 006A 9D9E      MPYK      DLPF17
0381 006B 6B17      LTD      IZ23
0382 006C 9F3B      MPYK      DLPF18
0383 006D 6B16      LTD      IZ22
0384 006E 83E9      MPYK      DLPF19
0385 006F 6B15      LTD      IZ21
0386 0070 832C      MPYK      DLPF20
0387 0071 6B14      LTD      IZ20
0388 0072 8B79      MPYK      DLPF21
0389 0073 6B13      LTD      IZ19
0390 0074 892C      MPYK      DLPF20
0391 0075 6B12      LTD      IZ18
0392 0076 83E9      MPYK      DLPF19
0393 0077 6B11      LTD      IZ17
0394 0078 9F3B      MPYK      DLPF18
0395 0079 6B10      LTD      IZ16
0396 007A 9D9E      MPYK      DLPF17
```

0397	007B	630F	LTD	I215
0398	007C	9EDA	MPYK	DLPF16
0399	007C	620E	LTD	I214
0400	007E	80B5	MPYK	DLPF15
0401	007F	650D	LTD	I213
0402	0080	8144	MPYK	DLPF14
0403	0081	630C	LTD	I212
0404	0082	806B	MPYK	DLPF13
0405	0083	620B	LTD	I211
0406	0084	9F67	MPYK	DLPF12
0407	0085	6B0A	LTD	I210
0408	0086	9F44	MPYK	DLPF11
0409	0087	6309	LTD	I29
0410	0088	9FE6	MPYK	DLPF10
0411	0089	6308	LTD	I28
0412	008A	8078	MPYK	DLPF9
0413	008B	6307	LTD	I27
0414	008C	8063	MPYK	DLPF3
0415	008D	6206	LTD	I26
0416	008E	9FF8	MPYK	DLPF7
0417	008F	6B05	LTD	I25
0418	0090	9FA6	MPYK	DLPF6
0419	0091	6B04	LTD	I24
0420	0092	9FD4	MPYK	DLPF5
0421	0093	6B03	LTD	I23
0422	0094	9FFF	MPYK	DLPF4
0423	0095	6B02	LTD	I22
0424	0096	806C	MPYK	DLPF3
0425	0097	6B01	LTD	I21
0426	0098	9FE7	MPYK	DLPF2
0427	0099	6B00	LTD	ILPF
0428	009A	9FDB	MPYK	DLPF1
0429	009B	7F8F	APAC	
0430	009C	5C78	SACH	ICOUT,4

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Data LPF Code Q Channel

0431			ZAC	
0432			LT	Q240
0433			MPYK	DLPF1
0434	009D	7F89	LTD	Q239
0435	009E	6A51	MPYK	DLPF2
0436	009F	9FD3	LTD	Q238
0437	00A0	6B50	MPYK	Q237
0438	00A1	9FE7	LTD	Q236
0439	00A2	6B4F	MPYK	Q235
0440	00A3	806C	LTD	Q234
0441	00A4	6B4E	MPYK	Q233
0442	00A5	9FFF	LTD	Q232
0443	00A6	6B4D	MPYK	Q231
0444	00A7	9FD4	LTD	
0445	00A8	6B4C	MPYK	
0446	00A9	9FA6	LTD	
0447	00AA	6B4B	MPYK	
0448	00AB	9FF8	LTD	
0449	00AC	6B4A	MPYK	
0450	00AD	806B	LTD	
0451	00AE	6B49	MPYK	
0452	00AF	8078	LTD	
0453	00B0	6B48	MPYK	



0454	0081	9FE6	MPYK	DLPF10
0455	0082	6847	LTD	QZ30
0456	0083	9F44	MPYK	DLPF11
0457	0084	6846	LTD	QZ29
0458	0085	9F67	MPYK	DLPF12
0459	0086	6845	LTD	QZ28
0460	0087	8068	MPYK	DLPF13
0461	0088	6844	LTD	QZ27
0462	0089	8144	MPYK	DLPF14
0463	008A	6843	LTD	QZ26
0464	008B	80B5	MPYK	DLPF15
0465	008C	6842	LTD	QZ25
0466	008C	9EDA	MPYK	DLPF16
0467	008E	6841	LTD	QZ24
0468	008F	9D9E	MPYK	DLPF17
0469	00C0	6840	LTD	QZ23
0470	00C1	9F38	MPYK	DLPF18
0471	00C2	683F	LTD	QZ22
0472	00C3	83E9	MPYK	DLPF19
0473	00C4	683E	LTD	QZ21
0474	00C5	892C	MPYK	DLPF20
0475	00C6	683D	LTD	QZ20
0476	00C7	8879	MPYK	DLPF21
0477	00C8	683C	LTD	QZ19
0478	00C9	892C	MPYK	DLPF20
0479	00CA	683B	LTD	QZ18
0480	00CB	83E9	MPYK	DLPF19
0481	00CC	683A	LTD	QZ17
0482	00CD	9F38	MPYK	DLPF18
0483	00CE	6839	LTD	QZ16
0484	00CF	9D9E	MPYK	DLPF17
0485	00D0	6838	LTD	QZ15
0486	00D1	9EDA	MPYK	DLPF16
0487	00D2	6837	LTD	QZ14
0488	00D3	80B5	MPYK	DLPF15
0489	00D4	6836	LTD	QZ13
0490	00D5	8144	MPYK	DLPF14
0491	00D6	6835	LTD	QZ12
0492	00D7	8068	MPYK	DLPF13
0493	00D8	6834	LTD	QZ11
0494	00D9	9F67	MPYK	DLPF12
0495	00DA	6833	LTD	QZ10
0496	00DB	9F44	MPYK	DLPF11
0497	00DC	6832	LTD	QZ9
0498	00DC	9FE6	MPYK	DLPF10
0499	00DE	6831	LTD	QZ8
0500	00DF	8078	MPYK	DLPF9
0501	00E0	6330	LTD	QZ7
0502	00E1	8068	MPYK	DLPF8
0503	00E2	632F	LTD	QZ6
0504	00E3	9FF8	MPYK	DLPF7
0505	00E4	6B2E	LTD	QZ5
0506	00E5	9FA6	MPYK	DLPF6
0507	00E6	6B2D	LTD	QZ4
0508	00E7	9FD4	MPYK	DLPF5
0509	00E8	6B2C	LTD	QZ3
0510	00E9	9FFF	MPYK	DLPF4

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0511 00EA 682B      LTD      QZ2
0512 00EB 806C      MPYK     DLPPF3
0513 00EC 682A      LTD      QZ1
0514 00ED 9FE7      MPYK     DLPPF2
0515 00EE 6829      LTD      QLPPF
0516 00EF 9FD3      MPYK     DLPPF1
0517 00F0 7F8F      APAC
0518 00F1 5C79      SACH      QDOOUT,4
0519                *
0520                *      Restore Registers
0521                *
0522 00F2 657D      ZALH     IACH
0523 00F3 617E      ADDS     IACL
0524 00F4 6A7F      LT       ITREG
0525                *
0526 00F5 7F82      EINT
0527 00F6 7F8D      RET
0528                *
0529                *      Begin Background Code for
0530                *      Calculation of I & Q Pilot
0531                *      and Sin & Cos Step Sizes.
0532                *      Perform Pilot LPF and Sin &
0533                *      Cos Table Lookup.
0534                *
0535 00F7 2073      BKGRND  LAC      SNCF LG      ) Wait for pilot/data
0536 00F8 FF00      BZ       BKGRND      ) synchronization.
0537                *
0538                *      The following two LPFs are for pilot
0539                *      recovery of the I & Q channel.
0540                *
0541                *      Note : the limited internal memory of the
0542                *      TMS-320 required that the pilot LPF
0543                *      filter states be stored externally;
0544                *      however, TBLW/TBLR instructions carry
0545                *      a 6 cycle overhead for memory access;
0546                *      to lower this overhead penalty, extra
0547                *      ram was added to be accessed through
0548                *      the I/O ports reducing the overhead
0549                *      to 4 cycles; memory addressing is ac-
0550                *      complished by an external counter that
0551                *      is advanced by an OUT ,7 instruction;
0552                *
0553                *      I Pilot LPF Code
0554                *
0555 00FA 7F89      ZAC
0556 00FB 6A68      LT       IPILOT
0557 00FC 9F34      MPYK     PLPF1
0558 00FD 4774      IN       TEMP1,7
0559 00FE 4F68      OUT      IPILOT,7
0560 00FF 6C74      LTA      TEMP1
0561 0100 9FE6      MPYK     PLPF2
0562 0101 4768      IN       IPILOT,7
0563 0102 4F74      OUT      TEMP1,7
0564 0103 6C68      LTA      IPILOT
0565 0104 9FF6      MPYK     PLPF3
0566 0105 4774      IN       TEMP1,7

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0567	0106	4F68	OUT	IPILOT,7
0568	0107	6C74	LTA	TEMP1
0569	0108	8011	MPYK	PLPF4
0570	0109	4768	IN	IPILOT,7
0571	010A	4F74	OUT	TEMP1,7
0572	010B	6C68	LTA	IPILOT
0573	010C	8036	MPYK	PLPF5
0574	010D	4774	IN	TEMP1,7
0575	010E	4F68	OUT	IPILOT,7
0576	010F	6C74	LTA	TEMP1
0577	0110	8060	MPYK	PLPF6
0578	0111	4768	IN	IPILOT,7
0579	0112	4F74	OUT	TEMP1,7
0580	0113	6C68	LTA	IPILOT
0581	0114	8088	MPYK	PLPF7
0582	0115	4774	IN	TEMP1,7
0583	0116	4F68	OUT	IPILOT,7
0584	0117	6C74	LTA	TEMP1
0585	0118	8080	MPYK	PLPF8
0586	0119	4768	IN	IPILOT,7
0587	011A	4F74	OUT	TEMP1,7
0588	011B	6C68	LTA	IPILOT
0589	011C	80C8	MPYK	PLPF9
0590	011D	4774	IN	TEMP1,7
0591	011E	4F68	OUT	IPILOT,7
0592	011F	6C74	LTA	TEMP1
0593	0120	80C8	MPYK	PLPF10
0594	0121	4768	IN	IPILOT,7
0595	0122	4F74	OUT	TEMP1,7
0596	0123	6C68	LTA	IPILOT
0597	0124	80B4	MPYK	PLPF11
0598	0125	4774	IN	TEMP1,7
0599	0126	4F68	OUT	IPILOT,7
0600	0127	6C74	LTA	TEMP1
0601	0128	8081	MPYK	PLPF12
0602	0129	4768	IN	IPILOT,7
0603	012A	4F74	OUT	TEMP1,7
0604	012B	6C68	LTA	IPILOT
0605	012C	8031	MPYK	PLPF13
0606	012D	4774	IN	TEMP1,7
0607	012E	4F68	OUT	IPILOT,7
0608	012F	6C74	LTA	TEMP1
0609	0130	9FC7	MPYK	PLPF14
0610	0131	4768	IN	IPILOT,7
0611	0132	4F74	OUT	TEMP1,7
0612	0133	6C68	LTA	IPILOT
0613	0134	9F4D	MPYK	PLPF15
0614	0135	4774	IN	TEMP1,7
0615	0136	4F68	OUT	IPILOT,7
0616	0137	6C74	LTA	TEMP1
0617	0138	9ECD	MPYK	PLPF16
0618	0139	4768	IN	IPILOT,7
0619	013A	4F74	OUT	TEMP1,7
0620	013B	6C68	LTA	IPILOT
0621	013C	9E57	MPYK	PLPF17
0622	013D	4774	IN	TEMP1,7
0623	013E	4F68	OUT	IPILOT,7

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0624	013F	6C74	LTA	TEMP1
0625	0140	9DF8	MPYK	PLPF18
0626	0141	4768	IN	IPILOT,7
0627	0142	4F74	OUT	TEMP1,7
0628	0143	6C68	LTA	IPILOT
0629	0144	9DCA	MPYK	PLPF19
0630	0145	4774	IN	TEMP1,7
0631	0146	4F68	OUT	IPILOT,7
0632	0147	6C74	LTA	TEMP1
0633	0148	9DD4	MPYK	PLPF20
0634	0149	4768	IN	IPILOT,7
0635	014A	4F74	OUT	TEMP1,7
0636	0148	6C68	LTA	IPILOT
0637	014C	9E27	MPYK	PLPF21
0638	014D	4774	IN	TEMP1,7
0639	014E	4F68	OUT	IPILOT,7
0640	014F	6C74	LTA	TEMP1
0641	0150	9ECA	MPYK	PLPF22
0642	0151	4768	IN	IPILOT,7
0643	0152	4F74	OUT	TEMP1,7
0644	0153	6C68	LTA	IPILOT
0645	0154	9FC1	MPYK	PLPF23
0646	0155	4774	IN	TEMP1,7
0647	0156	4F68	OUT	IPILOT,7
0648	0157	6C74	LTA	TEMP1
0649	0158	8106	MPYK	PLPF24
0650	0159	4768	IN	IPILOT,7
0651	015A	4F74	OUT	TEMP1,7
0652	015B	6C68	LTA	IPILOT
0653	015C	828E	MPYK	PLPF25
0654	015D	4774	IN	TEMP1,7
0655	015E	4F68	OUT	IPILOT,7
0656	015F	6C74	LTA	TEMP1
0657	0160	8446	MPYK	PLPF26
0658	0161	4768	IN	IPILOT,7
0659	0162	4F74	OUT	TEMP1,7
0660	0163	6C68	LTA	IPILOT
0661	0164	8617	MPYK	PLPF27
0662	0165	4774	IN	TEMP1,7
0663	0166	4F68	OUT	IPILOT,7
0664	0167	6C74	LTA	TEMP1
0665	0168	87E5	MPYK	PLPF28
0666	0169	4768	IN	IPILOT,7
0667	016A	4F74	OUT	TEMP1,7
0668	0168	6C68	LTA	IPILOT
0669	016C	8994	MPYK	PLPF29
0670	016D	4774	IN	TEMP1,7
0671	016E	4F68	OUT	IPILOT,7
0672	016F	6C74	LTA	TEMP1
0673	0170	8806	MPYK	PLPF30
0674	0171	4768	IN	IPILOT,7
0675	0172	4F74	OUT	TEMP1,7
0676	0173	6C68	LTA	IPILOT
0677	0174	8C23	MPYK	PLPF31
0678	0175	4774	IN	TEMP1,7
0679	0176	4F68	OUT	IPILOT,7
0680	0177	6C74	LTA	TEMP1

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0681	0178	8CC6	MPYK	PLPF32
0682	0179	4768	IN	IPILOT,7
0683	017A	4F74	OUT	TEMP1,7
0684	017B	6C68	LTA	IPILOT
0685	017C	8D13	MPYK	PLPF33
0686	017D	4774	IN	TEMP1,7
0687	017E	4F68	OUT	IPILOT,7
0688	017F	6C74	LTA	TEMP1
0689	0180	8CC6	MPYK	PLPF32
0690	0181	4768	IN	IPILOT,7
0691	0182	4F74	OUT	TEMP1,7
0692	0183	6C63	LTA	IPILOT
0693	0184	8C23	MPYK	PLPF31
0694	0185	4774	IN	TEMP1,7
0695	0186	4F68	OUT	IPILOT,7
0696	0187	6C74	LTA	TEMP1
0697	0188	8B06	MPYK	PLPF30
0698	0189	4768	IN	IPILOT,7
0699	018A	4F74	OUT	TEMP1,7
0700	018B	6C68	LTA	IPILOT
0701	018C	8994	MPYK	PLPF29
0702	018D	4774	IN	TEMP1,7
0703	018E	4F68	OUT	IPILOT,7
0704	018F	6C74	LTA	TEMP1
0705	0190	87E5	MPYK	PLPF28
0706	0191	4768	IN	IPILOT,7
0707	0192	4F74	OUT	TEMP1,7
0708	0193	6C68	LTA	IPILOT
0709	0194	8617	MPYK	PLPF27
0710	0195	4774	IN	TEMP1,7
0711	0196	4F68	OUT	IPILOT,7
0712	0197	6C74	LTA	TEMP1
0713	0198	8446	MPYK	PLPF26
0714	0199	4768	IN	IPILOT,7
0715	019A	4F74	OUT	TEMP1,7
0716	019B	6C68	LTA	IPILOT
0717	019C	828E	MPYK	PLPF25
0718	019D	4774	IN	TEMP1,7
0719	019E	4F68	OUT	IPILOT,7
0720	019F	6C74	LTA	TEMP1
0721	01A0	8106	MPYK	PLPF24
0722	01A1	4768	IN	IPILOT,7
0723	01A2	4F74	OUT	TEMP1,7
0724	01A3	6C68	LTA	IPILOT
0725	01A4	9FC1	MPYK	PLPF23
0726	01A5	4774	IN	TEMP1,7
0727	01A6	4F68	OUT	IPILOT,7
0728	01A7	6C74	LTA	TEMP1
0729	01A8	9ECA	MPYK	PLPF22
0730	01A9	4768	IN	IPILOT,7
0731	01AA	4F74	OUT	TEMP1,7
0732	01AB	6C68	LTA	IPILOT
0733	01AC	9E27	MPYK	PLPF21
0734	01AD	4774	IN	TEMP1,7
0735	01AE	4F68	OUT	IPILOT,7
0736	01AF	6C74	LTA	TEMP1
0737	01B0	9DD4	MPYK	PLPF20

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0738	0181	4768	IN	IPILOT,7
0739	0182	4F74	OUT	TEMP1,7
0740	0183	6C68	LTA	IPILOT
0741	0184	9DCA	MPYK	PLPF19
0742	0185	4774	IN	TEMP1,7
0743	0136	4F68	OUT	IPILOT,7
0744	0187	6C74	LTA	TEMP1
0745	0138	9DFB	MPYK	PLPF18
0746	0189	4768	IN	IPILOT,7
0747	018A	4F74	OUT	TEMP1,7
0748	018B	6C68	LTA	IPILOT
0749	018C	9E57	MPYK	PLPF17
0750	018D	4774	IN	TEMP1,7
0751	018E	4F68	OUT	IPILOT,7
0752	01BF	6C74	LTA	TEMP1
0753	01C0	9ECD	MPYK	PLPF16
0754	01C1	4768	IN	IPILOT,7
0755	01C2	4F74	OUT	TEMP1,7
0756	01C3	6C68	LTA	IPILOT
0757	01C4	9F4D	MPYK	PLPF15
0758	01C5	4774	IN	TEMP1,7
0759	01C6	4F68	OUT	IPILOT,7
0760	01C7	6C74	LTA	TEMP1
0761	01C8	9FC7	MPYK	PLPF14
0762	01C9	4768	IN	IPILOT,7
0763	01CA	4F74	OUT	TEMP1,7
0764	01CB	6C68	LTA	IPILOT
0765	01CC	8031	MPYK	PLPF13
0766	01CD	4774	IN	TEMP1,7
0767	01CE	4F68	OUT	IPILOT,7
0768	01CF	6C74	LTA	TEMP1
0769	01D0	8081	MPYK	PLPF12
0770	01D1	4768	IN	IPILOT,7
0771	01D2	4F74	OUT	TEMP1,7
0772	01D3	6C68	LTA	IPILOT
0773	01D4	8084	MPYK	PLPF11
0774	01D5	4768	IN	IPILOT,7
0775	01D6	4F68	OUT	IPILOT,7
0776	01D7	6C74	LTA	TEMP1
0777	01D8	80C3	MPYK	PLPF10
0778	01D9	4768	IN	IPILOT,7
0779	01DA	4F68	OUT	IPILOT,7
0780	01DB	6C74	LTA	TEMP1
0781	01DC	80C8	MPYK	PLPF9
0782	01DD	4768	IN	IPILOT,7
0783	01DE	4F68	OUT	IPILOT,7
0784	01DF	6C74	LTA	TEMP1
0785	01E0	8080	MPYK	PLPF8
0786	01E1	4768	IN	IPILOT,7
0787	01E2	4F68	OUT	IPILOT,7
0788	01E3	6C74	LTA	TEMP1
0789	01E4	8083	MPYK	PLPF7
0790	01E5	4768	IN	IPILOT,7
0791	01E6	4F68	OUT	IPILOT,7
0792	01E7	6C74	LTA	TEMP1
0793	01E8	8060	MPYK	PLPF6
0794	01E9	4763	IN	IPILOT,7

0795	01EA	4F69	OUT	IPILJT,7
0796	01EB	6C74	LTA	TEMP1
0797	01EC	8036	MPYK	PLPF5
0798	01ED	4768	IN	IPILJT,7
0799	01EE	4F68	OUT	IPILJT,7
0800	01EF	6C74	LTA	TEMP1
0801	01F0	8011	MPYK	PLPF4
0802	01F1	4768	IN	IPILJT,7
0803	01F2	4F68	OUT	IPILJT,7
0804	01F3	6C74	LTA	TEMP1
0805	01F4	9FF6	MPYK	PLPF3
0806	01F5	4768	IN	IPILJT,7
0807	01F6	4F68	OUT	IPILJT,7
0808	01F7	6C74	LTA	TEMP1
0809	01F8	9FE6	MPYK	PLPF2
0810	01F9	4768	IN	IPILJT,7
0811	01FA	4F68	OUT	IPILJT,7
0812	01FB	6C74	LTA	TEMP1
0813	01FC	9F34	MPYK	PLPF1
0814	01FD	7F8F	APAC	
0815	01FE	5968	SACH	IPILJT,1
0816				
0817				
0818				
0819	01FF	7F89	ZAC	
0820	0200	6A68	LT	QPILOT
0821	0201	9F34	MPYK	PLPF1
0822	0202	4774	IN	TEMP1,7
0823	0203	4F68	OUT	QPILOT,7
0824	0204	6C74	LTA	TEMP1
0825	0205	9FE6	MPYK	PLPF2
0826	0206	4768	IN	QPILOT,7
0827	0207	4F74	OUT	TEMP1,7
0828	0208	6C68	LTA	QPILOT
0829	0209	9FF6	MPYK	PLPF3
0830	020A	4774	IN	TEMP1,7
0831	020B	4F68	OUT	QPILOT,7
0832	020C	6C74	LTA	TEMP1
0833	020D	8011	MPYK	PLPF4
0834	020E	4768	IN	QPILOT,7
0835	020F	4F74	OUT	TEMP1,7
0836	0210	6C68	LTA	QPILOT
0837	0211	8036	MPYK	PLPF5
0838	0212	4774	IN	TEMP1,7
0839	0213	4F68	OUT	QPILOT,7
0840	0214	6C74	LTA	TEMP1
0841	0215	8060	MPYK	PLPF6
0842	0216	4768	IN	QPILOT,7
0843	0217	4F74	OUT	TEMP1,7
0844	0218	6C68	LTA	QPILOT
0845	0219	8088	MPYK	PLPF7
0846	021A	4774	IN	TEMP1,7
0847	021B	4F68	OUT	QPILOT,7
0848	021C	6C74	LTA	TEMP1
0849	021D	8080	MPYK	PLPF8
0850	021E	4768	IN	QPILOT,7
0851	021F	4F74	OUT	TEMP1,7

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0852	0220	6C6B	LTA	QPILOT
0853	0221	80C8	MPYK	PLPF9
0854	0222	4774	IN	TEMP1,7
0855	0223	4F6B	OUT	QPILOT,7
0856	0224	6C74	LTA	TEMP1
0857	0225	80C8	MPYK	PLPF10
0858	0226	476B	IN	QPILOT,7
0859	0227	4F74	OUT	TEMP1,7
0860	0228	6C6B	LTA	QPILOT
0861	0229	80B4	MPYK	PLPF11
0862	022A	4774	IN	TEMP1,7
0863	022B	4F6B	OUT	QPILOT,7
0864	022C	6C74	LTA	TEMP1
0865	022D	8081	MPYK	PLPF12
0866	022E	476B	IN	QPILOT,7
0867	022F	4F74	OUT	TEMP1,7
0868	0230	6C6B	LTA	QPILOT
0869	0231	8031	MPYK	PLPF13
0870	0232	4774	IN	TEMP1,7
0871	0233	4F6B	OUT	QPILOT,7
0872	0234	6C74	LTA	TEMP1
0873	0235	9FC7	MPYK	PLPF14
0874	0236	476B	IN	QPILOT,7
0875	0237	4F74	OUT	TEMP1,7
0876	0238	6C6B	LTA	QPILOT
0877	0239	9F4D	MPYK	PLPF15
0878	023A	4774	IN	TEMP1,7
0879	023B	4F6B	OUT	QPILOT,7
0880	023C	6C74	LTA	TEMP1
0881	023D	9ECD	MPYK	PLPF16
0882	023E	476B	IN	QPILOT,7
0883	023F	4F74	OUT	TEMP1,7
0884	0240	6C6B	LTA	QPILOT
0885	0241	9E57	MPYK	PLPF17
0886	0242	4774	IN	TEMP1,7
0887	0243	4F6B	OUT	QPILOT,7
0888	0244	6C74	LTA	TEMP1
0889	0245	9DF3	MPYK	PLPF18
0890	0246	476B	IN	QPILOT,7
0891	0247	4F74	OUT	TEMP1,7
0892	0248	6C6B	LTA	QPILOT
0893	0249	9DCA	MPYK	PLPF19
0894	024A	4774	IN	TEMP1,7
0895	024B	4F6B	OUT	QPILOT,7
0896	024C	6C74	LTA	TEMP1
0897	024D	9DD4	MPYK	PLPF20
0898	024E	476B	IN	QPILOT,7
0899	024F	4F74	OUT	TEMP1,7
0900	0250	6C6B	LTA	QPILOT
0901	0251	9E27	MPYK	PLPF21
0902	0252	4774	IN	TEMP1,7
0903	0253	4F6B	OUT	QPILOT,7
0904	0254	6C74	LTA	TEMP1
0905	0255	9ECA	MPYK	PLPF22
0906	0256	476B	IN	QPILOT,7
0907	0257	4F74	OUT	TEMP1,7
0908	0258	6C6B	LTA	QPILOT



0909	0259	9FC1	MPYK	PLPF23
0910	025A	4774	IN	TEMP1,7
0911	0258	4F68	OUT	QPILOT,7
0912	025C	6C74	LTA	TEMP1
0913	025D	8106	MPYK	PLPF24
0914	025E	4768	IN	QPILOT,7
0915	025F	4F74	OUT	TEMP1,7
0916	0260	6C63	LTA	QPILOT
0917	0261	828E	MPYK	PLPF25
0918	0262	4774	IN	TEMP1,7
0919	0263	4F68	OUT	QPILOT,7
0920	0264	6C74	LTA	TEMP1
0921	0265	8446	MPYK	PLPF26
0922	0266	4768	IN	QPILOT,7
0923	0267	4F74	OUT	TEMP1,7
0924	0268	6C68	LTA	QPILOT
0925	0269	8617	MPYK	PLPF27
0926	026A	4774	IN	TEMP1,7
0927	0268	4F68	OUT	QPILOT,7
0928	026C	6C74	LTA	TEMP1
0929	026D	87E5	MPYK	PLPF28
0930	026E	4768	IN	QPILOT,7
0931	026F	4F74	OUT	TEMP1,7
0932	0270	6C68	LTA	QPILOT
0933	0271	8994	MPYK	PLPF29
0934	0272	4774	IN	TEMP1,7
0935	0273	4F68	OUT	QPILOT,7
0936	0274	6C74	LTA	TEMP1
0937	0275	8306	MPYK	PLPF30
0938	0276	4768	IN	QPILOT,7
0939	0277	4F74	OUT	TEMP1,7
0940	0278	6C68	LTA	QPILOT
0941	0279	8C23	MPYK	PLPF31
0942	027A	4774	IN	TEMP1,7
0943	027B	4F68	OUT	QPILOT,7
0944	027C	6C74	LTA	TEMP1
0945	027D	8CD6	MPYK	PLPF32
0946	027E	4763	IN	QPILOT,7
0947	027F	4F74	OUT	TEMP1,7
0948	0280	6C68	LTA	QPILOT
0949	0281	8D13	MPYK	PLPF33
0950	0282	4774	IN	TEMP1,7
0951	0283	4F68	OUT	QPILOT,7
0952	0284	6C74	LTA	TEMP1
0953	0285	8CD6	MPYK	PLPF32
0954	0286	4768	IN	QPILOT,7
0955	0287	4F74	OUT	TEMP1,7
0956	0288	6C68	LTA	QPILOT
0957	0289	8C23	MPYK	PLPF31
0958	028A	4774	IN	TEMP1,7
0959	028B	4F68	OUT	QPILOT,7
0960	028C	6C74	LTA	TEMP1
0961	028D	8806	MPYK	PLPF30
0962	028E	4763	IN	QPILOT,7
0963	028F	4F74	OUT	TEMP1,7
0964	0290	6C68	LTA	QPILOT
0965	0291	8994	MPYK	PLPF29

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0966	0292	4774	IN	TEMP1,7
0967	0293	4F68	OUT	QPILOT,7
0968	0294	6C74	LTA	TEMP1
0969	0295	87E5	MPYK	PLPF28
0970	0296	4768	IN	QPILOT,7
0971	0297	4F74	OUT	TEMP1,7
0972	0298	6C68	LTA	QPILOT
0973	0299	8617	MPYK	PLPF27
0974	029A	4774	IN	TEMP1,7
0975	029B	4F68	OUT	QPILOT,7
0976	029C	6C74	LTA	TEMP1
0977	029D	8446	MPYK	PLPF26
0978	029E	4768	IN	QPILOT,7
0979	029F	4F74	OUT	TEMP1,7
0980	02A0	6C63	LTA	QPILOT
0981	02A1	828E	MPYK	PLPF25
0982	02A2	4774	IN	TEMP1,7
0983	02A3	4F68	OUT	QPILOT,7
0984	02A4	6C74	LTA	TEMP1
0985	02A5	8106	MPYK	PLPF24
0986	02A6	4768	IN	QPILOT,7
0987	02A7	4F74	OUT	TEMP1,7
0988	02A8	6C63	LTA	QPILOT
0989	02A9	9FC1	MPYK	PLPF23
0990	02AA	4774	IN	TEMP1,7
0991	02AB	4F68	OUT	QPILOT,7
0992	02AC	6C74	LTA	TEMP1
0993	02AD	9ECA	MPYK	PLPF22
0994	02AE	4768	IN	QPILOT,7
0995	02AF	4F74	OUT	TEMP1,7
0996	02B0	6C68	LTA	QPILOT
0997	02B1	9E27	MPYK	PLPF21
0998	02B2	4774	IN	TEMP1,7
0999	02B3	4F68	OUT	QPILOT,7
1000	02B4	6C74	LTA	TEMP1
1001	02B5	9DD4	MPYK	PLPF20
1002	02B6	4768	IN	QPILOT,7
1003	02B7	4F74	OUT	TEMP1,7
1004	02B8	6C68	LTA	QPILOT
1005	02B9	9DCA	MPYK	PLPF19
1006	02BA	4774	IN	TEMP1,7
1007	02BB	4F68	OUT	QPILOT,7
1008	02BC	6C74	LTA	TEMP1
1009	02BD	9DF3	MPYK	PLPF18
1010	02BE	4768	IN	QPILOT,7
1011	02BF	4F74	OUT	TEMP1,7
1012	02C0	6C68	LTA	QPILOT
1013	02C1	9E57	MPYK	PLPF17
1014	02C2	4774	IN	TEMP1,7
1015	02C3	4F68	OUT	QPILOT,7
1016	02C4	6C74	LTA	TEMP1
1017	02C5	9ECD	MPYK	PLPF16
1018	02C6	4768	IN	QPILOT,7
1019	02C7	4F74	OUT	TEMP1,7
1020	02C8	6C68	LTA	QPILOT
1021	02C9	9F4D	MPYK	PLPF15
1022	02CA	4774	IN	TEMP1,7

1023	02CB	4F6B	OUT	QPILOT,7
1024	02CC	6C74	LTA	TEMP1
1025	02CD	9FC7	MPYK	PLPF14
1026	02CE	476B	IN	QPILOT,7
1027	02CF	4F74	OUT	TEMP1,7
1028	02D0	6C6B	LTA	QPILOT
1029	02D1	8031	MPYK	PLPF13
1030	02D2	4774	IN	TEMP1,7
1031	02D3	4F6B	OUT	QPILOT,7
1032	02D4	6C74	LTA	TEMP1
1033	02D5	80B1	MPYK	PLPF12
1034	02D6	476B	IN	QPILOT,7
1035	02D7	4F74	OUT	TEMP1,7
1036	02D8	6C6B	LTA	QPILOT
1037	02D9	80B4	MPYK	PLPF11
1038	02DA	476B	IN	IPILOT,7
1039	02DB	4F6B	OUT	IPILOT,7
1040	02DC	6C74	LTA	TEMP1
1041	02DD	80C9	MPYK	PLPF10
1042	02DE	476B	IN	IPILOT,7
1043	02DF	4F6B	OUT	IPILOT,7
1044	02E0	6C74	LTA	TEMP1
1045	02E1	80C8	MPYK	PLPF9
1046	02E2	476B	IN	IPILOT,7
1047	02E3	4F6B	OUT	IPILOT,7
1048	02E4	6C74	LTA	TEMP1
1049	02E5	80B0	MPYK	PLPF8
1050	02E6	476B	IN	IPILOT,7
1051	02E7	4F6B	OUT	IPILOT,7
1052	02E8	6C74	LTA	TEMP1
1053	02E9	80B8	MPYK	PLPF7
1054	02EA	476B	IN	IPILOT,7
1055	02EB	4F6B	OUT	IPILOT,7
1056	02EC	6C74	LTA	TEMP1
1057	02ED	8060	MPYK	PLPF6
1058	02EE	476B	IN	IPILOT,7
1059	02EF	4F6B	OUT	IPILOT,7
1060	02F0	6C74	LTA	TEMP1
1061	02F1	8036	MPYK	PLPF5
1062	02F2	476B	IN	IPILOT,7
1063	02F3	4F6B	OUT	IPILOT,7
1064	02F4	6C74	LTA	TEMP1
1065	02F5	8011	MPYK	PLPF4
1066	02F6	476B	IN	IPILOT,7
1067	02F7	4F6B	OUT	IPILOT,7
1068	02F8	6C74	LTA	TEMP1
1069	02F9	9FF6	MPYK	PLPF3
1070	02FA	476B	IN	IPILOT,7
1071	02FB	4F6B	OUT	IPILOT,7
1072	02FC	6C74	LTA	TEMP1
1073	02FD	9FE6	MPYK	PLPF2
1074	02FE	476B	IN	IPILOT,7
1075	02FF	4F6B	OUT	IPILOT,7
1076	0300	6C74	LTA	TEMP1
1077	0301	9F34	MPYK	PLPF1
1078	0302	7F8F	APAC	
1079	0303	596B	SACH	QPILOT,1

1080 \*  
 1081 \* Sine and Cosine Calculation  
 1082 ● ORIGINAL PAGE IS  
 1083 \* The values for sin & cos are OF POOR QUALITY  
 1084 \* stored for the region 0 -  $\pi/4$   
 1085 \* in 128 locations each; the pilot  
 1086 \* samples are first stripped for  
 1087 \* sign and then compared to determine  
 1088 ● the octant before table lookup;  
 1089 \* the sign is then re-appended after  
 1090 \* the values have been determined;  
 1091 \*  
 1092 0304 6568 ZALM QPILOT )  
 1093 0305 587C SACH QSIGN ) Strip Q pilot sign.  
 1094 0306 7F88 ABS )  
 1095 0307 5874 SACH TEMP1  
 1096 0308 6568 ZALM IPILOT )  
 1097 0309 587B SACH ISIGN ) Strip I pilot sign.  
 1098 030A 7F88 ABS )  
 1099 030B 5875 SACH TEMP2  
 1100 030C 6274 SUBH TEMP1 ) Compare magnitudes to  
 1101 030C FA00 BLZ IOVERC ) determine octant.  
 030E 0342  
 1102 \*  
 1103 030F 6574 COVERI ZALM TEMP1 ) Check if denominator  
 1104 0310 FE00 BNZ DIVQOI ) equals zero.  
 0311 0319  
 1105 0312 7F89 ZAC  
 1106 0313 5061 SACL COS  
 1107 0314 7E01 LACK >1  
 1108 0315 007A ADD SNOFST  
 1109 0316 675E TBLR SIN  
 1110 0317 F900 B FIXSGN  
 0318 032F  
 1111 \*  
 1112 ● N.B. : NOP's are inserted after each SUBC  
 1113 \* instruction because the instruction  
 1114 \* following a SUBC may not use the  
 1115 \* accumulator.  
 1116 \*  
 1117 0319 6475 DIVQOI SUBC TEMP2 ) 7 Bit Fractional  
 1118 031A 7F80 NOP  
 1119 031B 6475 SUBC TEMP2 ) Divide  
 1120 031C 7F80 NOP  
 1121 031D 6475 SUBC TEMP2 )  
 1122 031E 7F80 NOP  
 1123 031F 6475 SUBC TEMP2 )  
 1124 0320 7F80 NOP  
 1125 0321 6475 SUBC TEMP2 )  
 1126 0322 7F80 NOP  
 1127 0323 6475 SUBC TEMP2 )  
 1128 0324 7F80 NOP  
 1129 0325 6475 SUBC TEMP2 ) End of Divide  
 1130 0326 7F80 NOP  
 1131 0327 5075 SACL TEMP2  
 1132 0328 2175 LAC TEMP2,1  
 1133 0329 007A ADD SNOFST

1134	032A	675E		TBLR	SIN	) Read sine value.
1135	032B	5075		SACL	TEMP2	
1136	032C	7E01		LACK	1	) Increment lookup address.
1137	032C	0075		ADD	TEMP2	
1138	032E	6761		TBLR	COS	) Read cosine value.
1139	032F	657B	FIXSGN	ZALH	ISIGN	
1140	0330	FA00		BLZ	SUBI1	)
	0331	0337				
1141	0332	657C		ZALH	QSIGN	) Re-append Sign.
1142	0333	FA00		BLZ	SUBQ1	)
	0334	033E				
1143	0335	F900		B	STEPS	
	0336	0373				
1144	0337	1061	SUBI1	SUB	COS	
1145	0338	5061		SACL	COS	
1146	0339	657C		ZALH	QSIGN	
1147	033A	FA00		BLZ	SUBQ1	
	033E	033E				
1148	033C	F900		B	STEPS	
	033C	0373				
1149	033E	105E	SUBQ1	SUB	SIN	
1150	033F	505E		SACL	SIN	
1151	0340	F900		B	STEPS	
	0341	0373				
1152			*			
1153	0342	6575	IOVERQ	ZALH	TEMP2	) Check if denominator
1154	0343	FE00		BNZ	DIVIOQ	) equals zero.
	0344	034C				
1155	0345	7F89		ZAC		
1156	0346	505E		SACL	SIN	
1157	0347	7E01		LACK	>1	
1158	0348	007A		ADD	SNOFST	
1159	0349	6761		TBLR	CCS	
1160	034A	F900		B	SGNFIX	
	034B	0362				
1161			●			
1162			*			
1163			*			
1164			*			
1165			*			
1166			*			
1167	034C	6474	DIVIOQ	SUBC	TEMP1	) 7 Bit Fractional
1168	034C	7F80		NOP		
1169	034E	6474		SUBC	TEMP1	) Divide
1170	034F	7F80		NOP		
1171	0350	6474		SUBC	TEMP1	) .
1172	0351	7F80		NOP		
1173	0352	6474		SUBC	TEMP1	) .
1174	0353	7F80		NOP		
1175	0354	6474		SUBC	TEMP1	) .
1176	0355	7F80		NOP		
1177	0356	6474		SUBC	TEMP1	) .
1178	0357	7F80		NOP		
1179	0358	6474		SUBC	TEMP1	) End of Divide
1180	0359	7F80		NOP		
1181	035A	5074		SACL	TEMP1	
1182	035B	2174		LAC	TEMP1,1	

N.B. : NOP's are inserted after each SUBC instruction because the instruction following a SUBC may not use the accumulator.

1183	035C	007A		ADD	SNQFST	
1184	035C	6761		TBLR	COS	) Read cosine value.
1185	035E	5075		SACL	TEMP2	
1186	035F	7E01		LACK	1	) Increment lookup address.
1187	0360	0075		ADD	TEMP2	
1188	0361	675E		TBLR	SIN	) Read sine value.
1189	0362	657B	SGNFIX	ZALH	ISIGN	
1190	0363	FA00		BLZ	SUBI2	)
	0364	036A				
1191	0365	657C		ZALH	QSIGN	) Re-append Sign.
1192	0366	FA00		BLZ	SUBQ2	)
	0367	0371				
1193	0368	F900		B	STEPS	
	0369	0373				
1194	036A	1061	SUBI2	SUB	COS	
1195	036B	5061		SACL	COS	
1196	036C	657C		ZALH	QSIGN	
1197	036D	FA00		BLZ	SUBQ2	
	036E	0371				
1198	036F	F900		B	STEPS	
	0370	0373				
1199	0371	105E	SUBQ2	SUB	SIN	
1200	0372	505E		SACL	SIN	
1201			*			
1202			*			
1203			*			
1204			*			
1205	0373	6562	STEPS	ZALH	PRECOS	
1206	0374	6261		SUBH	COS	
1207	0375	587B		SACH	ISIGN,0	
1208	0376	7F88		ABS		
1209	0377	5874		SACH	TEMP1,0	
1210	0378	6A74		LT	TEMP1	
1211			*			
1212	0379	8333		MPYK	>333	) Multiply by 1/5.
1213	037A	7F8E		PAC		
1214	037B	0B72		ADD	ONE,11	) Round off result.
1215			*			
1216	037C	5066		SACL	COSSTP	
1217	037D	657B		ZALH	ISIGN	
1218	037E	FD00		BGEZ	NEXT1	
	037F	0382				
1219	0380	1066		SUB	COSSTP	) Correct for negative
1220	0381	5066		SACL	COSSTP	) result.
1221			*			
1222	0382	655F	NEXT1	ZALH	PRESIN	
1223	0383	625E		SUBH	SIN	
1224	0384	587C		SACH	QSIGN,0	
1225	0385	7F88		ABS		
1226	0386	5874		SACH	TEMP1,0	
1227	0387	6A74		LT	TEMP1	
1228			•			
1229	0388	8333		MPYK	>333	) Multiply by 1/5.
1230	0389	7F8E		PAC		
1231	038A	0B72		ADD	ONE,11	) Round off result.
1232			*			
1233	038B	5064		SACL	SINSTP	

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1234	038C	657C	ZALH	QSIGN	
1235	038D	FD00	BGEZ	NEXT2	
	038E	0391			
1236	038F	1064	SUB	SINSTP	) Correct for negative
1237	0390	5064	SACL	SINSTP	) result.
1238			*		
1239	0391	6569	NEXT2	ZALH	OLDIP
1240	0392	6268		SUBH	IPILOT
1241	0393	587B		SACH	ISIGN,0
1242	0394	7F88		ABS	
1243	0395	5874		SACH	TEMP1,0
1244	0396	6A74		LT	TEMP1
1245			*		
1246	0397	8333		MPYK	>333
1247	0398	7F8E		PAC	
1248	0399	0872		ADD	ONE,11
1249			*		
1250	039A	506E		SACL	IPSTP
1251	039B	657B		ZALH	ISIGN
1252	039C	FD00		BGEZ	NEXT3
	039D	03A0			
1253	039E	106E		SUB	IPSTP
1254	039F	506E		SACL	IPSTP
1255			*		
1256	03A0	656C	NEXT3	ZALH	OLDQP
1257	03A1	626B		SUBH	QPILOT
1258	03A2	587C		SACH	QSIGN,0
1259	03A3	7F88		ABS	
1260	03A4	5874		SACH	TEMP1
1261	03A5	6A74		LT	TEMP1
1262			*		
1263	03A6	8333		MPYK	>333
1264	03A7	7F8E		PAC	
1265	03A8	0872		ADD	ONE,11
1266			*		
1267	03A9	5070		SACL	QPSTP
1268	03AA	657C		ZALH	QSIGN
1269			*		
1270	03AB	4D72		OUT	ONE,5
1271			*		
1272	03AC	FD00		BGEZ	BKGRND
	03AC	00F7			
1273	03AE	1070		SUB	QPSTP
1274	03AF	5070		SACL	QPSTP
1275			*		
1276	03B0	F900		B	BKGRND
	03B1	00F7			
1277			*		
1278			*		
1279			*		
1280	03B2	6E00	RESET	LDPK	0
1281	03B3	7F8B		SOVM	
1282			*		
1283	03B4	4000		IN	>0,0
1284	03B5	4000		OUT	>0,5
1285			*		
1286	03B6	7E01		LACK	1

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Reset Initialization Routine

) Point to data page 0.  
) Set overflow mode.

) Clear interrupt pin.  
) Reset ram counters.

```

1287 03B7 5000      SACL      >0
1288 03B8 6A00      LT        >0
1289                *
1290 03B9 6880      LARP      0
1291 03BA 707F      LARK      0,>7F
1292 03BB 7F89      ZAC
1293 03BC 5088      CLRRAM SACL  *
1294 03BD F400      BANZ      CLRRAM
      03BE 03BC
1295                *
1296 03BF 7054      LARK      0,IBUFF
1297 03C0 7159      LARK      1,QBUFF
1298                *
1299 03C1 7E01      LACK      1
1300 03C2 5072      SACL      ONE
1301 03C3 8500      MPYK      OFFSET
1302 03C4 7F8E      PAC
1303 03C5 507A      SACL      CSOFST
1304                *
1305 03C6 F900      B          BKGRND
      03C7 00F7
1306                *
1307                *
1308                *      Sine and Cosine Table Lookup Values
1309                *
1310                *
1311 0500      ADRG      >500
1312                *
1313 0500 0000      DATA     0,32767,258,32767,516,32764
      0501 7FFF
      0502 0102
      0503 7FFF
      0504 0204
      0505 7FFC
1314 0506 0306      DATA     774,32759,1032,32752,1289,32743
      0507 7FF7
      0508 0408
      0509 7FF0
      050A 0509
      050B 7FE7
1315 050C 060A      DATA     1546,32731,1803,32718,2060,32703
      050D 7F0B
      050E 0703
      050F 7FCE
      0510 080C
      0511 7FBF
1316 0512 090C      DATA     2316,32686,2572,32667,2828,32646
      0513 7FAE
      0514 0A0C
      0515 7F98
      0516 0B0C
      0517 7F86
1317 0518 0C0A      DATA     3082,32623,3337,32598,3590,32571
      0519 7F6F
      051A 0D09
      051B 7F56
      051C 0E06

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) Clear internal ram.

) Initialize auxiliary  
) register pointers.

) Store constants in ram.

) Branch to waiting state.



	051C 7F3B		
1318	051E 0F04	DATA	3844,32542,4096,32511,4347,32478
	051F 7F1E		
	0520 1000		
	0521 7EFF		
	0522 10F3		
	0523 7EDE		
1319	0524 11F6	DATA	4598,32444,4848,32407,5097,32369
	0525 7EBC		
	0526 12F0		
	0527 7E97		
	0528 13E9		
	0529 7E71		
1320	052A 14E2	DATA	5346,32329,5593,32287,5839,32244
	052B 7E49		
	052C 15D9		
	052D 7E1F		
	052E 16CF		
	052F 7DF4		
1321	0530 17C5	DATA	6085,32198,6329,32151,6572,32102
	0531 7DC6		
	0532 1889		
	0533 7D97		
	0534 19AC		
	0535 7D66		
1322	0536 1A9E	DATA	6814,32052,7055,32000,7295,31946
	0537 7D34		
	0538 188F		
	0539 7D00		
	053A 1C7F		
	053B 7CCA		
1323	053C 1D6D	DATA	7533,31890,7770,31833,8006,31775
	053D 7C92		
	053E 1E5A		
	053F 7C59		
	0540 1F46		
	0541 7C1F		
1324	0542 2031	DATA	8241,31715,8474,31653,8706,31590
	0543 78E3		
	0544 211A		
	0545 78A5		
	0546 2202		
	0547 7866		
1325	0548 22E8	DATA	8936,31526,9166,31460,9393,31393
	0549 7826		
	054A 23CE		
	054B 7AE4		
	054C 24B1		
	054D 7AA1		
1326	054E 2593	DATA	9619,31324,9844,31254,10067,31183
	054F 7A5C		
	0550 2674		
	0551 7A16		
	0552 2753		
	0553 79CF		
1327	0554 2831	DATA	10289,31111,10509,31037,10727,30962
	0555 7987		

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	0556	290D		
	0557	793D		
	0558	29E7		
	0559	78F2		
1328	055A	2AC0	DATA	10944,30886,11159,30809,11373,30731
	055B	78A6		
	055C	2B97		
	055D	7859		
	055E	2C6D		
	055F	780B		
1329	0560	2D41	DATA	11585,30652,11795,30571,12004,30490
	0561	77EC		
	0562	2E13		
	0563	776B		
	0564	2EE4		
	0565	771A		
1330	0566	2FE3	DATA	12211,30408,12416,30325,12620,30240
	0567	76C8		
	0568	3080		
	0569	7675		
	056A	314C		
	056B	7620		
1331	056C	3216	DATA	12822,30155,13022,30069,13221,29983
	056D	75C8		
	056E	32DE		
	056F	7575		
	0570	33A5		
	0571	751F		
1332	0572	3469	DATA	13417,29895,13613,29807,13806,29718
	0573	74C7		
	0574	352D		
	0575	746F		
	0576	35EE		
	0577	7416		
1333	0578	36AD	DATA	13997,29628,14187,29537,14375,29446
	0579	738C		
	057A	376B		
	057B	7361		
	057C	3827		
	057D	7306		
1334	057E	38E2	DATA	14562,29355,14746,29262,14929,29169
	057F	72AB		
	0580	399A		
	0581	724E		
	0582	3A51		
	0583	71F1		
1335	0584	3B06	DATA	15110,29076,15290,28982,15467,28888
	0585	7194		
	0586	3B8A		
	0587	7136		
	0588	3C6B		
	0589	70D8		
1336	058A	3D18	DATA	15643,28793,15818,28698,15990,28602
	058B	7079		
	058C	3DCA		
	058D	701A		
	058E	3E76		

1337	058F 6F8A 0590 3F21 0591 6F5A 0592 3FCA 0593 6EF9 0594 4071 0595 6E98	DATA	16161,28506,16330,28409,16497,28312
1338	0596 4117 0597 6E37 0598 418A 0599 6DD6 059A 425D 059B 6D74	DATA	16663,28215,16826,28118,16989,28020
1339	059C 42FD 059D 6D12 059E 439C 059F 6CB0 05A0 4439 05A1 6C4E	DATA	17149,27922,17308,27824,17465,27726
1340	05A2 44D4 05A3 68EB 05A4 456E 05A5 6888 05A6 4606 05A7 6826	DATA	17620,27627,17774,27528,17926,27430
1341	05A8 469D 05A9 6AC3 05AA 4732 05AB 6A60 05AC 47C5 05AD 69FC	DATA	18077,27331,18226,27232,18373,27132
1342	05AE 4857 05AF 6999 05B0 48E7 05B1 6936 05B2 4975 05B3 68D3	DATA	18519,27033,18663,26934,18905,26835
1343	05B4 4A02 05B5 686F 05B6 4A8E 05B7 680C 05B8 4B17 05B9 67A9	DATA	18946,26735,19086,26636,19223,26537
1344	05BA 4BA0 05BB 6746 05BC 4C26 05BD 66E2 05BE 4CAC 05BF 667F	DATA	19360,26438,19494,26338,19628,26239
1345	05C0 4D2F 05C1 661C 05C2 4DB2 05C3 65B9 05C4 4E32 05C5 6556	DATA	19759,26140,19890,26041,20018,25942
1346	05C6 4EB2 05C7 64F4	DATA	20146,25844,20272,25745,20396,25647

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	05C8 4F30		
	05C9 6491		
	05CA 4FAC		
	05CB 642F		
1347	05CC 5027	DATA	20519,25548,20641,25450,20761,25352
	05CD 63CC		
	05CE 50A1		
	05CF 636A		
	05D0 5119		
	05D1 6308		
1348	05D2 5190	DATA	20880,25254,20997,25157,21113,25059
	05D3 62A6		
	05D4 5205		
	05D5 6245		
	05D6 5279		
	05D7 61E3		
1349	05D8 52EC	DATA	21228,24962,21341,24865,21453,24769
	05D9 6182		
	05DA 5350		
	05DB 6121		
	05DC 53CD		
	05DD 60C1		
1350	05DE 543C	DATA	21564,24672,21674,24576,21782,24480
	05DF 6060		
	05E0 54AA		
	05E1 6000		
	05E2 5516		
	05E3 5FA0		
1351	05E4 5581	DATA	21889,24385,21995,24290,22099,24195
	05E5 5F41		
	05E6 55EB		
	05E7 5EE2		
	05E8 5653		
	05E9 5E83		
1352	05EA 56BA	DATA	22202,24100,22304,24005,22405,23911
	05EB 5E24		
	05EC 5720		
	05ED 5DC5		
	05EE 5785		
	05EF 5D67		
1353	05F0 57E9	DATA	22505,23818,22603,23724,22701,23631
	05F1 5D0A		
	05F2 5848		
	05F3 5CAC		
	05F4 58AD		
	05F5 5C4F		
1354	05F6 5900	DATA	22797,23538,22892,23446,22986,23354
	05F7 5BF2		
	05F8 596C		
	05F9 5896		
	05FA 59CA		
	05FB 583A		
1355	05FC 5A27	DATA	23079,23262,23170,23170
	05FD 5ADE		
	05FE 5A82		
	05FF 5A82		
1356			

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1357      *      Bootstrapping Routine for
1358      @      Loading Program Code from
1359      @      EPROM's to RAM.
1360      *
1361 0700      AORG      >700
1362      *
1363 0700 7E01  BOOT     LACK      >1
1364 0701 5000      SACL      >0
1365 0702 6A00      LT       >0
1366 0703 87FF      MPYK     >7FF
1367 0704 7F8E      PAC
1368 0705 670A  NOTDUN  TBLR     >A
1369 0706 7D0A      TBLW     >A
1370 0707 1000      SUB      >0
1371 0708 FD00      BGEZ     NOTDUN
      0709 0705
1372 070A 83B2      MPYK     RESET
1373 070B 7F8E      PAC
1374 070C 500A      SACL     >A
1375 070D 7E01      LACK     >1
1376 070E 7D0A      TBLW     >A
1377 070F F900      B        RESET
      0710 03B2
1378      *
1379      END
NO ERRORS, NO WARNINGS
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